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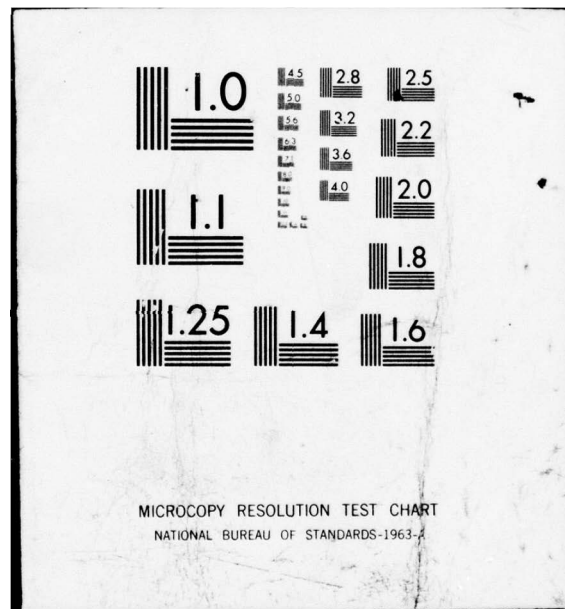
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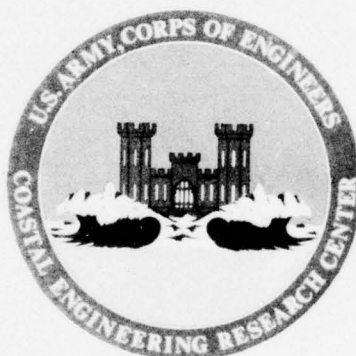
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TR 76-3

Storm Surge Simulation in Transformed Coordinates

VOLUME II
Program Documentation

by
John J. Wanstrath

TECHNICAL REPORT NO. 76-3
NOVEMBER 1976



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A two-dimensional time-dependent numerical storm surge model using orthogonal curvilinear coordinates is presented. The curvilinear coordinate system is based on a conformal mapping of the interior region bounded by the actual coast, the seaward boundary (taken as the 180-meter depth contour) and two parallel lateral boundaries into a rectangle in the image plane. Three regions of the Continental Shelf of the Gulf of Mexico and two regions of the eastern seaboard of the United States are mapped.		

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Since the transformation is conformal, the associated modifications of the vertically integrated equations of motion and mass continuity are minimized. The coast, seaward boundary, and the lateral boundaries of the computing grid are straight lines in the image plane thus facilitating the application of the boundary conditions. The final coordinates allow for the greatest resolution near the coast in a central area of principal storm surge development and modification.

The model is employed in the simulation of the storm surge induced by Hurricanes Carla (1961) and Camille (1969) which crossed the gulf coast of the United States and Hurricane Gracie (1959) which crossed the east coast. Analytical interpretations of the wind and atmospheric pressure-forcing functions are used in the computations.

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PREFACE

This report is published to provide coastal engineers with the results of a study to develop an operational program for numerical simulation of storm surges on a given segment of the Continental Shelf, using a curvilinear coordinate system. The report consists of two volumes. Volume I discusses the theory and application of the transformation procedure for generating the curvilinear shelf coordinate system for particular regions, and the theory, numerical algorithm, and application of the storm surge program for simulation of Hurricanes Carla (1961), Camille (1969), and Gracie (1959). Volume II presents the program documentation and the coded programs for carrying out the coordinate transformation (CONFORM), for establishing the spatial lattice (GRID), and for carrying out the storm surge calculations on the shelf (SSURGE). The work was carried out under the wave mechanics program of the U.S. Army Coastal Engineering Research Center (CERC).

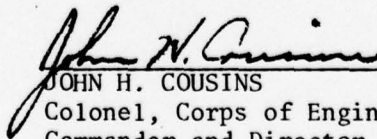
This volume was prepared by John J. Wanstrath; Volume I was prepared by John J. Wanstrath, Robert E. Whitaker, Robert O. Reid, and Andrew C. Vastano, Department of Oceanography, Texas A&M University, College Station, Texas, under CERC Contract No. DACW72-73-C-0014. Most of the computational work in the development and application was carried out at the National Center for Atmospheric Research which is supported by the National Science Foundation.

The authors express their appreciation to Thomas J. Reid for assistance in program coding, and to Dr. D. Lee Harris, CERC, for very constructive comments on the draft of this report.

Dr. D. Lee Harris, Chief, Oceanography Branch, was the CERC technical monitor of the report, under the general supervision of Mr. R.P. Savage, Chief, Research Division.

Comments on this publication are invited.

Approved for publication in accordance with Public Law 166, 79th Congress, approved 31 July 1945, as supplemented by Public Law 172, 88th Congress, approved 7 November 1963.


JOHN H. COUSINS
Colonel, Corps of Engineers
Commander and Director

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CONVERSION FACTORS, U. S. CUSTOMARY TO METRIC (SI) UNITS OF MEASUREMENT

U.S. customary units of measurement used in this report can be converted to metric (SI) units as follows:

Multiply	by	To obtain
inches	25.4	millimeters
	2.54	centimeters
square inches	6.452	square centimeters
cubic inches	16.39	cubic centimeters
feet	30.48	centimeters
	0.3048	meters
square feet	0.0929	square meters
cubic feet	0.0283	cubic meters
yards	0.9144	meters
square yards	0.836	square meters
cubic yards	0.7646	cubic meters
miles	1.6093	kilometers
square miles	259.0	hectares
acres	0.4047	hectares
foot-pounds	1.3558	newton meters
ounces	28.35	grams
pounds	453.6	grams
	0.4536	kilograms
ton, long	1.0160	metric tons
ton, short	0.9072	metric tons
degrees (angle)	0.1745	radians
Fahrenheit degrees	5/9	Celsius degrees or Kelvins ¹

¹ To obtain Celsius (C) temperature readings from Fahrenheit (F) readings, use formula: $C = (5/9)(F - 32)$.
To obtain Kelvin (K) readings, use formula: $K = (5/9)(F - 32) + 273.15$.

STORM SURGE SIMULATION IN TRANSFORMED COORDINATES

Volume II. Program Documentation

by
John J. Wanstrath

I. INTRODUCTION

Presented in this volume are the program documentation and listings of the coded programs for carrying out a simulation of a hurricane-induced storm surge on the Continental Shelf in curvilinear coordinates for a given reach of shelf. There are three separate programs detailed here for this purpose.

The first program, CONFORM, is employed for evaluation of the transformation coefficients which map the given reach of the Continental Shelf into a rectangle in the image plane, the shelf region being delineated by a smoothed version of the coastline, the shelf break (taken as the 180-meter depth contour in the examples), and bounded laterally by two parallel straight lines. The theory and several example applications of the transformation procedure are given in Section II of Volume I. The example input for CONFORM contained in the listings here are for the mapping of the region from a section across Laguna Madre about 90 kilometers south of Brownsville to Marsh Island. Particular care must be taken to follow the procedure exactly for the example if CONFORM is to be verified by obtaining the given transformation coefficients. This procedure is given explicitly in the CONFORM documentation.

The second program, GRID, develops the detailed computing grid information, based on the mapping coefficients evaluated by CONFORM plus coordinate stretching information supplied by the user (see Section III of Volume I). Part of the output of GRID is a listing of the grid positions which are required by the user in order to read from appropriate charts the detailed bathymetry field, which is necessary input for the final program SSURGE. The example data supplied here for GRID are for the Laguna Madre to Marsh Island region.

Program SSURGE (Shelf Surge) carries out the numerical integration of the storm surge equations in the transformed coordinate system supplied by CONFORM and GRID, using a parametric representation of a hurricane wind field and pressure field. The theory is given in Section III of Volume I. The particular example data given here are for Hurricane Carla and the Laguna Madre-Marsh Island grid system.

The appendixes to this volume contain detailed FORTRAN listings of the three programs in this application. The data to be supplied by the user for other applications are discussed in the documentation of each of these programs.

II. COMPUTER PROGRAM DOCUMENTATION FOR PROGRAM-CONFORM

1. Program Purpose.

The purpose of the program is to determine the transformation coefficients which will conformally map the interior region bounded by the actual coastline, a seaward boundary curve, and two parallel lateral boundaries into a rectangle in the image plane.

2. Program Description.

The program is written in FORTRAN IV language. This program and the program GRID provide all the necessary computing grid data for input to program SSURGE. The program GRID takes, as input, the transformation coefficients and determines the computing grid information (such as, scale factors, grid point locations, and, at each grid point, the orientation of the ξ -axis to the x -axis).

The program CONFORM is composed of:

MAIN	Defines constants. Reads and writes the coordinates delineating the given coastline and seaward boundary curve. Calls Subroutine COEFFS.
SUBROUTINE COEFFS	Determines the transformation coefficients. At the completion of each iteration, the coefficients, the variance between the transform-generated curves and that specified, and other pertinent information are written. COEFFS interfaces all other program subroutines and functions.
FUNCTION XTRAN	Is the transformation function $x(\xi, \eta)$.
FUNCTION YTRAN	Is the transformation function $y(\xi, \eta)$.
SUBROUTINE SLFAC	Determines the scale factor and derivatives, $\partial x / \partial \xi$, $\partial y / \partial \xi$, for a given value of ξ and η .
SUBROUTINE CUR1YB	Determines the necessary parameters to fit a spline under tension through the given <u>coastline</u> coordinates. The spline is fitted with Y_2 as a function of X_2 .
FUNCTION CURVYB	Interpolates the given <u>coastline</u> , returning a value of y at a specified value for x .

FUNCTION CURDYB	Differentiates the given <u>coastline</u> , returning a value of dy/dx at a specified value for x .
SUBROUTINE CUR2YB	Determines the necessary parameters to fit a spline under tension with $X2$ as a function of <u>coastline</u> arclength.
FUNCTION CUR4YB	Interpolates the given <u>coastline</u> returning a value of x at a specified value for arclength.
SUBROUTINE CUR3YB	Determines the necessary parameters to fit a spline under tension with $Y2$ as a function of <u>coastline</u> arclength.
FUNCTION CUR5YB	Interpolates the given <u>coastline</u> returning a value of y at a specified value for arclength.

There are identical subroutines and functions as delineated above for the seaward boundary curve specified by coordinates $X2P$ and $Y2P$. These subroutines and functions are recognized by the same names as their counterparts with a terminal letter A. For example, SUBROUTINE CUR1YA determines the necessary parameters to fit a spline under tension through the given seaward boundary curve.

3. Type of Computer.

The program CONFORM can be run on any computer with minimum core requirements of approximately 24K (based on the present sample program). However, significantly more computer memory would be required if one desires a large number of coefficients and/or numerous integration points. The program has been executed successfully on IBM 360, CDC/6600 and 7600, and GE/635. The present sample program requires no auxiliary storage devices, peripheral devices, or magnetic tape input or output. No site-orientated computer plot routines are involved in the program. Approximately 20 minutes of machine time on a CDD/7600 is required for the sample program (total number of coefficients, $2 \times NMAX = 220$; number of integration points, $0 < \xi < \lambda$, = 110; and number of iterations = 80).

4. Input Data.

Input data, other than constants defined in MAIN, are read in MAIN on IBM cards prepared according to the following list:

(1) Card 1

IWANT, MQ, MOP, NMAX,	Continuation flag, number of shore-
JMAS1, IL, VARWT	line and seaward boundary coordinates

number of mapping coefficients, maximum number of iterations, number of integration points, and the convergence criterion in format 6I5, F5.3.

(2) Card Group 2

X2,Y2 The x,y coordinates (units in x,y space) of the given coastline in the region $0 \leq x \leq \lambda$ are read with one pair per card in format 3X, F7.2, 3X, F7.2 (limit 150).

(3) Card Group 3

X2P,Y2P The x,y coordinates (units in x,y space) of the given seaward boundary curve in the region $0 \leq x \leq \lambda$ are read with one pair per card in format F7.2, 3X, F7.2 (limit 150).

Optional Card 4, Card Group 3, and Card 6

If IWANT = 1, indicating the program is being restarted, the following cards must be supplied:

(4) Card 4

B, BZRO The values of β and B_0 in units of length of x,y space from the last iteration of the previous run in format 2E14.7.

(5) Card Group 5

COB,COC The NMAX cards containing the dimensionless Fourier-type transformation coefficients from the last iteration of the previous run in sequential order with one pair per card (format 2E14.7). If more coefficients are desired in the present run than the previous one, blank cards should be supplied for the difference.

(6) Card 6

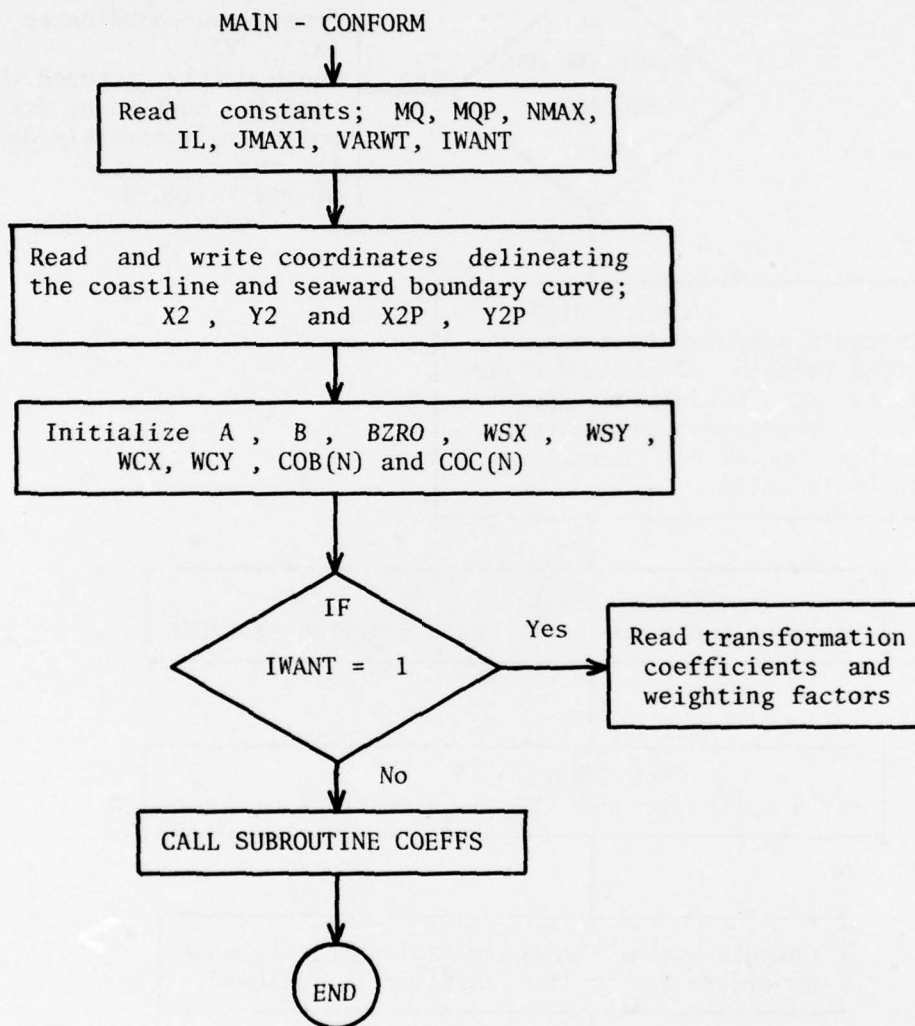
WSX,WSY The value of the weighting factors for the seaward boundary curve (x and y component) and
WCX,WCY coastline (x and y component) from the last iteration of the previous run (4E14.7).

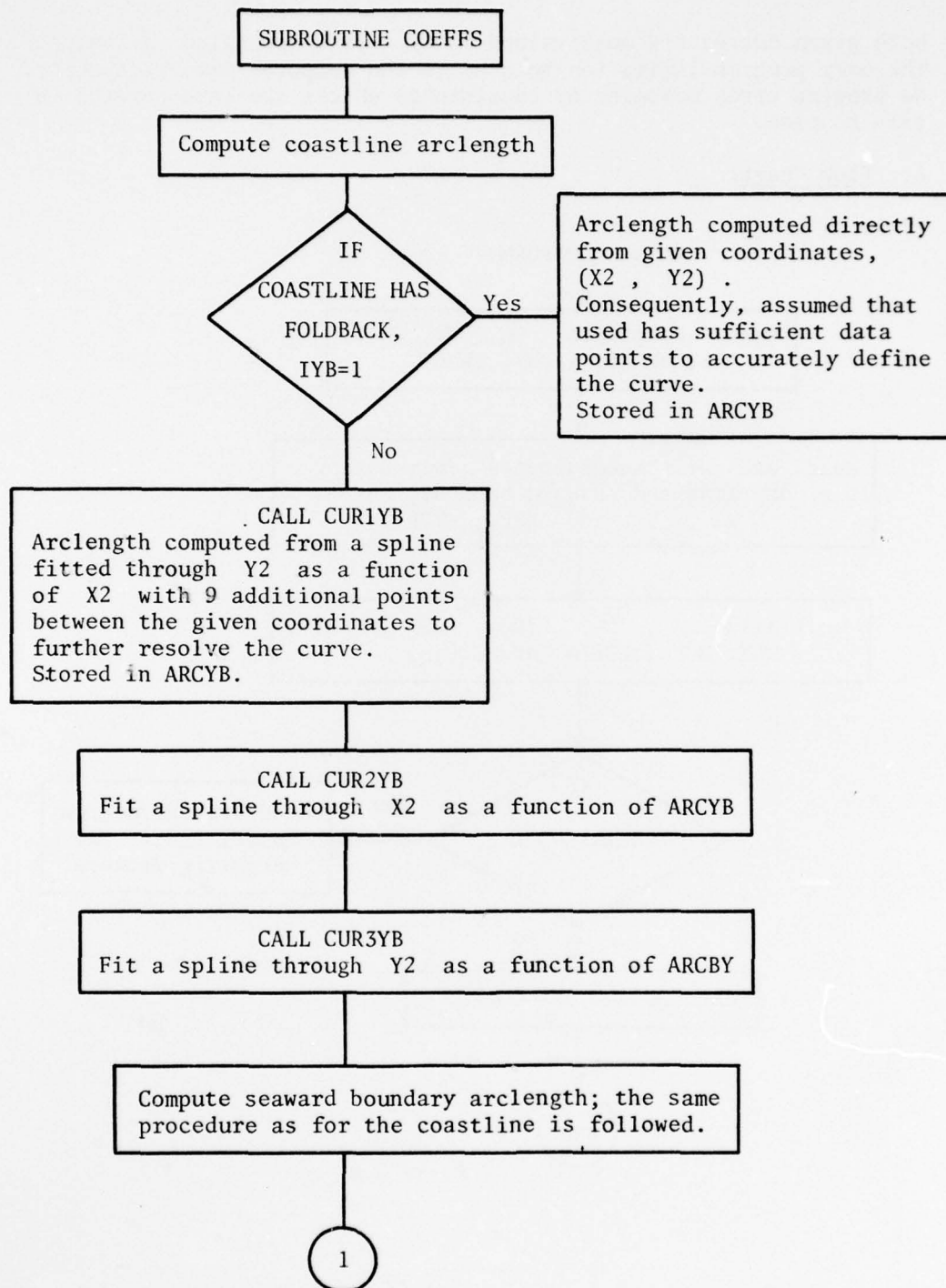
5. Mathematical Procedures and Program Limitations.

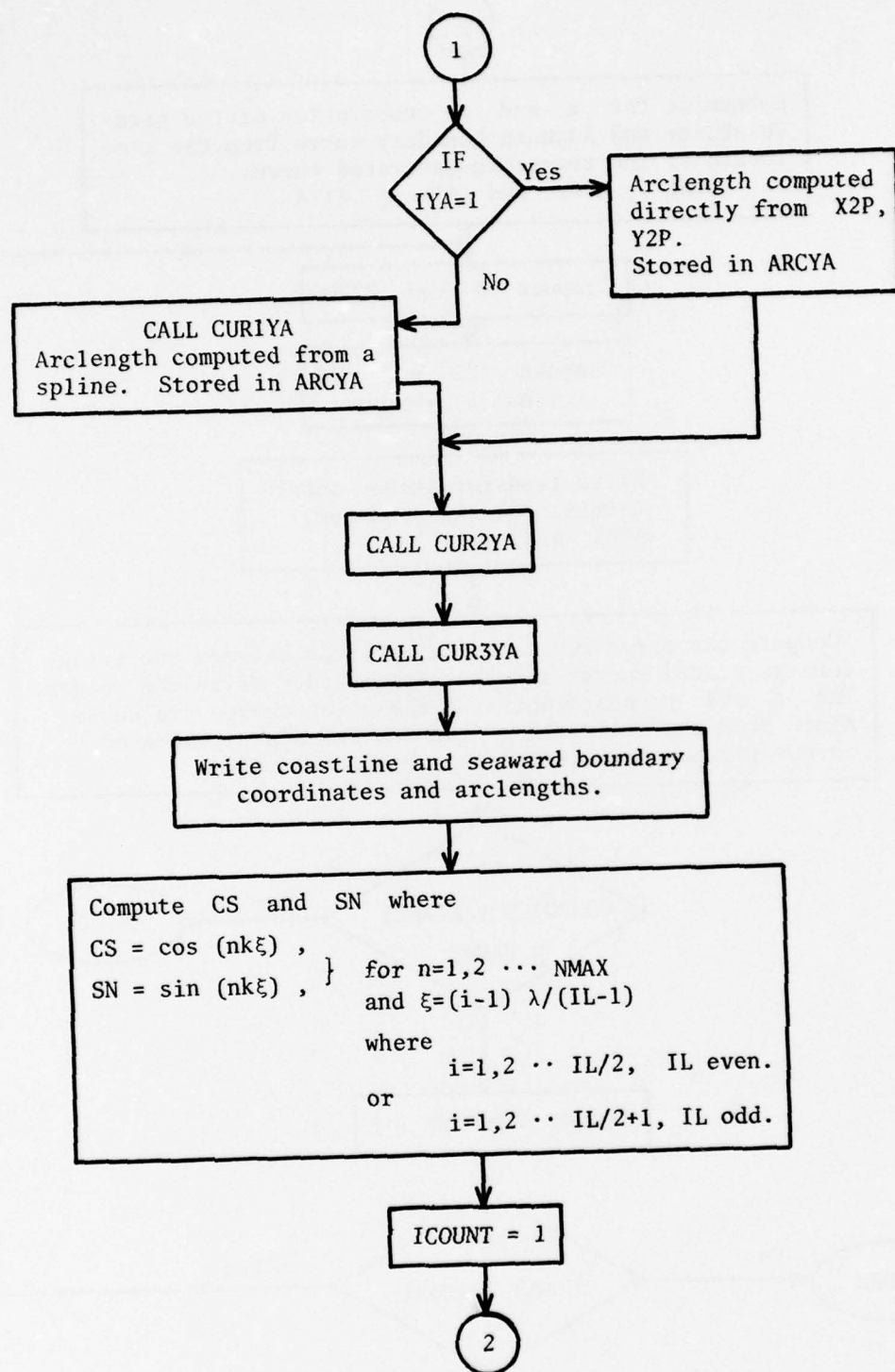
The conformal mapping relations, solutions for the transformation coefficients, and the iterative procedure for determining the coefficients are presented in Volume I of this report. The mapping equations are sufficiently general to treat the situation where either or

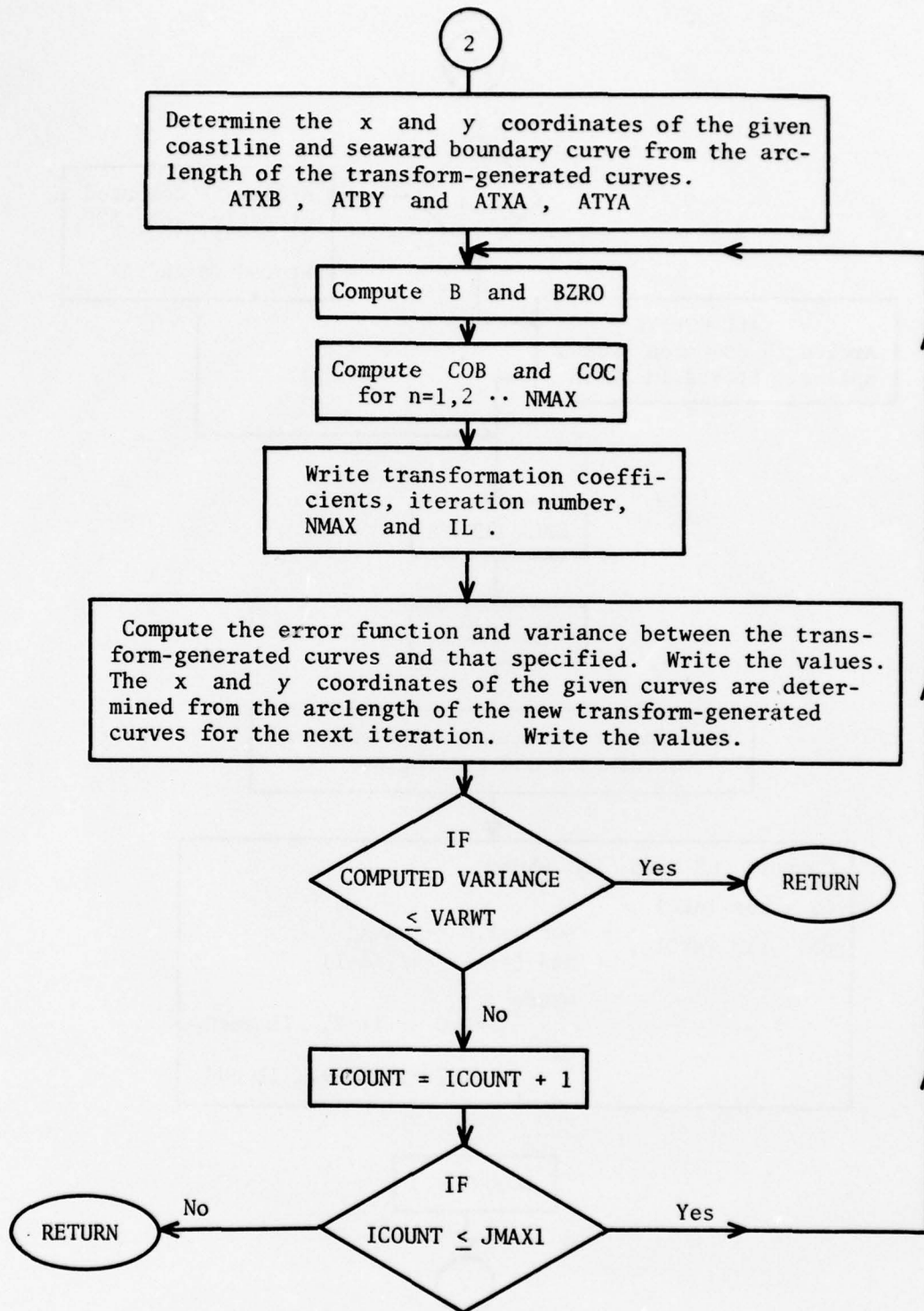
both given curves are multivalued in y for a specified x value. The only program limitation relates to the computer memory capacity. No program error messages or consistency checks are incorporated in this routine.

6. Flow Chart.









7. Glossary and Description of Terms.

Arrays

X2	Dimensioned MQ. Contains values of the x coordinate in units of x,y space of the given coastline (max.150).
Y2	Dimensioned MQ. Contains values of the y coordinate in units of x,y space of the given coastline (max.150).
X2P	Dimensioned MQP. Contains values of the x coordinate in units of x,y space of the given seaward boundary curve (max.150).
Y2P	Dimensioned MQP. Contains values of the y coordinate in units of x,y space of the given seaward boundary curve (max.150).
COB	Dimensioned NMAX. Contains values of the dimensionless transformation coefficient B_n (max.200).
COC	Dimensioned NMAX. Contains values of the dimensionless transformation coefficient C_n (max.200).
DUMB	Dimensioned NMAX. Contains the iterative value for B_n (max.200).
DUMC	Dimensioned NMAX. Contains the iterative value for C_n (max.200).
ARCYB	Dimensioned MQ. Contains values of the arclength for the given coastline coordinates X2 , Y2 (max.150).
ARCYA	Dimensioned MQP. Contains values of the arclength for the given seaward boundary coordinates X2P , Y2P (max.150).
SN	Dimensioned NMAX \times IL1 where IL1 is IL/2 for even IL or IL1 is IL/2 + 1 for odd IL. Contains values of $\sin (nk\xi)$.
CS	Dimensioned NMAX \times IL1. Contains values of $\cos (nk\xi)$.
ATXB	Dimensioned IL. Contains values of the x coordinate of the given coastline as determined from the arclength of the transform-generated curve (max.400).
ATYB	Dimensioned IL. Contains values of the y coordinate of the given coastline as determined from the arclength of the transform-generated curve (max.400).

ATXA Dimensioned IL. Contains values of the x coordinate of the given seaward boundary curve as determined from the arclength of the transform-generated curve (max.400).

ATYA Dimensioned IL. Contains values of the y coordinate of the given seaward boundary curve as determined from the arclength of the transform-generated curve (max.400).

Z Dimensioned IL. Contains values of ξ (max.400).

R,S,T,U,
V,W,X,Y Dimensioned IL. Temporary storage.

Constants

MQ Number of coordinates delineating the given coastline (max.150).

MQP Number of coordinates delineating the given seaward boundary curve (max.150).

NMAX Number of transformation coefficients, B_n or C_n (max.200).

IL Number of equally spaced integration points for $0 \leq \xi \leq \lambda$ with $IL \geq NMAX$ (max.400).

IWANT If IWANT = 1, the program is to be re-started requiring input from the previous run. If IWANT \neq 1, it is the initial mapping of the region.

VARWT Desired variance (in units of x,y space squared) between the transform-generated curves and that specified.

XLAMDA $\lambda = X2(MQ) = X2P(MQP)$

XK $k = \pi/\lambda$

A -B

B β

BZRO B_0

WSX,WSY The x and y component of the weighting factor for the seaward boundary curve.

WCX,WCY The x and y component of the weighting factor for the coastline.

8. Input and Output.

The input data required by CONFORM to determine the transformation coefficients which conformally map the Laguna Madre, Mexico, to Marsh Island, Louisiana, region into a rectangle are presented here as an example. The first card image gives the continuation code, number of coastline and seaward boundary coordinates, number of coefficients desired, maximum number of iterations, number of integration points, and the convergence criterion. The next 47 paired numbers are the coastline coordinates and the last 40 card images give the seaward boundary coordinates.

Program CONFORM provides detailed and voluminous output concerning primarily the rate of convergence. These output statements are not necessary for program completion and can be easily deleted with little alteration to the sequence of instructions. Optional output statements are indicated in the program listing (App. A) by an arrow (\leftarrow) on the right-hand side of the page.

The results from CONFORM required by Program GRID are β , B_0 , and the coefficients, B_n and C_n . These are given in the next section as input to program GRID.

Reference to Table 4 in Volume I of this report shows the values for the number of coefficients, maximum number of iterations, and number of integration points are only indicative of the final steps of this particular application. Explicitly, in order to obtain the given coefficients to conformally map the Laguna Madre to Marsh Island region into a rectangle in the image plane, the following steps must be followed:

- (1) Set NMAX to 40 and IL to 80 for the first 20 iterations.
- (2) For the next 10 iterations, NMAX is 60 and IL is 120.
- (3) Set NMAX to 80 and IL to 160 for iterations 31 through 50.
- (4) Take NMAX as 90 and IL as 180 for the next 10 iterations.
- (5) For iterations 61 through 70, NMAX is 100 and IL is 200.
- (6) Over the next 10 iterations, NMAX is 110 and IL is 220.
- (7) Starting with the 81st iteration, WCX and WSX are set to 0 and NMAX is 110 and IL is 220 through the 100th iteration.

(8) From iteration 101 through 110, NMAX is 130 and IL is 260.

(9) Over the last 10 iterations, NMAX is 150 and IL is 300.

Note that steps (7) through (9) utilize the alternate solution to the mapping equations (9) and (10) in Section II of Volume I of this report. The instructions which must be altered or removed are indicated in the program listing by parenthesis with the proper instruction enclosed.

The following input is required by CONFORM to conformally map the Laguna Madre, Mexico to Marsh Island, Louisiana region into a rectangle in the image plane. Note the fourth and fifth parameters on the first card image are only indicative of the final results. See Input and Output text for explanation of procedure used to obtain the mapping coefficients given as input to Program GRID.

C							C		
C	I N P U T D A T A						C		
C	1	47	40	150	1500.001		360.00	110.00	
C							C		
C	C O A S T L I N E C O O R D I N A T E S						C	S E A W A R D B O U N D A R Y C O O R D I N A T E S	
C							C		
C	000.00	035.00					000.00	002.00	
	005.60	040.00					007.50	005.00	
	010.50	044.80					016.00	010.00	
	018.00	051.00					021.50	014.50	
	028.00	059.00					028.00	019.00	
	040.00	066.80					036.00	023.00	
	050.50	073.00					045.00	028.00	
	056.50	076.50					054.00	032.00	
	063.00	082.00					060.00	036.00	
	070.00	093.00					066.00	040.00	
	074.00	102.00					077.00	046.00	
	076.50	108.50					085.00	051.00	
	079.00	116.00					089.00	055.00	
	082.50	127.00					095.00	064.00	
	088.00	137.80					104.00	076.00	
	095.00	146.00					110.00	084.00	
	106.00	154.00					112.00	089.00	
	121.00	162.00					113.50	095.00	
	136.00	167.00					114.50	101.00	
	153.00	168.30					117.50	108.00	
	158.00	168.00					121.00	112.00	
	161.50	167.30					127.00	116.00	
	166.00	168.80					139.00	121.00	
	171.00	169.00					153.00	123.50	
	183.00	168.00					165.00	123.00	
	197.00	166.00					179.00	119.00	
	214.00	165.00					193.00	115.00	
	230.00	166.00					213.00	104.00	
	242.00	167.00					229.00	092.00	
	250.00	166.70					244.00	080.00	
	253.40	167.20					257.00	071.00	
	257.00	169.50					267.00	066.00	
	265.00	169.00					276.00	062.00	
	280.00	166.00					289.00	056.00	
	291.00	163.00					298.00	049.00	
	296.00	159.30					307.00	042.00	
	298.50	159.90					318.00	035.00	
	303.00	159.00					333.00	027.00	
	314.00	153.00					347.00	020.00	
	323.00	148.00					360.00	014.00	
	328.00	142.00							
	331.00	137.20							
	335.50	129.20							
	342.50	121.00							
	349.50	115.00							
	352.50	113.00							

III. COMPUTER PROGRAM DOCUMENTATION FOR PROGRAM-GRID

1. Program Purpose.

The purpose of this program is to determine the grid point array in the stretched curvilinear shelf coordinate system and appropriate scale factors needed for program SSURGE. The detailed grid is needed in order for the user to read off depths from an appropriate bathymetric chart of the shelf region at grid locations.

2. Program Description.

The program is written in FORTRAN IV language. This program interfaces between Programs CONFORM and SSURGE. It is assumed that the conformal mapping of the storm surge region has been completed to the user's satisfaction. The program GRID takes, in part, as input, the transformation coefficients and determines computing grid information of scale factors, grid point locations, and, at each grid point, the orientation of the ξ -axis to the x -axis.

The program GRID is composed of

MAIN	Defines constants. Reads transformation coefficients outputted from CONFORM. Reads water depths along a line near center of grid from the seaward boundary to the coast. Computes grid point locations, scale factors (μ , ν , and F), and, at each grid point, $\cos \theta$ and $\sin \theta$. Writes computing grid information.
SUBROUTINE XUT	Writes information transferred into XUT.
SUBROUTINE SHCOR	Determines and writes grid point coordinates in x, y space and the distance in nautical miles between points.
SUBROUTINE TRAN	Computes the x and y coordinates of the transform-generated coastline and seaward boundary curve.
SUBROUTINE TRAN1	Computes $x(\xi, \eta)$ and $y(\xi, \eta)$.
SUBROUTINE TRAN2	Computes $\partial x / \partial \xi$, $\partial y / \partial \xi$ and $\theta = \tan^{-1}(\frac{\partial y / \partial \xi}{\partial x / \partial \xi})$.
SUBROUTINE CURV9	Contains the expansion curve $Y = Z + B(X)^C$ where A , B , and C are constants. The term Y is either S_p (units, nautical miles) or T (units, minutes). The term X is either S^* (units, nautical miles) or T^* (units, minutes). This subroutine computes Y and dY/dX given the coefficients and X .

- SUBROUTINE CURV1 - Determines the necessary parameters to compute an interpolatory spline under tension through a sequence of functional values contained in arrays X2 and Y2 .
- FUNCTION CURV2 - Interpolates the given curve, Y2 as a function of X2 , returning a value for y given x .
- SUBROUTINE CURV3 - Determines the necessary parameters to compute an interpolatory spline under tension through a sequence of functional values contained in arrays X2P and Y2P .
- FUNCTION CURV4 - Interpolates the given curve, Y2P as a function of X2P , returning a value for y given x .

3. Type of Computer.

The program GRID may be run on any computer with minimum core requirements of approximately 26K words (based on the present sample program appropriate to the Hurricane Carla surge simulation grid). GRID requires no auxiliary storage devices, peripheral devices, or magnetic tape input or output. No site-oriented computer plot routines are involved in the program. Approximately 25 minutes of machine time on a GE/635 is required for the sample program to determine the computing grid information. This time is based on the following pertinent program parameters:

- a) 150 transformation coefficients, B_n or C_n ;
- b) 121 evenly spaced values of ξ for determining the transform-generated coastline arclength as a function of ξ ;
- c) 51 evenly spaced values of η for determining the arc-length along a particular isoline of ξ as a function of η ;
- d) the computing grid of 47 ξ (or S*) lines and 15 η (or T*) lines;
- e) for determining the scale factor F , the area in x,y space of each quadrangle is approximated by using 4 evenly spaced increments between ξ isolines and 2 evenly spaced increments between η isolines.

For production runs, smaller sampling intervals might be required in b, c and especially, c .

4. Input Data.

Input data, other than constants defined in MAIN, are read in MAIN and are on IBM cards prepared according to the following list:

(1) Card 1

NMAX, NUMXI,	Number of mapping coefficients, number of ξ
NUMETA, DELSS,	lines + 2, number of η lines, ΔS^* in nautical
SSTRT, DELTT,	miles, first value of S^* in nautical miles,
ND, NS	ΔT^* in minutes, number of depths, number of
	points in format 3I4, 3F5.1, 2I4.

(2) Card 2

BETA BZRO	The value of β and B_0 from the conformal mapping solution in format 2E14.7.
-----------	--

(3) Card Group 3

COB, COC	The NMAX cards containing the Fourier-type transformation coefficients, B_n and C_n , in format 2E14.7.
----------	---

(4) Card Group 4

SY	Temporary storage for the ND values of the water depth (fathoms) along a line from the seaward boundary to the coast. This information is needed to evaluate the traveltime coordinate T.
----	---

5. Mathematical Procedures and Program Limitations.

Information concerning the expanding grid procedure and the relations transforming ξ, η to S^*, T^* space is presented in Volume I of this report. The user is required to know the coefficients of the expansion function

$$S_p = A + B(S^*)^C$$

for each region of the curve where S_p is arclength (nautical miles) along the transform-generated coastline. For the sample program, there are five regions of the expansion curve. Selecting $\Delta S^* = 6$ nautical miles, the number of ΔS^* intervals of each region and the value of $\partial S_p / \partial S^*$ at the end points of each region, we can determine the coefficients of each region from three simultaneous equations derived from the constraints:

For region I, 176 nautical miles $\leq S^* \leq 236$ nautical miles
(10 intervals of ΔS^*)

$$\frac{\partial S_p}{\partial S^*} = 2.6225 \quad \text{at } S^* = 176 \text{ nautical miles}$$

$$\frac{\partial S_p}{\partial S^*} = 1.5 \quad \text{at } S^* = 236 \text{ nautical miles}$$

$$S_p = S_p \quad \text{at } S^* = 236 \text{ nautical miles}$$

For region II, 236 nautical miles $\leq S^* \leq 260$ nautical miles
(4 intervals of ΔS^*)

$$\frac{\partial S_p}{\partial S^*} = 1.5 \quad \text{at } S^* = 236 \text{ nautical miles}$$

$$\frac{\partial S_p}{\partial S^*} = 1.5 \quad \text{at } S^* = 260 \text{ nautical miles}$$

$$S_p = S_p \quad \text{at } S^* = 260 \text{ nautical miles}$$

For region III, 260 nautical miles $\leq S^* \leq 302$ nautical miles
(7 intervals of ΔS^*)

$$\frac{\partial S_p}{\partial S^*} = 1.5 \quad \text{at } S^* = 260 \text{ nautical miles}$$

$$\frac{\partial S_p}{\partial S^*} = 1.0 \quad \text{at } S^* = 302 \text{ nautical miles}$$

$$S_p = 302 \text{ nautical miles at } S^* = 302 \text{ nautical miles}$$

For region IV, 302 nautical miles $\leq S^* \leq 356$ nautical miles
(9 intervals of ΔS^*)

$$\frac{\partial S_p}{\partial S^*} = 1.0 \quad \text{at } S^* = 302 \text{ nautical miles}$$

$$\frac{\partial S_p}{\partial S^*} = 1.0 \quad \text{at } S^* = 356 \text{ nautical miles}$$

$$S_p = 302 \text{ nautical miles at } S^* = 302 \text{ nautical miles}$$

For region V, 356 nautical miles $\leq S^* \leq$ 452 nautical miles
(16 intervals of ΔS^*)

$$\frac{\partial S_p}{\partial S^*} = 1.0 \quad \text{at } S^* = 356 \text{ nautical miles}$$

$$\frac{\partial S_p}{\partial S^*} = 2.7 \quad \text{at } S^* = 452 \text{ nautical miles}$$

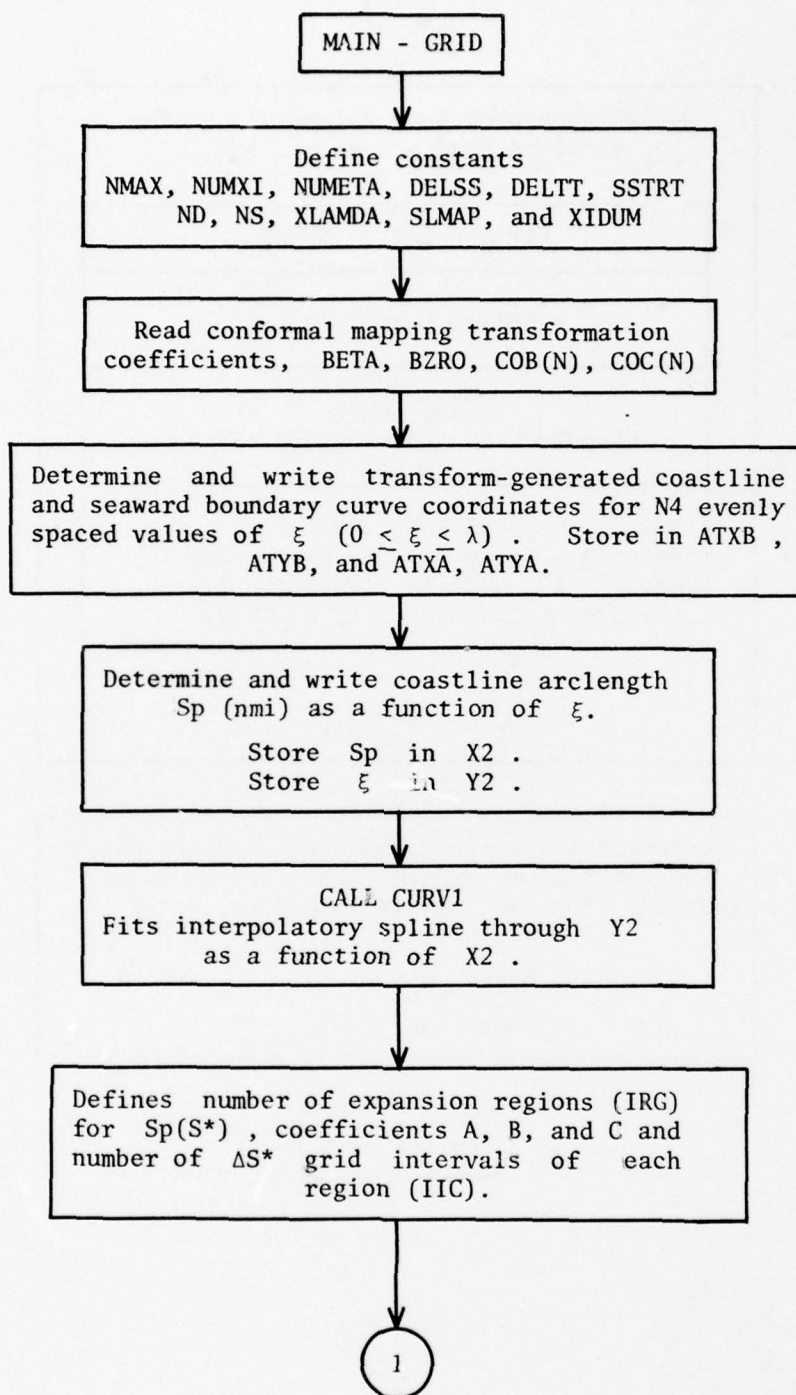
$$S_p = 356 \text{ nautical miles at } S^* = 356 \text{ nautical miles}$$

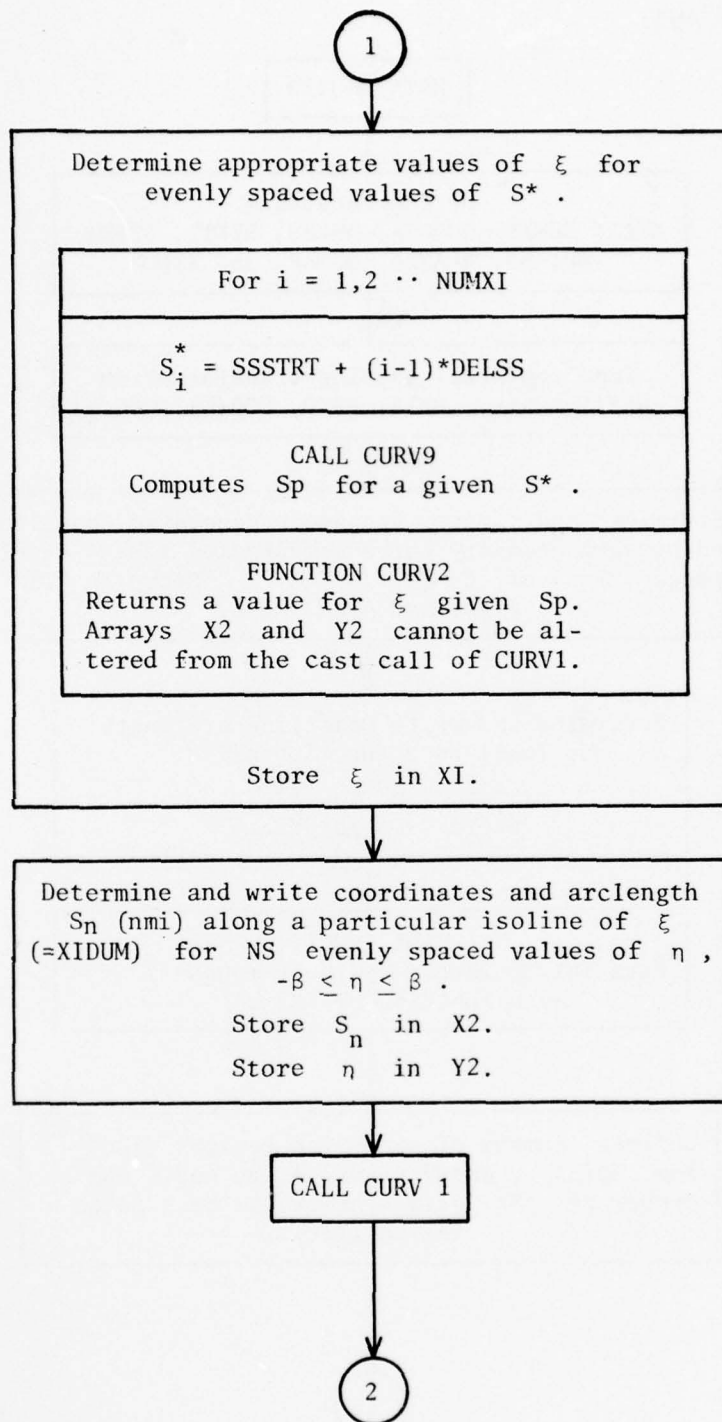
A similar procedure is followed for the expansion function

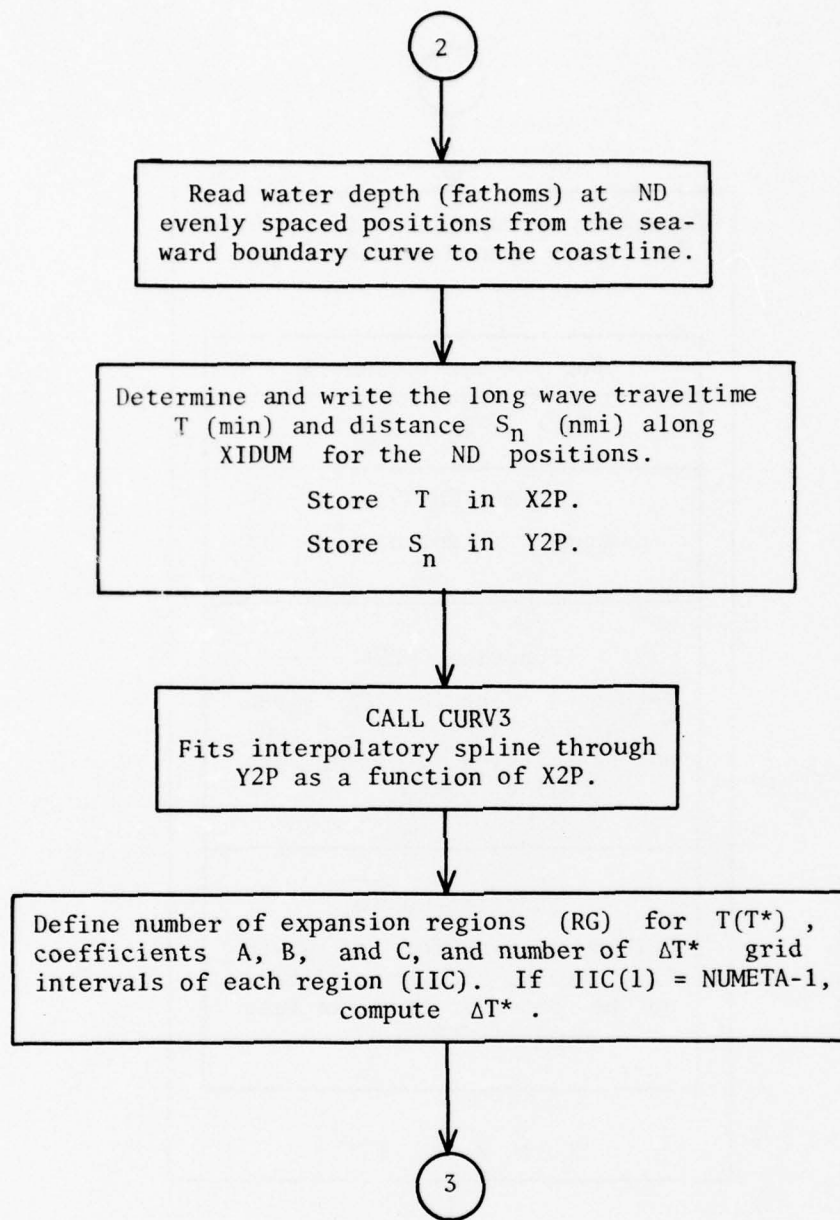
$$T = A + B(T^*)^C$$

where T is the long wave traveltime (minutes) along the particular isoline of ξ . The program assumes that there are, at most, two regions of the expansion curve with the second region being $\Delta T = \Delta T^*$. The expansion coefficients are determined by the program. If the user desires only one region (i.e., $T = T^*$ and $\Delta T^* =$ total long wave traveltime-number of η grid intervals), the program computes ΔT^* .

6. Flow Chart.







3

Determine appropriate values of η
for evenly spaced values of T^* .

For $j = 1, 2 \dots \text{NUMETA}$

$$T_j^* = (j-1) \times \text{DELTT}$$

CALL CURV9

Computes T for a given T^*

Function CURV4

Returns a value for S_n given
 T . Arrays $X2P$ and $Y2P$ can-
not be altered from the last
call of CURV3.

Function CURV2

Returns a value for η given
 S_n . Arrays $X2$ and $Y2$ can-
not be altered from the last
call of CURV1.

Store η in ETA .

The values of ξ and η are now known.
Determine the computing grid data.

4

4

CALL SHRCOR
Determines and writes the grid point coordinates
in x,y space and the distance (nmi) between
grid points.

Store x coordinate in X and
Store y coordinate in Y for
i = 2,3 .. NUMXI-1
j = 1,2 .. NUMETA.

Determine and write scale factor μ (units
x,y space-nmi).

Store μ in SX for i=1,2 .. NUMXI-2.

Determine and write scale factor ν (units of
x,y space-time minutes).

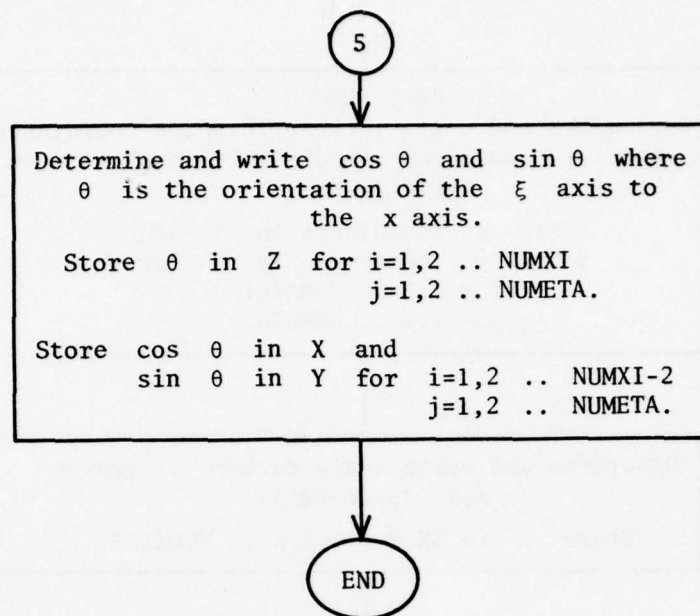
Store ν in SY for j=1,2 .. NUMETA.

Determine and write dimensionless scale factor F.
Compute area in x,y plane of each quadrangle
subdivided into IQAD intervals between ξ
lines and JQUAD intervals between η lines.

Store area in X for i=1,2 .. NUMXI-1
j=1,2 .. NUMETA.

Store F in Y for i=1,2 .. NUMXI-2.
j=1,2 .. NUMETA.

5



7. Description of Terms.

Arrays

All arrays except COB, COC, XI and ETA are reused throughout the program. The user is cautioned to consult each major program division for assessment of array contents.

X,Y,Z	Dimensioned NUMXI \times NUMETA.
X2,Y2 X2P,Y2P ATXA,ATYA ATXB,ATYB	Dimensioned the larger of N4, NS, ND, or IQUAD.
A, B, C IIC	Dimensioned IRG (the number of $Sp(S^*)$ expansion regions).
SX	Dimensioned NUMXI-2.
SY	Dimensioned NUMETA.
COB	Dimensioned NMAX. Contains the conformal mapping transformation coefficients, B_n .
COC	Dimensioned NMAX. Contains the conformal mapping transformation coefficients, C_n .
XI	Dimensioned NUMXI. Contains the values of ξ for determining the computing grid data.
ETA	Dimensioned NUMETA. Contains the values of η for determining the computing grid data.

Constants

NMAX	Number of conformal mapping transformation coefficients, B_n or C_n .
NUMXI	Number of computing grid ξ lines. With respect to the computing grid in Program SSURGE, there is an extra ξ line at each lateral end. This requirement results from the averaging procedure used in determining the grid data.
NUMETA	Number of computing grid η lines. This is the same number as in Program SSURGE.

DELSS	<p>The value in nautical miles of ΔS^* . This corresponds to DXI in Program SSURGE.</p> <p>Since in SSURGE the product, $\mu \Delta S^*$, is always computed in the surge equations, we determine DXI in meters such that μ values are dimensionless, i.e.,</p> $DXI = 1852 \frac{m}{nmi} \times \Delta S^* \text{ nmi} \times \left[SLMAP \frac{nmi}{x,y \text{ unit}} \times \mu \text{ unit} \right]$
DELTT	<p>The value in minutes at ΔT^* . This corresponds to DETA in Program SSURGE.</p> <p>Since in SSURGE, the product, $v \Delta T^*$, is always computed in the surge equations, we determine DETA in meters such that v values are dimensionless, i.e.,</p> $DETA = 1852 \frac{m}{nmi} \times \Delta T^* \text{ min} \times \left[SLMAP \frac{nmi}{x,y \text{ unit}} \times v \text{ unit} \right]$
SSSTRT	The first value of S^* in nautical miles.
ND	The number of water depths (fathoms) inputed from the seaward boundary to the coast for determining distance as a function of long wave traveltime.
NS	The number of points along XIDUM for determining η as a function of arclength S_n .
XLAMDA	Horizontal extent of the mapped region in units of x,y space.
XIDUM	The particular value of ξ used in determining $\eta(S_n)$.
SLMAP	The chart scale relating distance in nautical miles to distance in x,y units (i.e., nmi is equivalent to 51 units of length in x,y space).
G	Acceleration due to gravity ($\text{feet} \cdot \text{s}^{-2}$).
N4	The number of points used in determining ξ as a function of arclength S_p .
IRG	The number of expansion regions of $SP(S^*)$ or $t(T^*)$.

IQUAD The area in x,y space of each grid quadrangle is sub-
 and divided into IQUAD intervals between ξ lines and
 JQUAD JQUAD intervals between η lines.

8. Input and Output.

The first card input to Program GRID gives the number of conformal transformation coefficients NMAX, the number of ξ lines NUMXI, the number of η lines NUMETA, ΔS^* in nautical miles DELSS, the first value of S^* in nautical miles SSSTRT, ΔT^* in minutes DELTT, the number of water depths ND, and the number of points US used to establish $\eta = \eta(S_n)$.

The second card gives β and B_0 and the next 150 cards give the mapping coefficients B_n and C_n . These 151 cards are the punched output from Program CONFORM.

The remaining 31 cards are the depths picked off a bathymetric chart of the northwestern Gulf of Mexico. These depths are on a constant ξ -line selected by the user.

Expansion coefficients, provided by the user, appear as statements within the program after format 135.

The reader must refer to Section III of Volume I of this report for an explanation of the parameters associated with the stretched shelf coordinate system for the Hurricane Carla surge simulation.

Output from GRID consists of the transform-generated coastline and seaward boundary coordinates, the transform-generated arclengths along the coastline and seaward boundary, and for each of the five sections, $\partial Sp / \partial S^*$, S^* , Sp , and ξ are listed. Additionally, the transform-generated arclengths at values of η for evenly spaced increments of T^* and at η values for constant increments of T along the chosen ξ -line, the η values along the specified ξ -line such that ΔT^* is constant, and the traveltime and depths along the constant ξ -line are printed.

The following output is required by Program SSURGE for simulating the Hurricane Carla surge. This includes the x,y coordinates of the grid intersections, the scale factors μ and ν related to the transformation of ξ to S^* and η to T^* , respectively, the scale factor F , and the sines and cosines of theta giving the orientation of the ξ -axis to the x -axis. The program listing indicates when these may be punched or written on tape or disk for convenient input to SSURGE.

```

C
C      INPUT DATA
C 150 47 15 6.0176.0 8.0 31 51
C
2.1109529E-01 9.5078648E-01
-4.3493873E-01 -6.8176833E-01
-3.1662011E-01 1.5427266E-01
1.2422513E-01 -1.1738220E-01
-5.0636502E-01 -1.4470718E-02
1.6711864E-01 -1.9216334E-01
-3.5976884E-01 -6.7330628E-01
1.4192800E-01 1.3667185E-01
-1.1794944E-01 -3.0913591E-01
4.1190876E-01 1.3357793E-01
-3.7759354E-01 4.8326302E-03
7.9716016E-02 5.3212199E-02
-1.0800307E-01 1.6050344E-01
-1.2900839E-02 1.5596876E-01
-5.5636576E-02 1.4032560E-01
-1.3795311E-02 -6.3873108E-02
-3.5084819E-02 9.6181509E-02
6.6049823E-03 -4.1274375E-02
-1.4301171E-02 2.1339555E-02
9.3927601E-03 -2.2866277E-02
-1.1320465E-02 2.3924600E-02
-1.0776871E-03 -2.2690670E-03
-1.2749315E-02 6.3207555E-03
4.0667667E-03 1.4115754E-03
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9.1903310E-04 3.3485054E-04
-1.1438246E-03 -1.0357530E-04
3.7952317E-04 1.7815754E-04
-6.7125224E-04 9.4878230E-05
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-5.8352881E-04 1.4706647E-04
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-2.5129644E-04 3.0412098E-04
-1.0435642E-05 -2.4449992E-04
1.0222874E-05 2.3269536E-04
-8.8439003E-06 -1.5700862E-04
-1.2788127E-05 1.5418616E-04
-2.6134267E-05 -9.3255390E-05
-1.4402552E-05 1.0334477E-04
-5.0758231E-06 -5.2779377E-05
-2.3834472E-05 3.2466107E-05
2.6851103E-05 -2.6723894E-06
-4.3115519E-05 -2.0363452E-06
2.6351927E-05 1.1422553E-05
-2.3699234E-05 2.3080753E-06
1.0604752E-05 -2.8166598E-06
-1.1909960E-05 5.3967162E-06
7.9691199E-06 -7.3427355E-07
-9.4350325E-06 3.0569014E-06
3.5921445E-06 -2.8028600E-06
-3.1637865E-06 5.2027666E-06
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-3.1561570E-06 2.9766627E-06
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1.1309517E-06 -7.1666702E-07
-6.1223962E-07 1.4500429E-06
-1.8451712E-07 -1.1197107E-06
-3.3654205E-07 1.1018565E-06
8.9384915E-08 -4.5424002E-07
-3.0120364E-07 5.2354470E-07
-3.6734064E-08 -3.5625709E-07
-1.4140850E-07 4.2440585E-07
7.3883089E-08 -1.2844558E-07
-3.2262466E-07 5.8860751E-08
2.7314736E-07 1.0023264E-07
-2.8025699E-07 -3.2327544E-08
1.2341097E-07 1.0872806E-08
-9.4987154E-08 8.2818260E-08
1.9075643E-08 -6.2256573E-08
-3.8559006E-08 7.6237884E-08
1.2275724E-08 -4.7253453E-08
-2.2807855E-08 5.9522217E-08
-4.7725860E-09 -3.9176467E-08
-1.3059312E-08 4.0413841E-08
1.3466543E-09 -1.2140226E-08
-3.1784570E-09 -4.0184008E-11
2.6290277E-09 1.2313703E-08
-2.1406560E-09 -5.5426578E-09
1.8588775E-09 6.3954900E-09
-3.7924576E-09 -6.9248154E-09
1.9027985E-09 6.0566206E-09
-9.6309918E-10 -2.9732490E-09
-1.5450322E-09 1.5365158E-09
1.7949878E-09 3.7305565E-10
-2.4545629E-09 -5.5504161E-10
1.9894453E-09 9.3920530E-10
-2.0184501E-09 -6.3272567E-10
1.3540433E-09 7.4956038E-10
-1.1897658E-09 -2.6100463E-10
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-6.2031906E-14 3.0256047E-15
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95.
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25.
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22.
21.
21.
20.7
18.5
17.5
16.
15.3
14.5
13.5
12.7
11.
11.
11.
10.5
9.
7.5
4.5
2.

```

IV. COMPUTER PROGRAM DOCUMENTATION FOR PROGRAM-SSURGE

1. Program Purpose.

The purpose of the program is to numerically simulate the storm surge in orthogonal curvilinear coordinates with the vertically integrated form of the quasi-linear long-wave equations.

2. Program Description.

The program is written in FORTRAN IV language. It is assumed that the conformal mapping of the region under investigation has been completed. The transformation coefficients for three regions of the continental shelf of the Gulf of Mexico and two regions of the eastern seaboard are provided in Appendixes A and E in Volume I of this report.

An interfacing program is required which inputs the coefficients and generates a curvilinear computing grid to the user's satisfaction. The output from the program (and, in part, also the input to SSURGE) must be the scale factors, grid point locations, and, at each grid point, the orientation of the ξ -axis to the x-axis.

The Program SSURGE is composed of:

MAIN	Defines constants and interfaces the subroutines.
SUBROUTINE ZERO	Initializes all arrays to zero.
SUBROUTINE FIELD	Reads data and writes the water depth field relative to mean sea level, the wind field parameters and the storm positions.
SUBROUTINE WINDF	Calculates the wind and atmospheric pressure fields.
SUBROUTINE ELEV	Computes the water level anomaly, H .
SUBROUTINE FLUX	Computes transports, Q_{S*} and Q_{T*} .
SUBROUTINE DRAW1	Outputs H and vertically averaged water velocities, Q_{S*}/\bar{D} and Q_{T*}/\bar{D} , at hourly time intervals and saves the water level anomaly at prescribed grid locations for output at program completion.

SUBROUTINE METER Calculates and saves the vertically averaged water velocities at prescribed grid locations for output at program completion.

SUBROUTINE HUV Outputs the saved information of the simulated hydrographs, simulated current meters, and observed water levels at program completion.

3. Type of Computer.

The program SSURGE may be run on any computer with minimum core requirements of approximately 30K words of memory (based on the present sample program appropriate to the Hurricane Carla surge simulation). The program has been executed successfully on the IBM 360, CDC/6600 and 7600, and GE/635. The present sample program requires no auxiliary storage devices, peripheral devices or magnetic tape input or output. No site-dependent computer plot routines are involved in the program. Approximately 14.4 minutes of machine time on a GE/635 is required for the sample program to complete 66 hours of surge simulation.

4. Input Data.

Input data, other than constants defined in MAIN, are read in SUBROUTINE FIELD. These data are on cards prepared according to the following list.

(1) Card 1

NT1 - Number of cards (max. 50) containing on each TIM, ROT, RAD, VRMAX and PZRO (format I5).

(2) Card Group 2

NT1 cards with each card containing values of

- a) TIM The time in hours at which the hurricane wind and atmospheric pressure parameters are recorded (format F10.1).
- b) ROT The angle in degrees between the direction the storm is moving and the region of maximum winds (format F10.1).
- c) RAD The distance in nautical miles from the storm center to the region of maximum winds (format F10.1).

- d) VRMAX Maximum observed windspeed in knots (format F10.1).
- e) PZRO Atmospheric pressure in millibars of the storm center (format F10.1).

(3) Card 3

NT2 - Number of cards (max.150) containing on each TIMPOS, XPOS and YPOS (format 15).

(4) Card Group 4

NT2 cards with each card containing values of

- a) TIMPOS The time in hours at which the hurricane position is recorded (format F10.1).
- b) XPOS The x-coordinate in units of x,y space of the hurricane center (format F10.1).
- c) YPOS The y-coordinate in units of x,y space of the hurricane center (format F10.1).

(5) Card Group 5

GRID2 The fluid depth in fathoms relative to mean sea level along each column, $i=1,2..IM$, is read with a nested do-loop for $j=1,2..JM$ (format 11F7.2). The program will zero those values for even $i+j$ prior to computations. The depth data are positive numbers which the program converts to negative values (in meters) to be consistent with the coordinate system.

(6) Card Group 6

S The values of the dimensionless scale factor relating the (x,y) plane to the (ξ,η) plane are read along each column, $i=1,2..IM$, with a nested do-loop for $j=1,2..JM$ (format 5E14.7).

(7) Card Group 7

DSDXI The values of the dimensionless scale factor, μ , transforming ξ to S^* are read with one value per card for $i=1,2..IM$ (format E14.7).

(8) Card Group 8

DTDET Values of the dimensionless scale factor v transforming η to T^* are read with one value per card for $j=1,2..JM$ (format 2X,E14.7).

(9) Card Group 9

HOBS1 The values of the observed hourly water level in feet at grid location (IH1, JH1) are read with 19 values per card in format F4.1.

(10) Card Groups 10 through 14

HOBXk The values of the observed hourly water level in feet at grid location (IHk, JHk) are read sequentially with the same format as above.

(11) Card Group 15

XX, YY The paired x, y coordinates (units in x, y space) of the computational grid points are read along each column, $i=1,2..IM$, with a nested do-loop for $j=1,2..JM$ (format 10F7.2).

(12) Card Group 16

COSG, SING The paired values of the cosine θ and sine θ where θ is the angle between the ξ and x axis are read along each column, $i=1,2..IM$, with a nested do-loop for $j=1,2..JM$ (format 10F8.5).

A computer printout of the sample program and data cards are given later in this section.

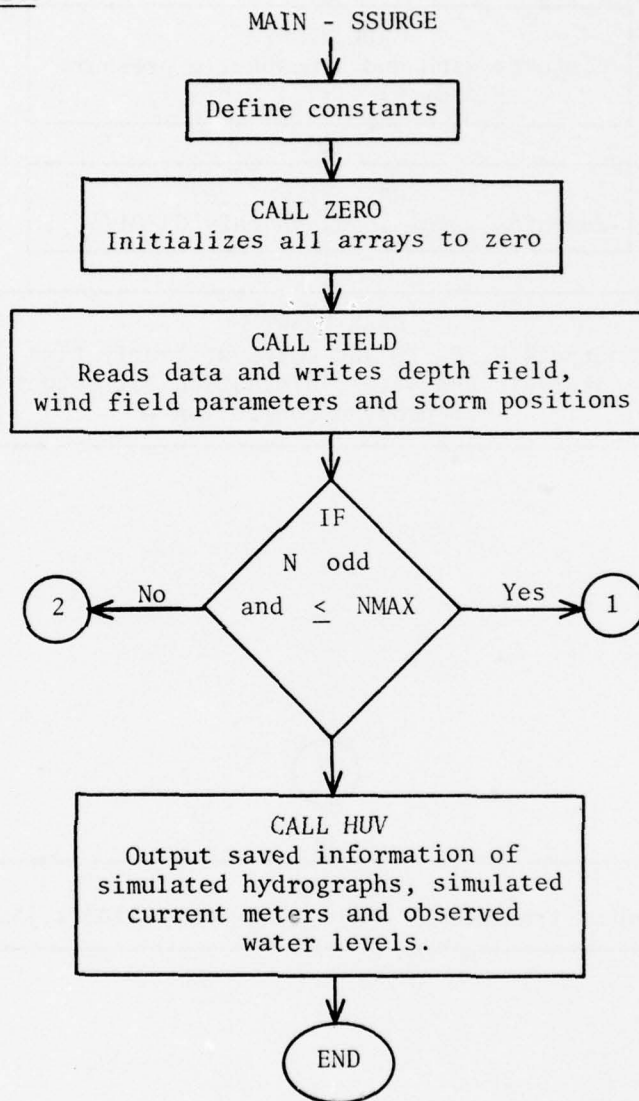
5. Mathematical Procedures and Program Limitations.

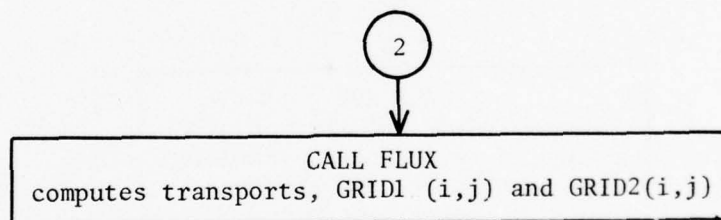
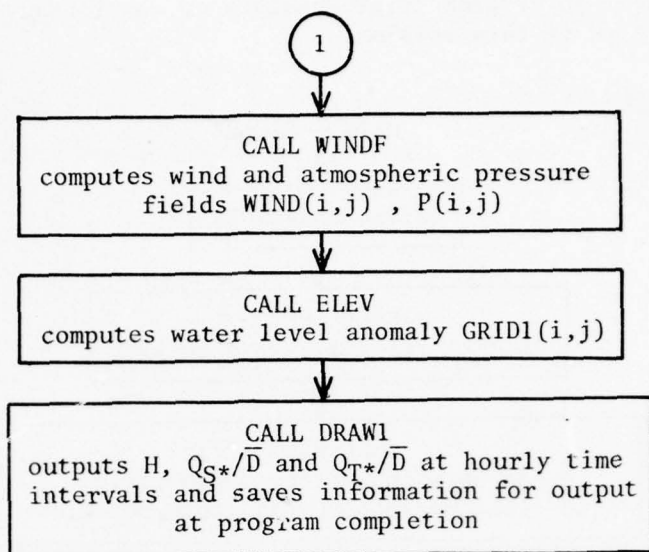
The storm surge equations, solutions, and algorithms are described in the text of Volume I of this report.

Basically, the model utilizes a centered difference, leapfrog analog of the vertically integrated, quasi-linear form of the long-wave equations. The algorithm treats the time dependency explicitly and employs a computing lattice in which the transports, Q_{S^*} and Q_{T^*} , are computed at the same location but are staggered in time and space with respect to the water

level anomaly. The program assumes that seabed scouring does not occur. No program error messages or consistency checks are incorporated in this version.

6. Flow Chart.





7. Glossary and Description of Terms.

Arrays

GRID1	Dimensioned $IM \times JM$. Contains H values in meters at odd $i+j$ and Q_{S^*} in meters squared per second at even $i+j$.
GRID2	Dimensioned $IM \times JM$. Contains fluid depth values, D_o , in meters at odd $i+j$ and Q_{T^*} in meters squared per second at even $i+j$.
S	Dimensioned $IM \times JM$. Contains <u>dimensionless</u> scale factor, F , determined from the conformal mapping of (x,y) space to (ξ,η) space.
DSDXI	Dimensioned IM . Contains the dimensionless scale factor, μ , transforming ξ to S^* .
DTDET	Dimensioned JM . Contains dimensionless scale factor, ν , transforming η to T^* .
XX	Dimensioned $IM \times JM$. Contains the x-coordinate in units of (x,y) space of the grid point locations.
YY	Dimensioned $IM \times JM$. Contains the y-coordinate in units of (x,y) space of the grid point locations.
COSG	Dimensioned $IM \times JM$. Contains cosine values of θ relating the orientation of the ξ -axis to the x-axis at the computational grid points.
SING	Dimensioned $IM \times JM$. Contains sine value of θ relating the orientation of the ξ -axis to the x-axis at the computational grid points.
WIND	Dimensioned $IM + 1 \times JM$. Contains values of the windspeed in meters per second. At a transport computational grid point (i,j) , the S^* -component is stored in WIND at (i,j) and the T^* -component is stored at $(i+1,j)$.
P	Dimensioned $IM \times JM$. Contains values of H_B (the hydrostatic elevation in meters of the sea surface corresponding to the atmospheric pressure anomaly) and stored at odd $i+j$.
HOBSk k=1,2..6	Each array is dimensioned 67. Contains the observed hourly water levels in meters at grid locations (IH_k , JH_k).

HYDk k=1,2..6	Each array is dimensioned 300. Contains values of the computed water level H in meters at grid locations (I_{Hk} , J_{Hk}).
UCMk k=1,2..6	Each array is dimensioned 300. Contains values of the vertically averaged water velocity, Q_{S*}/\bar{D} , in meters per second at grid location (I_{Tk} , J_{Tk}).
VC Mk k=1,2..6	Each array is dimensioned 300. Contains values of the vertically averaged water velocity, Q_{T*}/\bar{D} , in meters per second at grid location (I_{Tk} , J_{Tk}).
TIM	Dimensioned 50. Contains the time in hours at which the wind and atmospheric pressure field parameters (ROT, RAD, VRMAX and PZRO) are recorded.
ROT	Dimensioned 50. Contains the angle in degrees between the direction the storm is moving and the region of maximum winds.
RAD	Dimensioned 50. Contains the distance in nautical miles from the storm center to the region of maximum winds.
VRMAX	Dimensioned 50. Contains the maximum observed windspeed in knots.
PZRO	Dimensioned 50. Contains the atmospheric pressure in millibars of the storm center.
TIMPOS	Dimensioned 150. Contains the time in hours at which the storm position is recorded.
XPOS	Dimensioned 150. Contains the x-coordinate in units of (x,y) space of the storm center.
YPOS	Dimensioned 150. Contains the y-coordinate in units of (x,y) space of the storm center.

Constants

IM	Number of grid points in the S^* direction.
JM	Number of grid points in the T^* direction.
NMAX	Maximum number of time steps.

INC	Number of time steps between saving of surge results in HYDk, UCMk and VCMk. INC must be an even integer number.
DXI	Grid increment in meters in the S* direction.
DETA	Grid increment in units of meters in the T* direction. The units of DTDET·DETA (that is, $v \cdot \Delta T^*$) are in meters.
DELT	Time increment in seconds. DELT must be less than that required for numerical stability and, also, be an even integer multiple of 60 minutes.
GRAV	Acceleration due to gravity (≈ 9.8 meters per second squared).
F	Dimensionless seabed drag coefficient (≈ 0.0025).
IHK, JHK k=1,2..6	Grid point location for saving the computed water level. The sum of the indexes must be odd. Index IHk cannot exceed IM. Index JHK cannot exceed JM.
ITk, JTk k=1,2..6	Grid point location for saving the vertically averaged water velocities. The sum of the indexes must be even. Index ITk cannot exceed IM. Index JTk cannot exceed JM-1.
CORIO	Coriolis parameter ($\approx 6.70875 \times 10^{-5}$ second ⁻¹) for latitude 27° 23.232' N.
PHI	Wind ingress angle in units of degrees.
PINF	Far field atmospheric pressure in millibars (≈ 1016 millibars).

Comments

1. A symmetric analytical hurricane wind field representation as given by C. Jelesnianski (1965, A numerical calculation of storm tides induced by a tropical storm impinging on a continental shelf, *Mon. Wea. Rev.*, 94, 379-394) is employed in the surge model).
2. The wind stress coefficients, K_1 and K_2 , are 1.1×10^{-6} and 2.5×10^{-6} and are defined in SUBROUTINE FLUX.
3. Constants YRANGE, THIT, XHIT and YHIT are not used in this program version.

8. Input and Output.

Data statements in Program SSURGE establish the number of computational points, number of time steps, output interval, values of the grid and time steps, acceleration due to gravity, bottom stress coefficient, and locations of the simulated hydrographs and current meters, and the Coriolis parameter corresponding to latitude $27^{\circ} 23.232' N$.

Card input provides the number (NT1) of hurricane description sets, followed by NT1 cards giving the time (in hours after start of computations) and the three required storm parameters. These are succeeded by one card giving the number (NT2) of hurricane positions to be used, followed by NT2 cards providing the time and storm center positions in the original arbitrary Cartesian grid (see Volume I of this report). NT1 need not be equal to NT2, nor must the observed storm parameters and positions coincide in time.

For the Carla surge computations, the hurricane characteristics are stipulated at 6-hour intervals for the first 18 hours and at 3-hour intervals for the remainder of the 66-hour prototype time simulation. Note the radius to maximum winds are in *nautical miles*, the maximum winds are in *knots*, and the central pressures are in *millibars*. Due to the erratic movement of Hurricane Carla, the coordinates of the center of the storm are specified at hourly intervals, except for a single 6-hour interval spanning the end of the simulation. These coordinates are specified in *x,y* space (100 units = 219 kilometers).

The depth field, in *fathoms*, is introduced followed by the array of scale factors, *S*. The array of scale factors, DSDXI (an alias for μ) is read along the specified row and the scale factor array DTDET (an alias for ν) is specified along the chosen column.

The following six arrays are the observed hourly water levels (in feet) from Padre Island (HOBS1), Aransas Pass (HOBS2), Port O'Connor (HOBS 3), Pleasure Pier, Galveston (HOBS4), Mud Bayou (HOBS5), and Sabine Pass (HOBS6). These data are not necessary for any phase of the surge calculations and may be omitted.

The last two arrays input to SSURGE give the coordinates (XX,YY) of the grid points in units of *x,y* space, and the sines and cosines of theta at the computational points.

All input not in the MKS system of units is converted internally to the MKS system.

The storm parameters, hurricane center coordinates, and depth field are printed out immediately following input. At hourly time intervals, the water level anomalies and the depth averaged velocity component fields are printed. The six simulated hydrographs and current meters are printed out with their positions and the corresponding observed water levels at the completion of the surge simulation.

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The following data are required for the Hurricane Carla surge simulation. The reader is referred to the documentation of Program GRID for definition of the scale factors, grid point coordinates, and the sines and cosines of theta.

21	HURRICANE CARLA STORM PARAMETERS			
0.	60.	23.	90.	949.
6.	35.	22.	95.	943.
12.	65.	21.	100.	940.
18.	65.	24.	100.	937.
21.	60.	23.	100.	937.
24.	80.	22.	100.	937.
27.	65.	25.	100.	937.
30.	80.	27.	100.	936.
33.	150.	19.	100.	936.
36.	15.	21.	100.	936.
39.	15.	20.	100.	937.
42.	65.	22.	100.	937.

937.
938.
938.
939.
940.
942.
943.
945.
947.

100.
100.
95.
90.
70.
55.
55.
50.
55.

45.	23.	26.
48.	65.	28.
51.	105.	28.
54.	160.	33.
57.	145.	62.
60.	158.	98.
63.	176.	142.
66.	140.	167.
69.	117.	200.

HURRICANE CARLA TRACK

62

0.	249.7	-82.1
1.	247.9	-75.3
2.	245.4	-68.5
3.	243.1	-61.0
4.	238.1	-53.1
5.	232.8	-50.0
6.	225.3	-44.3
7.	219.0	-37.7
8.	213.5	-32.0
9.	208.9	-26.5
10.	204.8	-21.2
11.	202.2	-12.6
12.	199.2	-8.1
13.	191.7	-6.2
14.	188.0	-4.1
15.	188.0	-1.0
16.	188.9	3.1
17.	189.0	9.0
18.	191.0	13.4

19.	192.1	18.5
20.	192.1	25.0
21.	191.9	31.0
22.	190.2	38.0
23.	188.5	43.8
24.	182.7	48.2
25.	181.1	51.3
26.	181.3	54.9
27.	184.0	61.2
28.	186.0	65.0
29.	186.8	74.0
30.	182.3	81.0
31.	177.5	88.7
32.	172.0	93.3
33.	162.4	92.4
34.	155.6	93.2
35.	152.7	95.7
36.	152.8	98.1
37.	154.3	103.1
38.	156.3	107.1
39.	158.9	112.8
40.	158.0	121.0
41.	152.2	131.3
42.	145.0	134.9
43.	141.6	130.2
44.	145.1	126.8
45.	148.8	129.4
46.	151.9	136.7
47.	155.5	146.3
48.	157.0	152.2
49.	157.4	158.2

10.70	8.50	6.00	1.50	33.00	28.00	23.50	19.00	16.50	14.00	12.00
108.00	60.00	47.00	36.00	32.00	27.00	22.00	19.00	16.00	14.00	12.00
10.50	8.00	6.00	1.50	31.00	27.00	22.00	17.50	15.70	13.00	11.70
109.00	61.00	47.00	37.50	30.00	25.00	21.50	18.00	15.00	13.50	11.50
10.00	8.00	6.00	1.50	26.50	22.50	20.00	16.00	14.00	13.00	11.50
102.00	61.00	36.00	36.00	24.00	21.00	17.50	15.00	13.70	12.70	11.50
9.50	8.00	6.00	1.50	22.50	20.00	17.00	14.00	12.50	12.00	11.50
108.00	60.00	40.00	35.00	21.50	18.00	16.00	13.70	13.00	11.50	11.00
9.00	7.70	5.50	1.30	21.50	18.00	16.00	13.50	12.50	11.50	10.50
110.00	55.00	35.00	23.00	21.00	17.50	15.50	14.00	12.00	11.50	11.00
11.00	7.70	5.50	1.30	20.50	16.50	15.00	14.50	14.00	11.00	10.00
102.00	36.00	31.00	27.50	20.50	17.50	15.70	15.70	14.00	11.00	10.00
11.00	7.70	5.50	1.30	19.00	18.00	16.00	15.00	14.00	10.50	10.00
110.00	35.00	31.00	25.00	18.50	18.00	16.00	15.00	14.00	10.50	10.00
9.50	8.00	6.00	1.30	19.00	18.50	16.00	15.00	13.50	12.00	10.00
115.00	34.50	29.00	25.00	19.00	18.50	16.00	15.00	13.50	12.00	10.00
9.00	8.00	6.00	1.30	18.50	18.00	16.00	15.00	14.00	11.00	10.00
100.00	34.00	28.00	24.00	18.00	17.50	15.50	14.00	12.00	11.50	11.00
8.50	7.50	5.50	1.30	18.00	17.50	15.50	14.00	12.00	11.50	11.00
100.00	34.00	27.00	24.00	17.50	17.50	15.50	14.00	12.00	11.50	11.00
8.70	7.00	5.50	1.30	17.00	16.50	15.00	14.50	14.00	11.00	10.00
100.00	35.00	27.00	24.00	16.50	16.50	15.00	14.50	14.00	11.00	10.00
8.50	7.00	5.50	1.30	16.00	15.70	15.70	15.70	14.00	11.00	10.00
100.00	36.00	27.00	24.00	15.00	18.00	16.00	15.00	13.00	10.50	10.00
8.70	7.50	5.50	1.20	18.50	18.00	16.00	15.00	14.00	10.50	10.00
102.00	34.00	26.50	22.00	18.50	18.00	16.00	15.00	14.00	10.50	10.00
8.00	7.30	5.50	1.20	19.00	18.50	16.00	15.00	13.50	12.00	10.00
100.00	35.00	27.00	23.00	19.00	18.50	16.00	15.00	13.50	12.00	10.00
9.00	7.30	5.00	1.20	19.00	18.50	16.00	15.00	13.50	12.00	10.00
100.00	36.00	27.00	22.00	19.00	18.50	16.00	15.00	13.50	12.00	10.00
7.00	6.20	4.00	1.00							

100.00	30.00	26.70	21.00	21.00	18.00	16.00	15.00	13.00	11.50	11.00
10.00	7.00	4.00	1.20							
95.00	32.00	26.00	21.00	20.50	17.00	15.00	14.20	12.00	11.00	11.00
9.00	8.00	5.00	1.20							
100.00	31.00	26.00	21.00	19.00	17.00	15.00	14.00	11.50	10.50	10.50
9.00	8.00	5.50	1.20							
95.00	31.00	24.50	21.50	19.00	17.00	15.00	12.50	11.00	9.00	10.50
9.00	7.70	5.70	1.20							
100.00	31.50	24.00	21.50	18.50	16.00	14.50	11.50	11.00	9.00	9.50
9.00	7.50	5.70	1.20							
90.00	31.00	24.00	21.50	18.50	15.00	13.00	10.00	11.00	9.00	9.00
9.00	7.50	5.40	1.20							
90.00	31.00	26.00	21.00	18.00	14.00	13.00	10.00	10.50	9.00	9.00
9.00	7.50	5.00	1.20							
90.00	32.00	26.00	21.00	18.00	15.50	14.00	11.00	8.50	8.70	8.70
8.50	7.00	5.00	1.20							
100.00	33.00	26.50	21.50	17.50	15.00	13.50	11.00	6.50	8.50	8.50
8.00	7.00	5.20	1.20							
105.00	37.00	27.00	21.50	17.00	14.00	13.00	11.00	7.50	7.50	7.50
8.00	7.00	5.30	1.20							
95.00	37.50	28.00	20.50	16.00	13.50	12.50	10.50	9.00	8.50	7.20
7.20	6.70	5.30	1.20							
95.00	37.00	28.00	19.50	14.50	13.00	12.50	11.00	10.00	8.00	7.00
7.00	6.30	5.00	1.20							
95.00	36.00	27.50	18.00	18.00	12.00	12.00	10.50	9.00	8.00	7.20
5.00	6.30	4.00	1.00							
90.00	35.50	26.00	19.00	14.50	11.50	11.50	11.50	8.50	7.50	7.50
5.00	6.00	4.00	1.00							
95.00	34.00	26.00	19.00	15.00	11.00	12.00	11.00	8.70	8.00	7.00
5.00	6.00	4.20	1.00							
110.00	34.00	23.50	19.00	14.70	13.00	13.00	11.00	9.00	9.00	6.00

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1.0824768E+00 1.1271904E+00 1.1705289E+00 1.2123601E+00 1.2534428E+00
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1.5146752E+00 1.5262421E+00 1.5342630E+00 1.5390122E+00 1.5406130E+00
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1.4902367E+00 1.5151256E+00 1.5713631E+00 1.6068148E+00 1.6329124E+00
1.6558009E+00 1.6745767E+00 1.6911773E+00 1.7058222E+00 1.7192673E+00
1.7323044E+00 1.7470524E+00 1.7657062E+00 1.7907198E+00 1.8082151E+00
1.5550425E+00 1.5873117E+00 1.6391338E+00 1.6747159E+00 1.7039928E+00
1.7293187E+00 1.7524579E+00 1.7741182E+00 1.7940665E+00 1.8125184E+00
1.8293711E+00 1.8468545E+00 1.8694602E+00 1.9021138E+00 1.9255364E+00
1.6418245E+00 1.6616695E+00 1.7090353E+00 1.7442923E+00 1.7758022E+00
1.8049900E+00 1.8332815E+00 1.8611928E+00 1.8879352E+00 1.9125255E+00
1.9311228E+00 1.9380464E+00 1.9270075E+00 1.9004238E+00 1.8814047E+00
1.7225043E+00 1.7381167E+00 1.7778070E+00 1.8121023E+00 1.8456544E+00
1.8788385E+00 1.9128379E+00 1.9483185E+00 1.9846672E+00 2.0215143E+00
2.0548805E+00 2.0774502E+00 2.0778233E+00 2.0607204E+00 2.0493568E+00
1.7965964E+00 1.8079521E+00 1.8395907E+00 1.8723475E+00 1.9074805E+00
1.0442498E+00 1.9835687E+00 2.0268065E+00 2.0738916E+00 2.1271386E+00
2.1880780E+00 2.2634694E+00 2.3688770E+00 2.5493790E+00 2.6917623E+00
1.8778135E+00 1.8827348E+00 1.9022230E+00 1.9324185E+00 1.9686607E+00
2.0087526E+00 2.0534395E+00 2.1041572E+00 2.1618983E+00 2.2310803E+00
2.3171132E+00 2.4346987E+00 2.6067113E+00 2.8674335E+00 3.0545618E+00
1.9563065E+00 1.9531937E+00 1.9575452E+00 1.9844150E+00 2.0210031E+00
2.0634128E+00 2.1119192E+00 2.1678973E+00 2.2321556E+00 2.3084771E+00
2.3982261E+00 2.5018011E+00 2.6070034E+00 2.6550618E+00 2.7371290E+00
2.0412583E+00 2.0277659E+00 2.0125789E+00 2.0352485E+00 2.0715286E+00
2.1155270E+00 2.1668655E+00 2.2265745E+00 2.2948935E+00 2.3746489E+00
2.4651639E+00 2.5640250E+00 2.6562304E+00 2.7198523E+00 2.7427186E+00
2.1233956E+00 2.0988750E+00 2.0627685E+00 2.0808518E+00 2.1161562E+00
2.1608188E+00 2.2137915E+00 2.2756525E+00 2.3459652E+00 2.4267147E+00
2.5173933E+00 2.6229692E+00 2.7561489E+00 2.9517423E+00 3.0957615E+00
2.2101971E+00 2.1725416E+00 2.1117769E+00 2.1248165E+00 2.1579439E+00
2.2018436E+00 2.2550728E+00 2.3179536E+00 2.3894715E+00 2.4700442E+00
2.5544966E+00 2.6349629E+00 2.6984390E+00 2.7643277E+00 2.8146395E+00
2.2531337E+00 2.2091908E+00 2.1368146E+00 2.1474028E+00 2.1783285E+00

2.2205259E+00	2.2727737E+00	2.3356999E+00	2.4086962E+00	2.4927528E+00
2.5831397E+00	2.6723448E+00	2.7485051E+00	2.8323611E+00	2.8952547E+00
2.2515640E+00	2.2155313E+00	2.1567524E+00	2.1658727E+00	2.191905E+00
2.2290327E+00	2.2769025E+00	2.3373294E+00	2.4115608E+00	2.5041475E+00
2.6168129E+00	2.7529640E+00	2.9098486E+00	3.0923688E+00	3.2103936E+00
2.1934112E+00	2.1798798E+00	2.1593699E+00	2.1679690E+00	2.1882922E+00
2.2183509E+00	2.2590232E+00	2.3127557E+00	2.3820815E+00	2.4738014E+00
2.5936655E+00	2.7491929E+00	2.9336425E+00	3.1266695E+00	3.2373314E+00
2.1029439E+00	2.1228970E+00	2.1560113E+00	2.1604552E+00	2.1688814E+00
2.1847413E+00	2.2095903E+00	2.2456951E+00	2.2956448E+00	2.3658014E+00
2.4632818E+00	2.6004555E+00	2.7866729E+00	3.0280126E+00	3.1872594E+00
2.0953010E+00	2.1231411E+00	2.1603608E+00	2.1434089E+00	2.1264820E+00
2.1154370E+00	2.1106526E+00	2.1124223E+00	2.1212615E+00	2.1383993E+00
2.1649236E+00	2.2025968E+00	2.2514537E+00	2.3093541E+00	2.3458089E+00
2.3079370E+00	2.2817307E+00	2.2051310E+00	2.1300498E+00	2.0667525E+00
2.0142219E+00	1.9685286E+00	1.9272917E+00	1.8896660E+00	1.8537017E+00
1.8184831E+00	1.7816093E+00	1.7421811E+00	1.7005746E+00	1.6753996E+00
2.8536853E+00	2.6981526E+00	2.3357893E+00	2.1416617E+00	2.0024239E+00
1.8916662E+00	1.7949727E+00	1.7057304E+00	1.6221904E+00	1.5414140E+00
1.4645743E+00	1.3918863E+00	1.3282498E+00	1.2792876E+00	1.2565270E+00
2.7518200E+00	1			
2.2581083E+00	2			
1.8063600E+00	3			
1.3889950E+00	4			
1.1300950E+00	5			
1.0142083E+00	6			
9.9518750E-01	7			
9.6441917E-01	8			
9.5426917E-01	9			
8.9961167E-01	10			
8.6152250E-01	11			

8.5889167E-01	12
9.0493250E-01	13
9.2801500E-01	14
1.0272283E+00	15
9.2585417E-01	16
7.4422667E-01	17
7.5768167E-01	18
7.2820500E-01	19
7.1056167E-01	20
7.0484833E-01	21
7.0268417E-01	22
6.9382417E-01	23
6.7679500E-01	24
6.4817583E-01	25
6.0436167E-01	26
5.6183500E-01	27
5.2465750E-01	28
4.6668333E-01	29
4.4389833E-01	30
4.9014500E-01	31
4.8859917E-01	32
3.7770917E-01	33
3.4322000E-01	34
4.3321667E-01	35
4.6491083E-01	36
4.1661167E-01	37
5.1132083E-01	38
5.2853250E-01	39
4.9022000E-01	40
5.2170083E-01	41
5.5028417E-01	42

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6.1	6.7	6.6	6.8	7.0	6.8	6.5	6.6	6.7	7.0	7.7	7.6	8.2	8.6	8.7	8.3	8.6	8.9	8.8	PP2
8.5	8.2	8.2	8.2	8.5	8.8	8.6	8.1	8.1	8.1	8.0	8.0	8.6	8.5	7.8	8.0	7.9	7.3	7.2	PP3
7.4	6.6	6.6	5.9	6.0	6.4	6.3	6.2	6.2	5.7	5.2									PP4
2.2	2.3	2.4	2.5	2.8	2.9	3.1	3.1	3.1	2.9	2.7	2.6	2.6	2.4	2.3	2.4	2.5	2.6	2.6	MB1
3.0	3.7	4.3	4.6	5.0	5.4	5.6	5.7	5.9	6.1	6.3	6.7	6.9	7.1	7.2	7.2	7.3	7.3	7.5	MB2
7.7	8.0	8.2	8.4	8.6	8.7	8.9	8.7	8.5	8.2	8.2	8.2	8.4	8.6	8.6	8.6	8.6	8.5	8.4	MB3
8.2	8.0	8.0	8.0	8.0	8.1	8.1	8.1	8.2	8.2	8.2	8.1	8.2	8.2	8.2	8.2	.	.	.	MB4
3.4	3.3	3.3	3.3	3.5	3.5	3.1	2.8	3.0	3.2	3.2	3.7	3.9	4.2	4.7	4.7	5.0	5.0	5.3	SP1
5.4	5.4	5.5	5.3	5.4	5.8	5.6	5.7	6.0	6.1	6.4	6.2	6.2	6.2	6.1	6.1	6.1	6.0	6.0	SP2
6.5	6.9	7.4	7.3	7.2	6.9	7.0	6.8	6.5	6.4	5.8	6.5	6.7	6.7	6.8	6.7	6.4	6.1	6.7	SP3
5.4	5.7	5.6	5.5	5.7	5.8	5.8	6.2	6.2	5.5	5.8	5.3	4.8	4.4	4.0	4.1	.	.	.	SP4
103.01	74.99	95.97	80.17	91.56	83.09	88.30	85.18	85.89	86.74										
83.71	88.02	81.80	89.16	80.02	90.20	78.37	91.14	76.85	91.99										
75.35	92.79	73.93	93.53	72.65	94.17	71.63	94.66	70.90	95.00										
112.05	89.59	103.36	92.98	98.57	95.32	95.06	97.12	92.38	98.51										
90.10	99.68	88.01	100.73	86.04	101.70	84.18	102.59	82.45	103.38										
80.76	104.14	79.12	104.83	77.65	105.43	76.48	105.89	75.64	106.20										
114.46	100.83	107.91	103.32	103.63	105.47	100.31	107.25	97.65	108.70										
95.35	109.94	93.18	111.09	91.09	112.17	89.08	113.15	87.17	114.04										
85.25	114.37	83.37	115.63	81.65	116.27	80.26	116.73	79.27	117.05										
116.92	106.57	111.55	109.94	107.79	112.47	104.73	114.56	102.22	116.27										
99.93	117.78	97.82	119.18	95.70	120.53	93.62	121.79	91.60	122.96										
89.51	124.10	87.41	125.17	85.42	126.10	83.77	126.82	82.55	127.32										
119.58	110.32	114.99	114.43	111.62	117.42	108.82	119.88	106.48	121.89										
104.37	123.68	102.31	125.38	100.27	127.03	98.24	128.63	96.25	130.14										
94.19	131.66	92.07	133.17	90.05	134.54	88.35	135.65	87.07	136.45										
122.47	112.96	119.45	117.84	115.42	121.27	112.87	124.06	110.73	126.35										
108.78	128.40	106.88	130.37	104.99	132.29	103.12	134.17	101.29	135.99										
99.40	137.85	97.46	139.73	95.64	141.49	94.10	142.97	92.95	144.07										
125.79	115.15	122.18	120.72	119.47	124.54	117.18	127.64	115.25	130.19										
113.50	132.47	111.79	134.66	110.11	136.80	108.44	138.91	106.83	140.94										

105.19	143.73	173.54	145.14	102.02	147.12	100.76	148.76	99.90	149.99
129.61	117.20	126.40	123.33	124.01	127.51	122.00	130.89	120.31	133.66
118.78	136.14	117.29	138.51	115.83	140.84	114.39	143.11	113.01	145.30
111.60	147.53	110.20	149.76	108.93	151.82	107.90	153.50	107.15	154.73
133.66	119.01	130.87	125.56	128.81	130.73	127.09	133.65	125.65	136.60
124.34	139.24	123.08	141.77	121.83	144.24	120.60	146.65	119.42	148.96
119.22	151.30	117.02	153.63	115.91	155.77	115.00	157.51	114.33	158.78
137.67	120.48	135.31	127.35	133.59	132.05	132.15	135.84	130.94	138.94
129.85	141.70	128.80	144.34	127.76	146.93	126.74	149.45	125.75	151.87
124.74	154.32	123.72	156.77	122.76	159.02	121.97	160.86	121.37	162.21
141.61	121.62	139.70	128.75	138.30	133.62	137.14	137.54	136.16	140.76
135.28	143.61	134.43	146.34	133.60	149.02	132.78	151.62	132.00	154.13
131.19	156.68	130.36	159.24	129.62	161.61	128.98	163.56	128.50	164.99
145.56	122.49	144.09	129.83	143.02	134.83	142.11	138.86	141.36	142.15
140.65	145.07	140.04	147.86	139.41	150.59	138.80	153.25	138.23	155.80
137.65	158.41	137.09	161.02	136.58	163.46	136.17	165.49	135.88	167.00
149.73	123.14	148.71	130.63	147.97	135.75	147.33	139.86	146.81	143.20
146.33	146.17	145.88	148.99	145.46	151.74	145.05	154.41	144.68	156.97
144.33	159.56	144.01	162.14	143.75	164.54	143.57	166.49	143.47	167.93
154.28	123.57	153.81	131.16	153.42	136.37	153.07	140.55	152.77	143.94
152.49	146.94	152.23	149.77	151.99	152.52	151.76	155.17	151.57	157.68
151.41	160.22	151.28	162.72	151.19	165.03	151.13	166.89	151.11	168.24
158.74	123.65	158.86	131.33	158.83	136.63	158.74	140.87	158.64	144.30
158.53	147.32	158.42	150.17	158.32	152.91	158.22	155.53	158.14	158.00
158.07	160.45	158.05	162.83	158.10	164.95	158.26	166.63	158.48	167.84
164.32	123.13	165.27	131.03	165.68	136.47	165.90	140.81	166.02	144.30
166.11	147.37	166.16	150.25	166.19	153.02	166.21	155.68	166.20	158.18
166.15	160.67	166.05	163.11	165.86	165.34	165.55	167.17	165.17	168.56
167.88	122.42	169.40	130.55	170.07	136.11	170.47	140.52	170.73	144.07
170.92	147.17	171.07	150.09	171.20	152.90	171.30	155.59	171.38	158.14
171.44	160.70	171.48	163.24	171.52	165.59	171.59	167.53	171.67	168.93

171.98	121.27	174.02	129.80	174.94	135.52	175.52	140.02	175.91	143.63
176.22	146.78	176.48	149.74	176.70	152.58	176.91	155.30	177.09	157.86
177.26	160.43	177.44	162.96	177.61	165.27	177.75	167.13	177.86	168.47
176.23	119.93	178.58	128.90	179.70	134.77	180.43	139.37	180.94	143.04
181.35	146.23	181.70	149.22	182.01	152.09	182.29	154.82	182.55	157.39
182.81	159.95	183.07	162.46	183.32	164.73	183.53	166.57	183.68	167.89
180.69	118.60	183.11	127.89	184.41	133.90	185.27	138.59	185.89	142.32
186.37	145.57	186.79	148.60	187.17	151.49	187.51	154.23	187.82	156.80
185.18	117.42	187.68	126.73	189.14	132.90	190.13	137.69	190.84	141.50
188.13	159.35	188.44	161.83	188.72	164.06	188.97	165.84	189.16	167.10
191.40	144.80	191.83	147.87	192.30	150.80	192.68	153.57	193.01	156.15
193.33	158.70	193.64	161.16	193.93	163.36	194.16	165.10	194.34	166.32
199.57	116.22	192.32	125.54	193.96	131.78	195.09	136.67	195.83	140.56
196.52	143.93	197.04	147.07	197.50	150.06	197.89	152.87	198.23	155.49
198.55	158.07	198.83	160.54	199.07	162.74	199.26	164.48	199.41	165.71
193.76	114.82	196.99	124.14	198.87	130.50	200.15	135.52	201.04	139.52
201.73	142.99	202.30	146.21	202.78	149.28	203.19	152.17	203.52	154.85
203.81	157.48	204.05	160.01	204.25	162.26	204.39	164.04	204.49	165.31
197.80	113.07	201.65	122.56	203.81	129.09	205.25	134.26	206.24	138.39
207.00	141.98	207.62	145.31	208.12	148.49	208.53	151.48	208.85	154.25
209.11	156.98	209.31	159.59	209.45	161.92	209.53	163.76	209.58	165.08
201.77	111.02	206.30	120.80	208.75	127.53	210.37	132.89	211.48	137.18
212.31	140.90	212.97	144.38	213.51	147.69	213.93	150.82	214.24	153.72
214.47	156.57	214.62	159.30	214.70	161.73	214.71	163.65	214.68	165.03
205.65	108.82	210.83	118.90	213.58	125.88	215.39	131.44	216.62	135.91
217.53	139.80	218.26	143.44	218.83	146.90	219.27	150.18	219.58	153.24
219.79	155.24	219.91	159.13	219.92	161.71	219.87	163.73	219.78	165.16
209.42	106.54	215.15	116.95	218.20	124.19	220.20	129.97	221.55	134.62
222.56	138.68	223.35	142.45	223.98	146.12	224.44	149.58	224.77	152.80
224.97	155.99	225.06	159.06	225.03	161.80	224.95	163.97	224.87	165.48
213.09	104.06	219.37	114.92	222.71	122.44	224.90	128.45	225.39	133.29

227.49	137.53	222.37	141.51	225.06	145.33	229.57	148.96	229.93	152.37
230.15	155.75	230.24	159.03	230.15	161.98	230.07	164.34	229.93	166.06
216.51	101.61	223.42	112.87	227.05	120.67	229.43	126.91	231.06	131.94
232.27	136.36	233.24	140.51	234.00	144.50	234.58	148.33	234.99	151.92
235.26	155.50	235.38	158.99	235.36	162.16	235.22	164.72	235.00	166.56
219.68	99.38	226.98	111.00	230.86	119.05	233.42	125.49	235.17	130.69
236.49	135.26	237.54	175.57	238.35	143.73	239.04	147.71	239.51	151.46
239.83	155.22	240.01	158.88	240.07	162.23	240.07	164.94	240.08	166.95
223.05	56.72	230.54	108.85	235.08	117.19	237.83	123.85	239.73	129.24
241.17	133.98	242.34	138.46	243.30	142.75	244.04	146.96	244.59	150.90
244.98	154.84	245.21	158.69	245.31	162.15	245.36	164.92	245.36	166.95
227.13	93.63	235.60	106.25	240.05	114.93	243.02	121.84	245.10	127.43
246.70	132.36	248.02	137.03	249.12	141.56	250.01	145.95	250.68	150.12
251.16	154.32	251.42	158.45	251.41	162.14	251.21	164.89	250.99	166.52
230.92	50.55	235.84	103.82	244.56	112.81	247.72	119.94	249.96	125.71
251.71	130.79	253.10	135.61	254.44	140.31	255.45	144.88	256.32	149.25
256.97	153.72	257.39	158.22	257.47	162.48	257.14	166.17	256.40	169.18
233.43	88.59	242.72	102.16	247.59	111.35	250.89	118.62	253.23	124.49
255.09	129.67	256.67	134.59	258.04	139.38	259.21	144.06	260.18	148.55
251.00	153.16	261.64	157.85	262.08	162.36	262.41	166.35	262.80	169.65
236.88	85.70	246.55	99.93	251.61	109.38	255.06	116.83	257.55	122.83
259.54	128.11	261.27	133.14	262.80	138.04	264.15	142.82	265.21	147.44
266.37	152.18	267.31	156.98	268.13	161.50	268.85	165.20	269.46	167.80
241.40	82.14	251.46	97.08	256.71	106.85	260.34	114.48	263.00	120.61
265.17	126.01	267.09	131.13	268.83	136.13	270.41	141.02	271.82	145.72
273.17	150.56	274.42	155.44	275.48	160.01	276.23	163.74	276.70	166.40
246.03	78.52	256.25	94.32	261.63	104.37	265.41	112.16	268.22	118.35
270.55	123.85	272.64	129.04	274.58	134.10	276.37	139.03	278.02	143.78
279.64	148.65	281.21	153.56	282.64	158.23	283.75	162.27	284.51	165.59
250.21	75.52	260.44	91.96	265.90	102.21	269.78	110.10	272.70	116.35
275.16	121.89	277.35	127.11	279.45	132.18	281.47	137.12	283.31	141.87

285.14	146.73	286.94	151.59	288.66	156.06	290.31	159.64	292.01	162.13
257.99	70.54	267.66	88.01	273.15	98.51	277.16	106.52	280.25	112.86
282.89	118.37	285.34	123.57	287.69	128.61	289.95	132.51	292.10	138.20
294.26	143.02	296.37	147.86	298.15	152.45	299.41	156.39	299.90	159.65
263.43	67.55	272.47	85.48	277.93	96.07	282.01	104.11	285.18	110.44
287.91	115.93	290.48	121.08	292.97	126.06	295.40	130.87	297.75	135.48
300.16	140.22	302.59	145.02	304.86	149.59	306.85	153.45	308.59	156.28
270.87	64.61	278.99	82.14	284.42	92.75	288.54	100.79	291.78	107.08
294.61	112.50	297.29	117.55	299.93	122.37	302.55	127.00	305.13	131.40
307.86	135.89	310.72	140.41	313.45	144.75	315.80	148.51	317.39	151.55
276.70	62.60	284.52	79.32	289.95	89.91	294.09	97.93	297.35	104.17
300.21	109.50	302.94	114.42	305.64	119.08	308.35	123.50	311.05	127.63
313.96	131.77	317.09	135.84	320.31	139.62	323.20	142.77	325.82	145.14
283.15	59.55	291.62	75.67	297.09	86.23	301.20	94.23	304.44	100.40
307.27	105.61	309.97	110.26	312.65	114.79	315.33	118.90	318.01	122.64
320.88	126.25	323.95	129.61	327.03	132.44	329.77	134.47	331.92	135.69
293.63	52.72	303.93	69.11	309.46	79.97	313.40	88.05	316.41	94.16
318.99	99.22	321.43	103.73	323.80	107.83	326.14	111.53	328.40	114.79
330.74	117.83	333.10	120.56	335.29	122.81	337.03	124.45	338.23	125.54
311.18	39.23	322.18	60.03	327.08	72.18	330.23	80.77	332.52	87.04
334.41	92.09	336.14	96.48	337.79	100.28	339.28	103.84	340.88	106.84
342.40	109.61	343.92	112.10	345.31	114.16	346.44	115.69	347.26	116.69
.55874	.82934	.56145	.82751	.54720	.83700	.53982	.84178	.53315	.84602
.52608	.85043	.51818	.85527	.50931	.86058	.49959	.86626	.48919	.87218
.47777	.87848	.46548	.88506	.45242	.89181	.43656	.89968	.42036	.90736
.35693	.93413	.42444	.50546	.46227	.88674	.47007	.88263	.46893	.88323
.46359	.88605	.45545	.89026	.44507	.89550	.43298	.90140	.41969	.90767
.40495	.91434	.38918	.92116	.37303	.92782	.35552	.93467	.34041	.94028
.32546	.94556	.42488	.90525	.47296	.88108	.48564	.87416	.48606	.87393
.48043	.87704	.47064	.88233	.45732	.88930	.44094	.89754	.42188	.90665
.39946	.91675	.37418	.92736	.34870	.93724	.32838	.94455	.31865	.94737

.50507	.86308	.54598	.83780	.56292	.82651	.56566	.82464	.56195	.82717
.55454	.83216	.54412	.83901	.53086	.84746	.51495	.85722	.49652	.86802
.47475	.88012	.44595	.89305	.42469	.90534	.40419	.91468	.39439	.91894
.67306	.73959	.66458	.74722	.66024	.75105	.65526	.75541	.64908	.76072
.64190	.76579	.63357	.77368	.62404	.78139	.61340	.78977	.60173	.79870
.58854	.80847	.57350	.81892	.55860	.82944	.54340	.83947	.53251	.84579
.78695	.61702	.75865	.65145	.74237	.66999	.73400	.67915	.72754	.68607
.72184	.69206	.71641	.69768	.71116	.70303	.70621	.70800	.70174	.71244
.69771	.71638	.65438	.71961	.69198	.72191	.69056	.72327	.68987	.72393
.84300	.53792	.82353	.56728	.80907	.58771	.80049	.59534	.79487	.60678
.79071	.61219	.78745	.61638	.78501	.61948	.78352	.62137	.78316	.6218
.78420	.62051	.78704	.61650	.75186	.61070	.79851	.60198	.80368	.59506
.88964	.45666	.87453	.48458	.86305	.50512	.85614	.51675	.85176	.52393
.84873	.52883	.84655	.53231	.84510	.53461	.84439	.53573	.84444	.53565
.84532	.53426	.84711	.53142	.84560	.52743	.85216	.52328	.85375	.52068
.92952	.36877	.91428	.40508	.90487	.42568	.90000	.43590	.89684	.44235
.89461	.44684	.85294	.45018	.89164	.45274	.89064	.45471	.88984	.45627
.88911	.45770	.88833	.45921	.88725	.46128	.88524	.46513	.88284	.46968
.95285	.30345	.94232	.33472	.93618	.35151	.93292	.36009	.93079	.36554
.92930	.36933	.92814	.27224	.92716	.37466	.92626	.37690	.92529	.37927
.92407	.38223	.92244	.38614	.92032	.39117	.91764	.39741	.91520	.40301
.96857	.24873	.96325	.26862	.95948	.28179	.95735	.28894	.95605	.29319
.95524	.29582	.95473	.29748	.95440	.29852	.95418	.29922	.95356	.29992
.95361	.30105	.95296	.30310	.95193	.30631	.95068	.31018	.94950	.31254
.98010	.19852	.97870	.20525	.97660	.21506	.97524	.22116	.97452	.22431
.97422	.22561	.97424	.22553	.97453	.22424	.97507	.22188	.97582	.21858
.97678	.21425	.97793	.20896	.97920	.20289	.98061	.19595	.98182	.18981
.98908	.14740	.98993	.14156	.98894	.14832	.98803	.15426	.98759	.15702
.98751	.15756	.98773	.15620	.98823	.15296	.98902	.14781	.99005	.14072
.99135	.13123	.99287	.11923	.99446	.10514	.99603	.08897	.99715	.07544
.99708	.07632	.99744	.07145	.99681	.07983	.99617	.08743	.99582	.09136

.99570	.09268	.99578	.09179	.99607	.08860	.99655	.08295	.99721	.07464
.99800	.05318	.99881	.04881	.99947	.03243	.99991	.01310	.99956	-.00911
.99970	-.02429	.99999	-.00539	.99992	.01282	.99970	.02448	.99950	.03150
.99936	.03569	.99928	.03788	.99927	.03826	.99933	.03669	.99947	.03258
.99971	.02411	.99997	.00743	.99974	-.02281	.99757	-.06968	.99486	-.10128
.98997	-.14129	.99598	-.08959	.99836	-.05725	.99922	-.03938	.99961	-.02796
.99981	-.01972	.99992	-.01295	.99998	-.00666	1.00000	.00007	.99956	.00871
.99975	.02230	.99894	.04595	.99625	.08652	.98898	.14871	.98092	.19441
.97327	-.22965	.98898	-.14805	.99469	-.10296	.99670	-.08116	.99773	-.06729
.99836	-.05717	.99880	-.04888	.99914	-.04151	.99940	-.03456	.99962	-.02769
.99978	-.02074	.99988	-.01517	.99990	-.01403	.99983	-.01835	.99989	-.01478
.95894	-.28361	.98158	-.19103	.99002	-.14093	.99313	-.11706	.99480	-.10184
.99586	-.09094	.99659	-.08251	.99711	-.07596	.99746	-.07117	.99767	-.06822
.99774	-.06725	.99764	-.06872	.99736	-.07256	.99702	-.07712	.99675	-.08060
.95445	-.29839	.97592	-.21811	.98530	-.17084	.98917	-.14679	.99140	-.13086
.99285	-.11938	.99385	-.11072	.99453	-.10446	.99493	-.10057	.99508	-.09912
.99497	-.10016	.99460	-.10375	.99404	-.10906	.99350	-.11383	.99327	-.11580
.96006	-.27979	.97293	-.23109	.98083	-.15486	.98523	-.17126	.98800	-.15446
.98988	-.14188	.99123	-.13215	.99217	-.12493	.99274	-.12028	.99298	-.11831
.99288	-.11915	.99239	-.12314	.99150	-.13009	.99028	-.13910	.98915	-.14690
.96453	-.26397	.96653	-.24498	.97620	-.21687	.98129	-.19255	.98475	-.17397
.98722	-.15934	.98908	-.14737	.99047	-.13775	.99144	-.13055	.99205	-.12584
.99233	-.12352	.99225	-.12426	.99174	-.12830	.99051	-.13741	.98880	-.14927
.96159	-.27448	.96351	-.26767	.97083	-.23977	.97718	-.21242	.98164	-.19075
.98493	-.17296	.98750	-.15761	.98954	-.14429	.99111	-.13301	.99231	-.12379
.99322	-.11626	.99386	-.11062	.99415	-.10796	.99370	-.11209	.99239	-.12317
.94820	-.31767	.95376	-.30058	.96443	-.26432	.97278	-.23172	.97860	-.20580
.98294	-.18395	.98640	-.16438	.98921	-.14650	.99148	-.13029	.99328	-.11575
.99476	-.10226	.99593	-.09013	.99672	-.08096	.99687	-.07905	.99637	-.08515
.92562	-.37845	.94117	-.33792	.95719	-.28945	.96810	-.25057	.97555	-.21980
.98110	-.19349	.98556	-.16933	.98920	-.14656	.99214	-.12510	.99447	-.10502

.99634	-.08548	.99776	-.06653	.99871	-.05085	.99923	-.03917	.99945	-.03309
.89622	-.44360	.92700	-.37507	.94954	-.31363	.96321	-.26875	.97241	-.23327
.97926	-.20262	.98474	-.17401	.98922	-.14646	.99279	-.11986	.99555	-.09425
.99765	-.06851	.99908	-.04294	.99983	-.01821	.99997	.00771	.99953	.03056
.86685	-.49858	.91282	-.40835	.94200	-.33561	.95828	-.28585	.96917	-.24640
.97726	-.21206	.98373	-.17963	.98900	-.14754	.99315	-.11681	.99628	-.08622
.99850	-.05474	.99974	-.02265	.99996	.00909	.99912	.04190	.99765	.06791
.85598	-.51701	.90302	-.42959	.93490	-.35491	.95341	-.30167	.96579	-.25931
.97500	-.22222	.98238	-.18692	.98837	-.15210	.99307	-.11751	.99654	-.08306
.99889	-.04705	.99995	-.00991	.99969	.02487	.99876	.04981	.99820	.06005
.85249	-.52275	.89583	-.44440	.92823	-.37201	.94857	-.31656	.96220	-.27234
.97237	-.23345	.98755	-.19626	.98721	-.15940	.99245	-.12262	.99631	-.08582
.99889	-.04704	.99998	-.00628	.99943	.03375	.99776	.06684	.99628	.08622
.83739	-.55719	.88385	-.46778	.92214	-.38685	.94386	-.33035	.95845	-.28527
.96940	-.24551	.97827	-.20735	.98554	-.16942	.99130	-.13160	.99557	-.09404
.99848	-.05507	.99989	-.01464	.99962	.02741	.99726	.07395	.99427	.10586
.82731	-.56174	.87965	-.47562	.91686	-.39920	.93946	-.34266	.95470	-.29758
.96621	-.25775	.97564	-.21938	.98347	-.18108	.98975	-.14280	.99447	-.10503
.99775	-.06711	.99950	-.03163	.99999	-.00464	.99998	.00589	.99997	.00824
.81542	-.57888	.87201	-.48948	.91151	-.41127	.93462	-.35566	.95025	-.31148
.96219	-.27240	.97210	-.23456	.98052	-.19644	.98748	-.15777	.99292	-.11880
.99689	-.07883	.99915	-.04123	.99992	-.01236	.99998	.00705	.99988	.01544
.80291	-.59610	.86464	-.50240	.90601	-.42325	.92911	-.36980	.94480	-.32765
.55690	-.29042	.96714	-.25423	.97609	-.21735	.98385	-.17900	.99040	-.13824
.99582	-.09133	.99937	-.03535	.99955	.02991	.99520	.09787	.98744	.15802
.80960	-.58699	.86413	-.50325	.90160	-.43257	.92414	-.38205	.93947	-.34263
.95139	-.30798	.96163	-.27436	.97076	-.24006	.97893	-.20419	.98621	-.16550
.99285	-.11940	.99823	-.05949	.99973	.02337	.99121	.13227	.97918	.20300
.79843	-.60209	.85892	-.51211	.89870	-.43855	.92041	-.39095	.93517	-.35419
.94671	-.32210	.95667	-.29116	.96565	-.25985	.97376	-.22758	.98103	-.19385
.98763	-.15677	.99300	-.11807	.99615	-.08762	.99650	-.08362	.99556	-.08982

.80272	-.59636	.86002	-.51026	.89582	-.44441	.91694	-.40109	.92978	-.36812
.94054	-.33968	.94988	-.31261	.95832	-.28568	.96596	-.25870	.97273	-.23193
.97866	-.20548	.98297	-.18376	.98436	-.17607	.98173	-.19030	.97651	-.21549
.80179	-.59760	.85830	-.51315	.89318	-.44969	.91094	-.41253	.92300	-.38480
.93245	-.36130	.94065	-.33937	.94806	-.31808	.95475	-.29739	.96070	-.27759
.96614	-.25804	.97116	-.23842	.97599	-.21781	.98034	-.19732	.98343	-.18127
.82272	-.56845	.86571	-.50054	.89152	-.45299	.90628	-.42268	.91629	-.40051
.92410	-.38215	.93085	-.36540	.93693	-.34952	.94240	-.33448	.94720	-.32063
.95137	-.20805	.95478	-.29731	.95829	-.28580	.96486	-.26277	.96849	-.24904
.82930	-.55880	.86722	-.49792	.89070	-.45460	.90213	-.43146	.90987	-.41490
.91579	-.40165	.92082	-.38999	.92521	-.37921	.92940	-.36908	.93304	-.35977
.93597	-.35207	.93632	-.35115	.92822	-.37176	.90009	-.43571	.87539	-.4834
.86681	-.49863	.88012	-.47474	.89045	-.45509	.89594	-.44215	.90120	-.43340
.90410	-.42733	.90620	-.42285	.90787	-.41925	.90947	-.41576	.91151	-.41128
.91498	-.40350	.92196	-.39729	.93617	-.35156	.95943	-.28196	.97113	-.23855
.90070	-.43445	.89046	-.45506	.89036	-.45525	.89325	-.44057	.89472	-.44562
.89493	-.44620	.89418	-.44771	.89274	-.45057	.89106	-.45389	.88980	-.45635
.88981	-.45633	.89163	-.45266	.89291	-.45023	.88477	-.46604	.87805	-.47857
.92147	-.38845	.89657	-.44290	.89003	-.45591	.88974	-.45646	.88829	-.45928
.88531	-.46500	.88077	-.47355	.87469	-.48469	.86728	-.49781	.85900	-.51197
.85034	-.52623	.84345	-.53714	.84323	-.53755	.85462	-.51925	.86235	-.50631
.92608	-.37732	.89746	-.44110	.88926	-.45721	.88767	-.46047	.88411	-.46727
.87842	-.47789	.87033	-.49247	.85951	-.51113	.84566	-.53271	.82847	-.56004
.80644	-.59132	.77884	-.62722	.74684	-.66501	.71381	-.70034	.69442	-.71957
.89096	-.45409	.88237	-.45913	.88977	-.45640	.88870	-.45849	.88386	-.46774
.87594	-.48247	.86466	-.50237	.84930	-.52777	.82942	-.55862	.80363	-.59513
.76860	-.63973	.72071	-.69324	.65803	-.75299	.58212	-.81310	.52378	-.85185
.83846	-.54496	.87063	-.47565	.90023	-.43541	.90256	-.43056	.89834	-.43929
.89011	-.45575	.87807	-.47854	.86183	-.50719	.84105	-.54095	.81540	-.57889
.78316	-.62182	.74425	-.66791	.70267	-.71152	.66849	-.74372	.64624	-.76314
.87400	-.48593	.92811	-.37230	.94366	-.33092	.94735	-.32016	.94562	-.32526

.94090	-.33868	.93360	-.35831	.92358	-.38340	.51067	-.41314	.89473	-.44661
.87471	-.42465	.85035	-.52622	.82288	-.56822	.79417	-.60770	.77273	-.63473

APPENDIX A

FORTRAN Listing of Program CONFORM

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C PROGRAM CCNFORM. DETERMINES TRANSFORMATION COEFFS FOR CONFORMAL
C MAPPING OF INTERIOR REGION BOUNDED BY 2 CURVES INTO RECTANGLE.
C
C DIMENSION X2(150) , Y2(150)
C DIMENSION X2P(150) , Y2P(150)
C DIMENSION COB(200) , COC(200)
C
C COMMON/YB/ X2, Y2 , MQ
C COMMON/YA/ X2P , Y2P , MQP
C COMMON/COEF/ VAPWT,JMAX1,IL
C COMMON/FOIA/ COB , COC , BZRO,XK,NMAX
C
C READ CONTINUATION FLAG, NUMBER OF SHORELINE COORDS, NUMBER OF
C SEAWARD BORY COORDS, NUMBER OF COEFFS, MAX NUMBER OF ITERATIONS,
C NUMBER OF INTEGRATION POINTS AND CONVERGENCE CRITERION
C READ(5,1)IWANT, MQ, MQP, NMAX, JMAX1, IL, VAPWT
C 1 FORMAT (6F15, F5.3)
C
C
C
C READ COORDS DELINEATING SHORELINE
C DO 20 L=1,MQ
C READ(5,11) X2(L) , Y2(L)
C 11 FORMAT( 3X , F7.2 , 3X , F7.2 )
C 20 CONTINUE
C READ COORDS DELINEATING SEAWARD BDRY
C DO 30 J=1,MQP
C READ (5,31) X2F(J) , Y2P(J)
C 30 CONTINUE
C 31 FORMAT( F7.2 , 3X , F7.2 )
C

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C
PI= 3.1415927
XLAMDA= X2(MQ)
XK= PI/XLAMDA

WRITE(6,9) MQ,MCP,XLAMDA,VARMT
FORMAT( 1H1 ,//////
9 //,20X,40NUMBER OF COORDS DELINEATING SHORELINE= ,I3
9 //,20X , 43NUMBER OF COORDS DELINEATING SEAWARD BDRY= ,I3
9 //,20X,32HORIZONTAL EXTENT OF SHORELINE= ,F7.2
9 //,20X,29HCONVERGENCE VARIANCE, VARWT= ,F9.6
WRITE(6,60) NMAX,JMAX1,IL
FORMAT( //,20X, 39NUMBER OF TRANSFORMATION COEFFS ,NMAX= ,I3
60 //,20X, 29NUMBER OF ITERATIONS ,JMAX1= ,I3
9 //,20X, 34NUMBER OF INTEGRATION POINTS ,IL= ,I3
WRITE(6,70)
FORMAT( 1H1 ,62X,16HSHORELINE COORDS ,/// )
70 MQ13= MQ/3
MQ3= MC13*3
IADD= MQ-MQ3
DO 71 I=1,MQ13
J= I+MQ13
K= J+MQ13
WRITE(6,72) I,I,X2(I),Y2(I), J,J,X2(J),Y2(J),K,K,X2(K),Y2(K)
72 FORMAT( /,3( 7X,3HX2(,I3,5H),Y2(,I3,3F)= ,F7.2,3X,F7.2) )
IF( IADD .EQ. 0 ) GO TO 75
IF( IADD .EQ. 1 ) NUM1= MQ
IF( IADD .EQ. 2 ) NUM1= MQ-1
DO 73 I=NUM1,MQ
73 WRITE(6,74) I,I,X2(I),Y2(I)
74 FORMAT( /, 85X,3HX2(,I3,5H),Y2(,I3,3H)= ,F7.2,3X,F7.2 )
75 CONTINUE

```

```

80      WRITE(6,80)
      FORMAT( 1H1          ,61X,19HSEAWARD BDY CORDS      ,// )
      MCP13= MCP/3
      MCP3= MCP13*3
      IADD= MCP-MQP3
      DO 81 I=1,MQP13
      J= I+MCP13
      K= J+MCP13
      81  WRITE(6,82)I,I,X2P(I),Y2P(I),J,J,X2P(J),Y2P(J),K,K,X2P(K),Y2P(K)
      82  FORMAT(/,3(5X,4HX2P(,I3,6F),Y2P(,I3,3F)= ,F7.2,3X,F7.2) )
      IF( IADD .EQ. 0 ) GO TO 85
      IF( IACC .EQ. 1 ) NUM1= MQP
      IF( IADD .EQ. 2 ) NUM1= MQP-1
      DO 83 I=NUM1,MQP
      83  WRITE(6,84)I,I,X2P(I),Y2P(I)
      84  FORMAT(/, 87X,4HX2P(,I3,6H),Y2P(,I3,3F)= ,F7.2,3X,F7.2 )
      85  CONTINUE
C
C  DETERMINE COEFFS
C
      A= 0.0
      B= 0.0
      BZRO= 0.0
      WSX= 1.0
      WCX= 1.0
      WSY= 1.0
      WCY= 1.0
      DO 100 N=1,200
      COB(N)= 0.0
      COC(N)= 0.0
      100 CONTINUE

```

(WSX = 0.0)
(WCX = 0.0)


```

IF( IWANT .EQ. 1 ) GO TO 101
GO TO 105
101 READ(5,102) B , BZRO
102 FORMAT( 2E14.7 )
DO 103 N=1,NMAX
103 READ(5,102) COB(N) , COC(N)
READ(5,104) WSX,WSY,WCX,WCY
104 FORMAT( 4E14.7 )
105 CONTINUE
C
A = -B
CALL COEFFS( XLAMDA , A , B , WSX,WSY,WCX,WCY )
C
PUNCH 102 , B,BZRO
C
DO 107 N=1,NMAX
107 PUNCH 102 , COB(N) , COC(N)
C
PUNCH 104 , WSX,WSY,WCX,WCY
C
999 STOP
END
SUBROUTINE COEFFS( XLAMDA , A , B , WSX,WSY,WCX,WCY )
DIMENSION COB(200) , COC(200)
DIMENSION PLMB(200) , DUMC(200)
DIMENSION X2P(150) , Y2(150)
DIMENSION X2P(150) , Y2P(150)
DIMENSION ARCYA(150) , ARCYB(150)
DIMENSION SN(30,30) , CS(30,30)
DIMENSION ATXA(400) , ATYA(400) , ATXB(400) , ATYB(400)
DIMENSION U(400) , V(400) , Z(400)
DIMENSION R(408) , S(408) , T(408) , W(400)
DIMENSION X(408) , Y(408)

```

```

COMMON X,Y
COMMON/YB/ X2, Y2 , MQ
COMMON/YA/ X2P , Y2P , MQP
COMMON/JCHNR/ R
COMMON/JOHNS/ S
COMMON/JOHNT/ T
COMMON/LVM/ U , V , W
COMMON/AYA/ ARCYA
COMMON/AYE/ ARCYB
COMMON/COEF/
COMMON/FORIA/
VARWT,JMAX1,IL
COB , COC
, BZRO,XK,NMAX

C
SIGMA= -1.C
SIGMA1= -1.0
C DETERMINE THE NECESSARY PARAMETERS TO COMPUTE AN INTERPOLATORY
C SPLINE UNDER TENSION THROUGH A SEQUENCE OF FUNCTIONAL VALUES.

MQ1= MQ-1
MQP1= MQP-1
IYB= 0
DO 10 I=1,MQ1
IF( X2(I+1) .LT. X2(I) ) IYB= 1
10 CONTINUE
IF( IYB .EG. 1 ) GO TO 15
CALL CUR1YB( SLP1 , SLPN , SIGMA )
INC= 11
XINC= INC-1
ARCYB(1)= 0.0
DO 13 I=1,MQ1
K= I
II=I+1
DELX= X2(II)-X2(I)

```

```

DELX= DELX/XINC
SUM=0.0
DO 12 J=1,INC
XJ= J-1
XDUM= X2(I) + XJ*DELX
U(J)= CURDYB( XDUM , SIGMA , K )
U(J)= U(J)*U(J) + 1.0
U(J)= SQRT( U(J) )
SUM= SUM + U(J)
SUM= SUM -0.5*U(I) - 0.5*U(INC)
12  ARCYB(II)= ARCYB(I) + SUM*DELX
13  ARCB= ARCYB(MQ)
GO TO 19
15  CONTINUE
ARCYB(1)= 0.0
DO 18 I=1,MQ1
II= I+1
DELX= X2(II)-X2(I)
DELX= DELX*DELX
DELY= Y2(II)-Y2(I)
DELY= DELY*DELY
18  ARCYB(II)= ARCYB(I) + SQRT( DELX + DELY )
19  ARCB= ARCYB(MQ)
CONTINUE
C
CALL CUR2YB( SLP1 , SLPN , SIGMA)
CALL CUR3YE( SLP1 , SLPN , SIGMA)
C
IYA= 0
DO 20 I=1,MQPI
IF( X2P(I+1) .LT. X2P(I) ) IYA= 1
20

```

```

20 CONTINUE
  IF( IYA.EQ. 1 ) GO TO 25
  CALL CUR1YA( SLP1 , SLPN , SIGMA )
  INC= 11
  XINC= INC-1
  ARCYA(1)= 0.0
  DO 23 I=1,MOP1
    K= I
    II=I+1
    DELX= X2P(II)-X2P(I)
    DELX= DELX/XINC
    SUM=0.0
    DO 22 J=1,INC
      XJ= J-1
      XDUM= X2P(I) + XJ*DELX
      U(J)= CURDYA( XDUM , SIGMA1 , K )
      U(J)= U(J)*U(J) + 1.0
      U(J)= SQRT( U(J) )
      SUM= SUM + U(J)
    SUM= SUM -0.5*U(1) - 0.5*U(INC)
  23 ARCYA(II)= ARCYA(I) + SUM*DELX
    ARCA= ARCYA(MOP)
    GO TO 29
  25 CONTINUE
    ARCYA(1)= 0.0
    DO 28 I=1,MOP1
      II= I+1
      DELX= X2P(II) - X2P(I)
      DELX= DELX*DELX
      DELY= Y2P(II) - Y2P(I)
      DELY= DELY*DELY

```



```

28   ARCYA(II)= ARCYA(I) + SQRT( DELX + DELY )
    ARCA= ARCYA(MGF)
29   CONTINUE
C
    CALL CUR2YA( SLP1 , SLPN , SIGMA1 )
    CALL CUR3YA( SLP1 , SLPN , SIGMA1 )
C
    WRITE(6,30)
30   FORMAT( 1H1,/,/,45X,40HARCLENGTH CF SEAWARD BDRY AND COASTLINE
          9//,10X,25HARCLENGTH OF SEAWARD BDRY,8X,3HX2P,9X,3HY2P
          915X,22HARCLENGTH CF COASTLINE,7X,2HX2,10X,2HY2
          DO 31 IT=1,MQP
          IK= IT
          ALNA= ARCYA(IT)
          ATXA(IT)= CUR4YA( ALNA , SIGMA1 , IK )
          ATYA(IT)= CUR5YA( ALNA , SIGMA1 , IK )
          DO 32 IT=1,MC
          IK= IT
          ALNB= ARCYB(IT)
          ATXB(IT)= CUR4YB( ALNB , SIGMA , IK )
          ATYB(IT)= CUR5YB( ALNB , SIGMA , IK )
          IF( MQ .GE. MQP ) NUM2= MQP
          IF( MQ .LE. MQP ) NUM2= MC
          DO 33 I=1,NUM2
          WRITE(6,34)ARCYA(I),ATXA(I),ATYA(I), ARCYB(I),ATXB(I),ATYB(I)
34   FORMAT(25X,F8.2,7X,F7.2,5X,F7.2,25X,F8.2,7X,F7.2,5X,F7.2
          IF( MQ .EQ. MQP ) GO TO 41
          IF( MQ .GT. MQP ) GO TO 35
          IF( MQ .LT. MQP ) GO TO 38
          NUM1= MQP+1
35   DO 36 I=NUM1,MC

```

```

36 WRITE(6,37)
37 FORMAT( 84X,F8.2,7X,F7.2,5X,F7.2
          ,
          ARCYB(1),ATXB(1),ATYB(1)
          )
38 NUM1= MG+1
DO 39 I=NUM1,MQP
39 WRITE(6,40) ARCYA(1),ATXA(1),ATYA(1)
40 FORMAT( 25X,F8.2,7X,F7.2,5X,F7.2
          )
41 CONTINUE
C
C
      IL12= IL/2
      IL2= 2*IL12
      IADD= 0
      IF( IL2 .NE. IL ) IADD= 1
      IL1= IL12 + IADD
      XIL= IL-1
      DELXI= XLAMDA/XIL
      FT= DELXI/XLAMDA
      DO 45 IT=1,IL
      XIT= IT-1
      Z(IT)= XIT*CELXI
45 NUM1= 1
46 NUM2= NMAX
      DO 50 N=NUM1,NUM2
      XN= N
      XNK= XN*XK
      DO 50 IT=1,IL1
      XNKXI= XNK*Z(IT)
      SN(N,IT)= SIN( XNKXI )
      CS(N,IT)= COS( XNKXI )
50
C

```

```

55      ICOUNT= 1
      CONTINUE
      IF( ICOUNT .EQ. 1 ) GO TO 70
      GO TO 79
70      IF( ABS(B) .LT. 0.001 ) GO TO 71
      GO TO 76
71      YSUMA= 0.0
      YSUMB= 0.0
      DO 74 IT=1,IL
      IK= IT
      ALNA= ARCA*Z(IT)/XLAMDA
      ALNB= ARCB*Z(IT)/XLAMDA
      ATXA(IT)= CUR4YA( ALNA , SIGMA1 , IK )
      ATYA(IT)= CUR5YA( ALNA , SIGMA1 , IK )
      ATXB(IT)= CUR4YB( ALNB , SIGMA , IK )
      ATYB(IT)= CUR5YB( ALNB , SIGMA , IK )
      ATXA(IT)= ATXA(IT)-Z(IT)
      ATXB(IT)= ATXB(IT)-Z(IT)
      YSUMA= YSUMA + ATYA(IT)
      YSUMB= YSUMB + ATYB(IT)
74      YSUMA= YSUMA - 0.5*ATYA(1) - 0.5*ATYA(IL)
      YSUMB= YSUMB - 0.5*ATYB(1) - 0.5*ATYB(IL)
      ADUM= YSUMA*FT*WSY
      BDUM= YSUMB*FT*WCY
      GO TO 81
C
76      CONTINUE
      A= -B
      ETAA= A
      ETAB= E
      SUMA= 0.0

```

```

SUMB= 0.0
DO 77 IT=1,IL
XI= Z(IT)
CALL SLFAC( XI,ETAA,DXCETA,DYDETA,SCFACA,SF)
CALL SLFAC( XI,ETAB,DXDETA,DYDETA,SCFACB,SF)
SUMA= SUMA + SCFACA
SUMB= SUMB + SCFACB
U(IT)= SCFACA
V(IT)= SCFACB
77 SUMA= SUMA - 0.5*U(1) - 0.5*U(IL)
SUMB= SUMB - 0.5*V(1) - 0.5*V(IL)
ALNA= SUMA*DELXI
ALNB= SUMB*DELXI
XMODA= ARCA/ALNA
XMODB= ARCE/ALNB
SUMA= 0.0
SUMB= 0.0
ALNA= 0.0
ALNB= 0.0
DO 78 IT=1,IL
IK= IT
ATXA(IT)= CUR4YA( ALNA , SIGMA1 , IK )
ATYA(IT)= CUR5YA( ALNA , SIGMA1 , IK )
ATXB(IT)= CUR4YB( ALNB , SIGMA , IK )
ATYB(IT)= CUR5YB( ALNB , SIGMA , IK )
IF( IT .EQ. IL ) GO TO 78
II= IT+1
SUMA= SUMA + ( U(IT) + U(II) ) *DELXI/2.0
SUMB= SUMB + ( V(IT) + V(II) ) *DELXI/2.0
ALNA= SUMA*XMODA
ALNB= SUMB*XMODB

```



```

78      CONTINUE
C
79      YSUMA= 0.0
      YSUMB= 0.0
      DO 80 IT=1,IL
        ATXA(IT)= ATXA(IT)-Z(IT)
        ATXB(IT)= ATXB(IT)-Z(IT)
        YSUMA= YSUMA + ATYA(IT)
        YSUMB= YSUMB + ATYB(IT)
      80      YSUMA= YSUMA - 0.5*ATYA(1) - 0.5*ATYA(IL)
        YSUMB= YSUMB - 0.5*ATYB(1) - 0.5*ATYB(IL)
        ADUM= YSUMA*FT*WSY
        BDUM= YSUMB*FT*WCY

81      CONTINUE
      A11= WCY+WSY
      A12= WCY-WSY
      B1= BDUM-ADUM
      B2= BDUM+ADUM
      BTOTUM= A11*A11-A12*A12
      BTOTUM= ( B1*A11-B2*A12 )/BTOTUM
      BZDUM= ( E2*A11-B1*A12 )/BTOTUM
      BERR= BTOTUM-B
      BZERR= BZDUM-BZRO
      B= BTOTUM
      BZRO= BZDUM
      A= -B

C
      AVGWX= ( WSX+WCX )/0.5
      AVGWY= ( WSY+WCY )/0.5
      WBAR= ( WCX-WSX+WCY-WSY )/0.5

```

C

```

82      NUM2= NMAX
      XKB= XK*B
      DO 89 N=1,NUM2
      XASUMS= 0.0
      XBSUMS= 0.0
      YASUMC= 0.0
      YBSUMC= 0.0
      N12= N/2
      N2= 2*N12
      DO 87 IT=1,IL
      IF( IT.GT. IL1 ) GO TO 83
      GO TO 85
      IIT= IL-IT+1
      SINN= SN(N,IIT)
      COSS= CS(N,IIT)
      IF( N.EQ. N2 ) GO TO 84
      R(IT)= ATXA(IT)*SINN
      S(IT)= ATXB(IT)*SINN
      T(IT)= -ATYA(IT)*COSS
      W(IT)= -ATYE(IT)*COSS
      GO TO 86
      R(IT)= -ATXA(IT)*SINN
      S(IT)= -ATXB(IT)*SINN
      T(IT)= ATYA(IT)*COSS
      W(IT)= ATYB(IT)*COSS
      GO TO 86
      SINN= SN(N,IT)
      COSS= CS(N,IT)
      R(IT)= ATXA(IT)*SINN
      S(IT)= ATXB(IT)*SINN

```

```

      T(IT)= A1YA(IT)*COSS
      W(IT)= A1YB(IT)*COSS
      CONTINUE
      XASUMS= XASUMS + R(IT)
      XBSUMS= XBSUMS + S(IT)
      YASUMC= YASUMC + T(IT)
      YBSUMC= YBSUMC + W(IT)
      CONTINUE
      XASUMS= XASUMS - 0.5*R(1) - 0.5*R(IL)
      XBSUMS= XBSUMS - 0.5*S(1) - 0.5*S(IL)
      YASUMC= YASUMC - 0.5*T(1) - 0.5*T(IL)
      YBSUMC= YBSUMC - 0.5*W(1) - 0.5*W(IL)
      XASUMS= XASUMS*FT*WSX
      XBSUMS= XBSUMS*FT*WCX
      YASUMC= YASUMC*FT*WSY
      YBSUMC= YBSUMC*FT*WCY
      XN= N
      XNKB= XN*XKB
      SHB= SINH( XNKB )
      CHR= COSH( XNKB )
      TR= SHH/CHR
      SM= TE*TE
      TM= SM/SHB
      A11= SM*AVGWX + AVGWY
      A12= TE*WEAR
      A22= SM*AVGWY + AVGWX
      B1= TM*(-XASUMS+XBSUMS) + (+YASUMC+YBSUMC)/CHE
      B2= TM*(-YASUMC+YBSUMC) + (+XASUMS+XBSUMS)/CHE
      HOTTOM= A11*A22 - A12*A12
      DUMB(N)= ( P1*A22-B2*A12 )/BOTTOM
      DUMC(N)= ( B2*A11-B1*A12 )/BOTTOM

```

```

89 CONTINUE
C
EB1= DUME(1)-COB(1)
EB2= DUMB(2)-COB(2)
EC1= DUMC(1)-COC(1)
EC2= DUMC(2)-COC(2)
C
WRITE(6,250) ICCUNT , NMAX , IL
250 FORMAT( 1H1,20X,18HITERATION NUMBER= ,I3,10X ,6HNMAX= ,I2,10X ,
912HNUM POINTS= ,I4 )
C
WRITE(6,260) A, E, BERR
260 FORMAT(49X,7HALPHA= ,F11.6
9/ ,50X,6HBETA= ,F11.6,3X,8HCHANGE= ,E10.3)
C
WRITE(6,261) BZRC , BZERR
261 FORMAT(48X,8HFE=ZERO= ,F11.6,3X,8HCHANGE= ,E10.3 ,/ )
C
NUMB= 0
NUMC= 0
XKB= XK*F
DO 270 N=1,NMAX
XN= N
XNKB= XN*XKB
PRB= DUMB(N)*COB(N)
PRC= DUMC(N)*COC(N)
IF( PRB .LT. 0.0 ) NUMB= NUMB + 1
IF( PRC .LT. 0.0 ) NUMC= NUMC + 1
ERRB= DUME(N)-COB(N)
ERRC= DUMC(N)-COC(N)
COB(N)= DUMB(N)

```



```

COC(N)= DUMC(N)
AMPB= AES( COB(N)*COSH(XNKB) )
AMPC= ABS( CCC(N)*SINH(XNKB) )
270 WRITE(6,271) N,COR(N),ERRB ,AMPB ,N,CCC(N),ERRC ,AMPC
271 FORMAT( 7X,2F8(.13,3F)= ,F14.7,3X,E10.3,3X,E10.3 , 27X
.92HC(.13,3F)= ,E14.7,3X,E10.3,3X,E10.3 )
C
WRITE(6,272) NUMB , NUMC
272 FORMAT(/,7X,34HNUM OF COEFFS THAT CHANGED SIGN= ,I3
937X .34HNUM OF COEFFS THAT CHANGED SIGN= ,I3 ,// )
C
C
C DETERMINE THE VARIANCE BETWEEN THE PREDICTED COASTLINE AND
C SEAWARD BOUNDARY AND THAT SPECIFIED.
ETAA= A
ETAB= R
SUMA= 0.0
SUMB= 0.0
SUMEXA= 0.0
SUMEYA= 0.0
SUMEXB= 0.0
SUMEYB= 0.0
DO 277 IT=1,IL
XI= Z(IT)
R(IT)= XTRAN( XI , ETAA )
S(IT)= YTRAN( XI , ETAA )
T(IT)= XTRAN( XI , ETAB )
W(IT)= YTRAN( XI , ETAB )
CALL SLFAC( XI,ETAA,DXDETA,DYDETA,SCFACA,SF)
CALL SLFAC( XI,ETAB,DXDETA,DYDETA,SCFACB,SF)
SUMA= SUMA + SCFACA

```

```

SUMB= SUME + SCFACH
SUMXA= (ABS(ATXA(IT)+Z(IT)-R(IT)))**2
SUMYA= (ABS(ATYA(IT)-S(IT)))**2
SUMXB= (ABS(ATXB(IT)+Z(IT)-T(IT)))**2
SUMYB= (ABS(ATYB(IT)-W(IT)))**2
SUMXA= SUMXA + SUMXA
SUMYA= SUMYA + SUMYA
SUMXB= SUMXB + SUMXB
SUMYB= SUMYB + SUMYB
U(IT)= SCFACA
V(IT)= SCFACH
SUMXA= SUMXA - 0.5*SUMXA - 0.5*(ABS(ATXA(1)+Z(1)-R(1)))**2
SUMYA= SUMYA - 0.5*SUMYA - 0.5*(ABS(ATYA(1)-S(1)))**2
SUMXB= SUMXB - 0.5*SUMXB - 0.5*(ABS(ATXB(1)+Z(1)-T(1)))**2
SUMYB= SUMYB - 0.5*SUMYB - 0.5*(ABS(ATYB(1)-W(1)))**2
EFXA= SUMXA*FT*WSX
EFYA= SUMYA*FT*WSY
EFXB= SUMXB*FT*WCX
EFYB= SUMYB*FT*WCY
EF= EFXA+EFYA+EFXB+EFYB
EBAR= EF/4.0
WSY= EFXA/EBAR
WCY= EFXB/EBAR
WSX= EFXA/EBAR
WCX= EFXB/EBAR
SUMA= SUMA - 0.5*U(1) - 0.5*U(IL)
SUMB= SUMB - 0.5*V(1) - 0.5*V(IL)
ALNA= SUMA*DELXI
ALNB= SUMB*DELXI
XMODA= ARCA/ALNA
XMODB= ARCE/ALNB

```

(Remove)
(Remove)

277

```

SUMA= 0.0
SUMB= 0.0
ALNA= 0.0
ALNB= 0.0
VARXA= 0.0
VARYA= 0.0
VARXB= 0.0
VARYB= 0.0
DO 278 IT=1,IL
IK= IT
X(IT)= ALNA
Y(IT)= ALNE
ATXA(IT)= CUR4YA( ALNA , SIGMA1 , IK )
ATYA(IT)= CUREYA( ALNA , SIGMA1 , IK )
ATXB(IT)= CUR4YE( ALNE , SIGMA , IK )
ATYB(IT)= CUREYB( ALNB , SIGMA , IK )
VARXA= VARXA + ABS( ATXA(IT)-R(IT) )**2
VARYA= VARYA + ABS( ATYA(IT)-S(IT) )**2
VARXB= VARXB + ABS( ATXB(IT)-T(IT) )**2
VARYB= VARYB + ABS( ATYB(IT)-W(IT) )**2
IF( IT .EQ. IL ) GO TO 278
II= IT+1
SUMA= SUMA + ( U(IT) + U(II) ) * DELXI/2.0
SUMB= SUMB + ( V(IT) + V(II) ) * DELXI/2.0
ALNA= SUMA*XMCDX
ALNB= SUMB*XMCDY
278 CONTINUE
VARXA= VARXA/XIL
VARYA= VARYA/XIL

```

```

VARXB= VARXB/XIL
VARYB= VARYB/XIL
VAR= ( VARXA+VARYA+VARXB+VARYB )/4.0
VARA= 0.5*( VARXA+VARYA )
VARB= 0.5*( VARXE+VARYB )

C
C
WRITE(6,280) XM(CD,XM(CD), VARXB,EFXB, VARYB,VARB,EFYB
9VARXA,EFXA, VARYA,VARA,EFYA, VAR , EF
280 FORMAT( 35X,56H RATIO OF SEAWARD BDRY ARCLNGTH TO *TRANSFORM* GEN
GENERATED = ,F8.4
9/,32X,56H RATIO OF SEAWARD BDRY ARCLNGTH TO *TRANSFORM* GENERATED
9= ,F8.4 ,//, 66X,8H VARIANCE ,26X,7H ER FNCT
9//,7X,48H TRANSFORM COASTLINE FROM THAT SPECIFIED USING X ,E14.7 ,
920X,E14.7
9/ ,7X,48H TRANSFORM COASTLINE FROM THAT SPECIFIED USING Y ,E14.7 ,
92X,E14.7,4X,E14.7
9/,4X,51H TRANSFORM SEAWARD BDRY FROM THAT SPECIFIED USING X ,E14.7,
920X,E14.7
9/,4X,51H TRANSFORM SEAWARD BDRY FROM THAT SPECIFIED USING Y ,E14.7,
92X,E14.7,4X,E14.7
9/ ,71X,E14.7,20X,E14.7
WRITE(6,281)
281 FORMAT (// ,15X,42H SEAWARD BDRY COORDS , 0---XI---LAMDA , ETA=A,
923X ,39H COASTLINE COORDS , 0---XI---LAMDA , ETA=B
9/ ,9X,9HX(XI,ETA),2X,7FX-GIVEN,4X,9HY(XI,ETA),2X,7HY-GIVEN,4X
98HARC-TRAN,4X,1H
98X ,9HX(XI,ETA),2X,7FX-GIVEN,4X,9HY(XI,ETA),2X,7HY-GIVEN,4X
98HARC-TRAN
C
DO 285 I=1,IL

```



```

285 WRITE(6,286) I,R(I),ATXA(I),S(I),ATYA(I),X(I)
91,T(I),ATXE(I),W(I),ATYR(I),Y(I)
286 FORMAT( 4X,I3,2X,F7.2,3X,F7.2,5X,F7.2,3X,F7.2,4X,F8.2,4X,1HI
94X      ,I3,2X,F7.2,3X,F7.2,5X,F7.2,3X,F7.2,4X,F8.2
)
C
C      ICOUNT= ICOUNT + 1
IF( VAR .LE. VARWT ) GO TO 375
300 IF( ICOUNT .LE. JMAX1 ) GO TO 55
375 RETURN
END
FUNCTION XTRAN( XI , ETA )
DIMENSION COB(200) , COC(200)
COMMON/FCRIA/ COE , COC
XTRAN= 0.0
XKA= XK*ETA
XKXI= XK*XI
DO 10 N=1,NMAX
XN= N
XNKA= XN*XKA
XNKXI= XN*XKXI
CSH= COSH(XNKA)
SNH= SINH(XNKA)
XTRAN=XTRAN+(COC(N)*CSH      +COB(N)*SNH      ) * SIN(XNKXI)
CONTINUE
XTRAN= XTRAN + XI
RETURN
END
10 FUNCTION YTRAN( XI , ETA )
DIMENSION COB(200) , COC(200)
COMMON/FCRIA/ COB , COC
      , BZRO,XK,NMAX

```

```

YTRAN= 0.0
XKA= XK*ETA
XKXI= XK*XI
DO 10 N=1,NMAX
XN= N
XNKA= XN*XKA
XNKXI= XN*XKXI
CSH= COSH(XNKA)
SNH= SINH(XNKA)
YTRAN=YTRAN+(COB(N)*CSH +COC(N)*SNH )*COS(XNKXI)
CONTINUE
YTRAN= YTRAN + ETA + BZRD
RETURN
END
SUBROUTINE SLFAC( XI , ETA , DXDETA , DYDETA , SCFAC , SF )
DIMENSION CCE(200) , COC(200)
COMMON/FORIA/ CCB , COC
XKA= XK*ETA
XKXI= XK*XI
DXDETA= 0.0
DYDETA= 0.0
DO 10 N=1,NMAX
XN= N
XNKA= XN*XKA
XNKXI= XN*XKXI
CSH= COSH(XNKA)
SNH= SINH(XNKA)
XDETA= XN*XK*(COB(N)*CSH +COC(N)*SNH )*SIN(XNKXI)
YDETA= XN*XK*(COB(N)*SNH +COC(N)*CSH )*COS(XNKXI)
DXDETA= DXDETA + XDETA
DYDETA= DYDETA + YDETA

```

10

```

10  CONTINUE
    DYDETA= DYDETA + 1.0
    SF= (ABS(CYDETA))**2 + (AES(CYDETA))**2
    SCFAC= SQRT( SF )
    RETURN
END
SUBROUTINE CUR1YB( SLF1 , SLFN , SIGMA )
    DIMENSION X2(150) , Y2(150)
    DIMENSION A(150) , S(408)
    COMMON/JOHNA/ A
    COMMON/JOHNS/ S
    COMMON/YB/ X2, Y2 , MG
    C FITS SPLINE-- Y2 AS A FUNCTION OF X2
    N= MG
    NM1 = N-1
    NP1 = N+1
    DELX1 = X2(2)-X2(1)
    DX1 = (Y2(2)-Y2(1))/DELX1
    IF (SIGMA.LT.0.) GO TO 5
    SLPP1 = SLF1
    SLPPN = SLFN
    1 SIGMAP = AES(SIGMA)*(N-1)/(X2(N)-X2(1))
    DELS = SIGMAP*DELX1
    EXPS = EXP(DELS)
    SINHS = .5*(EXPS+1./EXPS)
    SINHN = 1./(DELX1*SINHS)
    DIAG1 = SINHN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
    DIAGIN = 1./DIAG1
    A(1) = DIAGIN*(DX1-SLPP1)
    SPDIAG = SINHN*(SINHS-DELS)
    S(1) = DIAGIN*SPDIAG

```

```

IF (N.EQ.2) GO TO 3
DO 2 I = 2,NM1
  DELX2 = X2(I+1)-X2(I)
  DX2 = (Y2(I+1)-Y2(I))/DELX2
  DELS = SIGMAP*DELX2
  EXPS = EXP(DELS)
  SINHS = .5*(EXPS+1./EXPS)
  SINHN = 1./((DELX2*SINHS)
  DIAG2 = SINHN*(DELS*(.5*(EXPS+1./EXPS))-SINHS)
  DIAGN = 1./((DIAG1+DIAG2-SPDIAG* S(I-1))
  A(I) = DIAGN*(DX2-DX1-SPDIAG* A(I-1))
  SPDIAG = SINHN*(SINHS-DELS)
  S(I) = DIAGN*SPDIAG
  DX1 = DX2
2  DIAG1 = DIAG2
3  DIAGN = 1./((DIAG1-SPDIAG* S(NM1))
  A(N) = DIAGN*(SLPPN-DX2-SPDIAG* A(NM1))
DO 4 I = 2,N
  IBAK = NP1-I
4  A(IBAK) = A(IEAK)- S(IEAK)* A(IEAK+1)
  RETURN
5 IF (N.EQ.2) GO TO 6
  DELX2 = X2(3)-X2(2)
  DELX12 = X2(3)-X2(1)
  C1 = -(DELX12+DELX1)/DELX12/DELX1
  C2 = DELX12/DELX1/DELX2
  C3 = -DELX1/DELX12/DELX2
  SLPP1 = C1*Y2(1) + C2*Y2(2) + C3*Y2(3)
  DELN = X2(N)-X2(NM1)
  DELNM1 = X2(NM1)-X2(N-2)
  DELNN = X2(N)-X2(N-2)

```



```

C1 = (DELNN+DELN)/DELNN/DELN
C2 = -DELNN/DELN/DELNM1
C3 = DELN/DELNN/DELNM1
SLPPN = C2*Y2(N-2) + C2*Y2(NM1) + C1*Y2(N)
GO TO 1
6 A(1) = 0.
  A(2) = 0.
  RETURN
END
FUNCTION CURVYB( T , SIGMA , IT )
  DIMENSION X2(150) , Y2(150)
  DIMENSION A(150)
  COMMON/JOHNA/ A
  COMMON/YB/ X2, Y2 , MG
C THIS FUNCTION INTERPOLATES THE COASTLINE AT A GIVEN VALUE FOR X.
C THE VALUE RETURNED IN CURVYB IS THE VALUE OF Y AT X.
C SUBROUTINE CURVYB MUST BE CALLED EARLIER.
  N= M0
  S = X2(N)-X2(1)
  SIGMAP = ABS(SIGMA)*(N-1)/S
  IF (IT.EQ.1) I1 = 2
1 DO 2 I = I1,N
  IF( X2(I)-T ) 2,2,3
2 CONTINUE
  I = N
3 IF( X2(I-1) .LE. T .OR. T .LE. X2(I) ) GO TO 4
  I1 = 2
  GO TO 1
4 DEL1 = T-X2(I-1)
  DEL2 = X2(I)-T
  DELS = X2(I)-X2(I-1)

```

```

EXPS1 = EXP(SIGMAP*DEL1)
SINHDI = .5*(EXPS1-1./EXPS1)
EXPS = EXP(SIGMAP*DEL2)
SINHDI2 = .5*(EXPS-1./EXPS)
EXPS = EXPS1*EXPS
SINHS = .5*(EXPS-1./EXPS)
CURVYR= ( A(I)*SINHDI+ A(I-1)*SINHDI2)/SINHS+((Y2(I)-A(I))*DEL1 +
9(Y2(I-1) - A(I-1))*DEL2 )/DELS
I1 = I
RETURN
END
FUNCTION CURDYB( T , SIGMA , IT )
DIMENSION X2(150) , Y2(150)
DIMENSION A(150)
COMMON/JCHNA/ A
COMMON/YB/ X2, Y2 , MQ
C THIS FUNCTION DIFFERENTIATES THE COASTLINE AT A GIVEN VALUE
C FOR X. THE VALUE RETURNED IN CURDYB IS THE VALUE OF DY/DX AT X.
C SUBROUTINE CURVE MUST BE CALLED EARLIER.
N = MQ
S = X2(N)-X2(1)
SIGMAP = AES(SIGMA)*(N-1)/S
IF (IT.EQ.1) I1 = 2
1 DO 2 I = I1,N
  IF( X2(I)-T ) 2,2,3
2 CONTINUE
  I = N
3 IF( X2(I-1) .LE. T .OR. T .LE. X2(I) ) GO TO 4
  I1 = 2
  GO TO 1
4 DEL1 = T-X2(I-1)

```

```

DEL2 = X2(I)-T
DELS = X2(I)-X2(I-1)
EXPS1 = EXP(SIGMAP*DELI)
COSH01 = .5*(EXPS1+1./EXPS1)
EXPS = EXP(SIGMAP*DEL2)
COSH02 = .5*(EXPS+1./EXPS)
EXPS = EXPS1*EXPS
SINHS = .5*(EXPS-1./EXPS)/SIGMAF
CURDYB= ( A(I)*COSH01- A(I-1)*COSH02)/SINHS+((Y2(I)-A(
1 I))-(Y2(I-1)-A(I-1)))/DELS
1 I1 = I
RETURN
END
SUBROUTINE CUR2YB( SLP1 , SLPN , SIGMA )
DIMENSION ARCYB(150)
DIMENSION X2(150) , Y2(150)
DIMENSION C(150) , S(408)
COMMON/JOHNC/ C
COMMON/JCHNS/ S
COMMON/AYB/ ARCYB
COMMON/YE/ X2, Y2 , MQ
C FITS SPLINE== X2 AS A FUNCTION OF ARCYB
N= MQ
NM1 = N-1
NP1 = N+1
DELX1 = ARCYB(2)-ARCYB(1)
DX1 = (X2(2)-X2(1))/DELX1
IF (SIGMA.LT.0.) GO TO 5
SLPP1 = SLP1
SLPPN = SLPN
1 SIGMA = ABS(SIGMA)*(N-1)/(ARCYB(N)-ARCYB(1))

```

```

DELS = SIGMAP*DELX1
EXPS = EXP(DELS)
SINHS = .5*(EXPS-1./EXPS)
SINHIN = 1./((DELX1*SINHS)
DIAG1 = SINHIN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
DIAGIN = 1./DIAG1
C(1) = DIAGIN*(DX1-SLPP1)
SPDIAG = SINHIN*(SINHS-DELS)
S(1) = DIAGIN*SPDIAG
IF (N.EQ.2) GO TO 3
DO 2 I = 2,NM1
    DELX2 = ARCYR(I+1)-ARCYR(I)
    DX2 = (X2(I+1)-X2(I))/DELX2
    DELS = SIGMAP*DELX2
    EXPS = EXP(DELS)
    SINHS = .5*(EXPS-1./EXPS)
    SINHIN = 1./((DELX2*SINHS)
    DIAG2 = SINHIN*(DELS*(.5*(EXPS+1./EXPS))-SINHS)
    DIAGIN = 1./((DIAG1+DIAG2-SPDIAG* S(I-1))
    C(I) = DIAGIN*(DX2-DX1-SPDIAG* C(I-1))
    SPDIAG = SINHIN*(SINHS-DELS)
    S(I) = DIAGIN*SPDIAG
    DX1 = DX2
2   DIAG1 = DIAG2
3   DIAGIN = 1./((DIAG1-SPDIAG* S(NM1))
    C(N) = DIAGIN*(SLPPN-DX2-SPDIAG* C(NM1))
    DO 4 I = 2,N
        IBAK = NP1-I
4       C(IEAK) = C(IEAK)- S(IEAK)* C(IEAK+1)
    RETURN
5   IF (N.EQ.2) GO TO 6

```


AD-A034 651

TEXAS A AND M RESEARCH FOUNDATION COLLEGE STATION
STORM SURGE SIMULATION IN TRANSFORMED COORDINATES. VOLUME II. P--ETC(U)
NOV 76 J H WANSTRATH

F/G 4/2

DACW72-73-C-0014

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CERC-TR-76-3-VOL-2

NL

2 OF 2

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END

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DELX2 = ARCYB(3)-ARCYB(2)
DELX12 = ARCYB(3)-ARCYB(1)
C1 = -(DELX12+DELX1)/DELX12/DELX1
C2 = DELX12/DELX1/DELX2
C3 = -DELX1/DELX12/DELX2
SLPP1 = C1*X2(1) + C2*X2(2) + C3*X2(3)
DELN = ARCYB(N)-ARCYB(NM1)
DELNM1 = ARCYB(NM1)-ARCYB(N-2)
DELNN = ARCYB(N)-ARCYB(N-2)
C1 = (DELNN+DELN)/DELNN/DELN
C2 = -DELNN/DELN/DELNM1
C3 = DELN/DELNN/DELNM1
SLPPN = C3*X2(N-2) + C2*X2(NM1) + C1*X2(N)
GO TO 1
6 C(1) = 0.
  C(2) = 0.
  RETURN
END
FUNCTION CUR4YB( T , SIGMA , IT )
  DIMENSION ARCYB(150)
  DIMENSION X2(150) , Y2(150)
  DIMENSION C(150)
  COMMON/JOHNC/ C
  COMMON/AYE/ ARCYB
  COMMON/YB/ X2, Y2 , MG
  C THIS FUNCTION INTERPOLATES THE COASTLINE AT A GIVEN VALUE FOR
  C THE ARCLENGTH. THE VALUE RETURNED IN CUR4YB IS THE VALUE OF X
  C AT ITS PARTICULAR ARCLENGTH. SUBROUTINE CUR2YE MUST BE CALLED BEFORE.
  N= MG
  S = ARCYB(N)-ARCYB(1)
  SIGMAP = ABS(SIGMA)*(N-1)/S

```

```

IF (IT.EG.1) I1 = 2
1 DO 2 I = I1,N
  IF( ARCYB(I)-T ) 2,2,3
2  CONTINUE
  I = N
3  IF( ARCYB(I-1) .LE. T .OR. T .LE. ARCYB(I) ) GO TO 4
  I1 = 2
  GO TO 1
4  DEL1 = T-ARCYB(I-1)
  DEL2 = ARCYB(I)-T
  DELS = ARCYB(I)-ARCYB(I-1)
  EXPS1 = EXP(SIGMA*DEL1)
  SINHD1 = .5*(EXPS1-1./EXPS1)
  EXPS = EXP(SIGMA*DEL2)
  SINHD2 = .5*(EXPS-1./EXPS)
  EXPS = EXPS1*EXPS
  SINHS = .5*(EXPS-1./EXPS)
  CUR4YB= ( C(I)*SINHD1+ C(I-1)*SINHD2)/SINHS+(X2(I)-C(I))*DEL1 +
9(X2(I-1) - C(I-1))*DEL2 )/DELS
  I1 = 1
  RETURN
END
SUBROUTINE CUR3YB( SLP1 , SLPN , SIGMA )
  DIMENSION ARCYB(150)
  DIMENSION X2(150) , Y2(150)
  DIMENSION C(150) , S(408)
  COMMON/JOHND/ D
  COMMON/JOHNS/ S
  COMMON/AYF/ ARCYB
  COMMON/YB/ X2, Y2 , MQ
C  FITS SPLINE== Y2 AS A FUNCTION OF ARCYB

```



```

N= MQ
NM1 = N-1
NP1 = N+1
CELX1 = ARCYB(2)-ARCYB(1)
DX1 = (Y2(2)-Y2(1))/DELX1
IF (SIGMA.LT.0.) GO TO 5
SLPP1 = SLPI
SLPPN = SLPN
1 SIGMAP = ABS(SIGMA)*(N-1)/(ARCYB(N)-ARCYB(1))
DELS = SIGMAP*DELX1
EXPS = EXP(DELS)
SINHS = .5*(EXPS-1./EXPS)
SINHIN = 1./((DELX1*SINHS)
DIAG1 = SINHIN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
DIAGIN = 1./DIAG1
D(1) = DIAGIN*(DX1-SLPP1)
SPDIAG = SINHIN*(SINHS-DELS)
S(1) = DIAGIN*SPDIAG
IF (N.EG.2) GC TC 3
DO 2 I = 2,NM1
  DELX2 = ARCYB(I+1)-ARCYB(I)
  DX2 = (Y2(I+1)-Y2(I))/DELX2
  DELS = SIGMAP*DELX2
  EXPS = EXP(DELS)
  SINHS = .5*(EXPS-1./EXPS)
  SINHIN = 1./((DELX2*SINHS)
  DIAG2 = SINHIN*(DELS*(.5*(EXPS+1./EXPS)-SINHS)
  DIAGIN = 1./((DIAG1+DIAG2-SPDIAG* S(I-1))
  D(I) = DIAGIN*(DX2-DX1-SPDIAG* D(I-1))
  SPDIAG = SINHIN*(SINHS-DELS)
  S(I) = DIAGIN*SPDIAG

```

```

DX1 = DX2
2  DIAG1 = DIAG2
3  DIAGIN = 1./((CIAC1-SPDIAG* S(NM1))
   D(N) = DIAGIN*(SLPPN-DX2-SPCIAG* D(NM1))
DO 4 I = 2,N
   IBAK = NFI-1
4  D(IBAK) = D(IBAK) - S(IBAK)* D(IEAK+1)
   RETURN
5  IF (N.EQ.2) GO TO 6
   DELX2 = ARCYB(3)-ARCYB(2)
   DELX12 = ARCYB(3)-ARCYB(1)
   C1 = -(DELX12+DELX1)/DELX12/DELX1
   C2 = DELX12/DELX1/DELX2
   C3 = -DELX1/DELX12/DELX2
   SLPP1 = C1*Y2(1) + C2*Y2(2) + C3*Y2(3)
   DELN = ARCYB(N)-ARCYB(NM1)
   DELNM1 = ARCYE(NM1)-ARCYB(N-2)
   DELNN = ARCYB(N)-ARCYE(N-2)
   C1 = (DELN+DELN)/DELN/DELN
   C2 = -DELN/DELN/DELN
   C3 = DELN/DELN/DELN
   SLPPN = C3*Y2(N-2) + C2*Y2(NM1) + C1*Y2(N)
   GO TO 1
6  D(1) = 0.
   D(2) = 0.
   RETURN
END
FUNCTION CUREYB( T , SIGMA , IT )
DIMENSION ARCYB(150)
DIMENSION X2(150) , Y2(150)
DIMENSION D(150)

```

```

COMMON/JCHND/ D
COMMON/AYE/ ARCYB
COMMON/YB/ X2, Y2 , MC
C THIS FUNCTION INTERPOLATES THE COASTLINE AT A GIVEN VALUE FOR
C THE ARCLENGTH. THE VALUE RETURNED IN CUR5YB IS THE VALUE OF Y
C AT ITS PARTICULAR ARCLENGTH. SUERCUTINE CUR3YB MUST BE CALLED BEFORE.
N= MQ
S = ARCYE(N)-ARCYB(1)
SIGMAP = ABS(SIGMA)*(N-1)/S
IF (IT.EQ.1) I1 = 2
1 DO 2 I = I1,N
  IF( ARCYB(I)-T ) 2,2,3
2 CONTINUE
  I = N
3 IF( ARCYB(I-1) .LE. T .OR. T .LE. ARCYB(I) ) GO TO 4
  I1 = 2
  GO TO 1
4 DEL1 = T-ARCYB(I-1)
  DEL2 = ARCYB(I)-T
  DELS = ARCYB(I)-ARCYB(I-1)
  EXPS1 = EXP(SIGMAP*DEL1)
  SINHD1 = .5*(EXPS1-1./EXPS1)
  EXPS = EXP(SIGMAP*DEL2)
  SINHD2 = .5*(EXPS-1./EXPS)
  EXPS = EXPS1*EXPS
  SINHS = .5*(EXPS-1./EXPS)
  CUR5YB= ( D(I)*SINHD1 + D(I-1)*SINHD2)/SINHS+((Y2(I)-D(I))*DELI +
9(Y2(I-1) - C(I-1))*CEL2 )/DELS
  I1 = I
  RETURN
END

```

```

SUBROUTINE CUR1YA( SLPI, SLPN, SIGMA )
  DIMENSION B(150), S(408)
  DIMENSION X2P(150), Y2P(150)
  COMMON/JCHNE/ B
  COMMON/JOHNS/ S
  COMMON/YA/ X2P, Y2P, MQP
  C FITS SPLINE=Y2P AS A FUNCTION OF X2F
  N= MQP
  NM1 = N-1
  NP1 = N+1
  DELX1 = X2P(2)-X2P(1)
  DX1 = (Y2F(2)-Y2F(1))/DELX1
  IF (SIGMA.LT.0.) GO TO 5
  SLPP1 = SLPI
  SLPPN = SLPN
  1 SIGMAP = ARS(SIGMA)*(N-1)/(X2P(N)-X2P(1))
  DELS = SIGMAP*DELX1
  EXPS = EXP(DELS)
  SINHS = .5*(EXPS-1./EXPS)
  SINHN = 1./((DELX1*SINHS)
  DIAG1 = SINHN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
  DIAGN = 1./DIAG1
  R(1) = DIAGIN*(DX1-SLPP1)
  SPDIAG = SINHN*(SINHS-DELS)
  S(1) = DIAGIN*SPDIAG
  IF (N.EC.2) GO TO 3
  DO 2 I = 2,NM1
    DELX2 = X2P(I+1)-X2P(I)
    DX2 = (Y2F(I+1)-Y2F(I))/DELX2
    DELS = SIGMAP*DELX2
    EXPS = EXP(DELS)

```



```

SINH5 = .5*(EXPS-1./EXPS)
SINHIN = 1./((DELX2*SINH5)
DIAG2 = SINHIN*(DELS*(.5*(EXPS+1./EXPS))-SINH5)
DIAGIN = 1./((CIAC1+DIAG2-SPDIAG* S(I-1))
B(I) = CIACIN*(DX2-DX1-SPCIAC* B(I-1))
SPDIAG = SINHIN*(SINH5-DELS)
S(I) = CIACIN*SPDIAG
DX1 = DX2
2_ DIAG1 = DIAG2
3 CIACIN = 1./((CIAC1-SFCIAC* S(NM1))
B(N) = DIAGIN*(SLPPN-DX2-SPDIAC* B(NM1))
DO 4 I = 2,N
IBAK = NF1-1
4 B(IRAK) = B(IBAK)- S(IEAK)* B(IBAK+1)
RETURN
5 IF (N.FC.2) GC TC 6
DELX2 = X2P(3)-X2P(2)
DELX12 = X2P(3)-X2P(1)
C1 = -(DELX12+DELX1)/DELX12/DELX1
C2 = DELX12/DELX1/DELX2
C3 = -DELX1/DELX12/DELX2
SLPP1 = C1*Y2P(1)+ C2*Y2P(2)+ C3*Y2P(3)
DELN = X2P(N)-X2P(NM1)
DELNM1 = X2P(NM1)-X2P(N-2)
DELNN = X2P(N)-X2P(N-2)
C1 = (DELNN+DELN)/DELNN/DELN
C2 = -DELNN/DELN/DELNM1
C3 = DELN/DELNN/DELNM1
SLPPN = C3*Y2P(N-2)+ C2*Y2P(NM1)+ C1*Y2P(N)
GO TO 1
6 B(1) = 0.

```



```

      B(2) = C.
      RETURN
      END
      FUNCTION CURVYA( T , SIGMA , IT )
      DIMENSION X2P(150) , Y2P(150)
      DIMENSION B(150)
      COMMON/JOHNE/ R
      COMMON/YA/ X2F , Y2F , MQP
      C THIS FUNCTION INTERPOLATES THE SEAWARD BDRY AT A GIVEN VALUE FOR X.
      C THE VALUE RETURNED IN CURVYA IS THE VALUE OF Y AT X.
      C SUBROUTINE CUR1YA MUST BE CALLED EARLIER.
      N= MQP
      S = X2P(N)-X2P(1)
      SIGMA1= ABS(SIGMA)*(N-1)/S
      IF (IT.EQ.1) I1 = 2
      1 DO 2 I = I1,N
      IF( X2P(I)-T ) 2,2,3
      2 CONTINUE
      I = N
      3 IF( X2P(I-1) .LE. T .OR. T .LE. X2P(I) ) GO TO 4
      I1 = 2
      GO TO 1
      4 DEL1 = T-X2P(I-1)
      DEL2 = X2P(I) - T
      DELS = X2P(I)-X2P(I-1)
      EXPS1 = EXP(SIGMAF*DEL1)
      SINHD1 = .5*(EXPS1-1./EXPS1)
      EXPS = EXP(SIGMAF*DEL2)
      SINHD2 = .5*(EXPS-1./EXPS)
      EXPS = EXPS1*EXPS
      SINHS = .5*(EXPS-1./EXPS)

```

```

CURVYA= ( E(I)*SINHDI+ B(I-1)*SINHDI2)/SINHDI+((Y2P(I)-B(I))*DELI +
9(Y2P(I-1) -E(I-1))*DEL2 )/DELS
I1 = I
RETURN
END
FUNCTION CURDYA( T , SIGMA , IT )
DIMENSION X2P(150) , Y2P(150)
DIMENSION E(150)
COMMON/JOHNB/ B
COMMON/YA/ X2P , Y2P , MQP
C THIS FUNCTION DIFFERENTIATES THE SEAWARD BDRY AT A GIVEN VALUE
C FOR X. THE VALUE RETURNED IN CURDYA IS THE VALUE OF DY/DX AT X.
C SUBROUTINE CURIYA MUST BE CALLED EARLIER.
N= MQP
S = X2P(N)-X2P(1)
SIGMAP = ABS(SIGMA)*(N-1)/S
IF (IT.EQ.1) I1 = 2
1 DO 2 I = I1,N
IF( X2P(I)-T ) 2,2,3
2 CONTINUE
I = N
3 IF( X2P(I-1) .LE. T .OR. T .LE. X2P(1) ) GO TO 4
I1 = 2
GO TO 1
4 DEL1 = T-X2P(I-1)
DEL2 = X2P(I) - T
DELS = X2P(I)-X2P(I-1)
EXPS1 = EXP(SIGMAP*DELI)
COSHDI = .5*(EXPS1+1./EXPS1)
EXPS = EXP(SIGMAP*DEL2)
COSHDI2 = .5*(EXPS+1./EXPS)

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```

EXPS = EXPS1*EXPS
SINHS = .5*(EXPS-1./EXPS)/SIGMAP
CURDYA= ( B(I)*COSHC1- B(I-1)*COSTD2)/SINHS+((Y2P(I))-B(
1 I))-(Y2P(I-1)-B(I-1))/DELS
I1 = I
RETURN
END
SUBROUTINE CUR2YA( SLP1 , SLPN , SIGMA )
DIMENSION ARCYA(150)
DIMENSION F(150) , S(408)
DIMENSION X2P(150) , Y2P(150)
COMMON/JCHNE/ E
COMMON/JOHNS/ S
COMMON/AYA/ ARCYA
COMMON/YA/ X2P , Y2P , MQF
C FITS SPLINE--X2P AS A FUNCTION OF ARCYA
N = MQP
NM1 = N-1
NP1 = N+1
DELX1 = ARCYA(2)-ARCYA(1)
DX1 = (X2P(2)-X2P(1))/DELX1
IF (SIGMA.LT.C.) GO TO 5
SLPP1 = SLP1
SLPPN = SLPN
1 SIGMAP = AES(SIGMA)*(N-1)/(ARCYA(N)-ARCYA(1))
DELS = SIGMAP*DELX1
EXPS = EXP(DELS)
SINHS = .5*(EXPS-1./EXPS)
SINHIN = 1./((DELX1*SINHS)
DIAG1 = SINHIN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
DIAGIN = 1./DIAG1

```

```

E(I) = DIAGIN*(DX1-SLPP1)
SPDIAG = SINHIN*(SINHS-DELS)
S(I) = DIAGIN*SPDIAG
IF (N.EQ.2) GC TO 3
DO 2 I = 2,NM1
    DELX2 = ARCYA(I+1)-ARCYA(I)
    DX2 = (X2P(I+1)-X2F(I))/DELX2
    DELS = SIGMAP*DELX2
    EXPS = EXP(DELS)
    SINHS = .5*(FXFS+1./EXPS)
    SINHIN = 1./((DELX2*SINHS)
    DIAG2 = SINHIN*(DELS*(.5*(EXPS+1./EXPS))-SINHS)
    DIAGIN = 1./((DIAG1+DIAG2-SPDIAG* S(I-1))
    E(I) = DIAGIN*(DX2-DX1-SPDIAG* E(I-1))
    SPDIAG = SINHIN*(SINHS-DELS)
    S(I) = DIAGIN*SPDIAG
    DX1 = DX2
2   DIAG1 = DIAG2
3   DIAGIN = 1./((DIAG1-SPDIAG* S(NM1))
    E(N) = DIAGIN*(SLPPN-DX2-SPDIAG* E(NM1))
DO 4 I = 2,N
    IBAK = NP1-I
4   E(IBAK) = E(IBAK)- S(IBAK)* E(IBAK+1)
    RETURN
5   IF (N.EQ.2) GC TO 6
    DELX2 = ARCYA(3)-ARCYA(2)
    DELX12 = ARCYA(3)-ARCYA(1)
    C1 = -(DELX12+DELX1)/DELX12/DELX1
    C2 = DELX12/DELX1/DELX2
    C3 = -DELX1/DELX12/DELX2
    SLPP1 = C1*X2P(1)+ C2*X2P(2)+ C3*X2P(3)

```



```

DELN = ARCYA(N)-ARCYA(NM1)
DELM1 = ARCYA(NM1)-ARCYA(N-2)
DELN = ARCYA(N)-ARCYA(N-2)
C1 = (DELN+DELN)/DELN/DELN
C2 = -DELN/DELN/DELM1
C3 = DELN/DELN/DELM1
SLPPN = C3*X2P(N-2) + C2*X2P(NM1) + C1*X2P(N)
GO TO 1
6 E(1) = 0.
F(2) = 0.
RETURN
END
FUNCTION CUR4YA( T , SIGMA , IT )
DIMENSION ARCYA(150)
DIMENSION X2P(150) , Y2P(150)
DIMENSION E(150)
COMMON/JCHNE/ E
COMMON/AYA/ ARCYA
COMMON/YA/ X2P , Y2P , MQP
C THIS FUNCTION INTERPOLATES THE SEAWARD PCRY AT A GIVEN VALUE FOR
C THE ARCLNGTH. THE VALUE RETURNED IN CUR4YA IS THE VALUE OF X
C AT ITS PARTICULAR ARCLNGTH. SUBROUTINE CUR2YA MUST BE CALLED BEFORE.
N= MQP
S = ARCYA(N)-ARCYA(1)
SIGMAP = ABS(SIGMA)*(N-1)/S
IF (IT.EQ.1) I1 = 2
1 DO 2 I = I1,N
  IF ( ARCYA(I)-T ) 2,2,3
2 CONTINUE
  I = N
3 IF( ARCYA(I-1) .LE. T .OR. T .LE. ARCYA(1) ) GO TO 4

```

```

      I1 = 2
      GO TO 1
4     DEL1 = T-ARCYA(I-1)
      DEL2 = ARCYA(I)-T
      DELS = ARCYA(I)-ARCYA(I-1)
      EXPS1 = EXP(SIGMAP*DEL1)
      SINHD1 = .5*(EXPS1-1./EXPS1)
      EXPS = EXP(SIGMAP*DEL2)
      SINHD2 = .5*(EXPS-1./EXPS)
      EXPS = EXPS1*EXPS
      SINHS = .5*(EXPS-1./EXPS)
      CUR4YA = ( E(I)*SINHDI+ E(I-1)*SINHDI2)/SINHS+((X2P(I)-E(I))*DEL1 +
9(X2P(I-1)-E(I-1))*DEL2 )/DELS
      I1 = I
      RETURN
      END
      SUBROUTINE CUR3YA( SLP1 , SLFN , SIGMA )
      DIMENSION ARCYA(150)
      DIMENSION X2P(150) , Y2P(150)
      DIMENSION F(150) , S(408)
      COMMON/JCHNF/ F
      COMMON/JOHNS/ S
      COMMON/AYAY/ ARCYA
      COMMON/YA/ X2F , Y2F , MGP
      C FITS SPLINE--Y2P AS A FUNCTION OF ARCYA
      N = MGP
      NM1 = N-1
      NP1 = N+1
      DELX1 = ARCYA(2)-ARCYA(1)
      DX1 = (Y2P(2)-Y2P(1))/DELX1
      IF (SIGMA.LT.0.) GO TO 5

```

```

SLPP1 = SLPP1
SLPPN = SLPPN
1 SIGMAP = ABS(SIGMA)*(N-1)/(ARCYA(N)-ARCYA(1))
DELS = SIGMAP*DELX1
EXPS = EXP(DELS)
SINHS = .5*(EXPS+1./EXPS)
SINHIN = 1./((DELX1*SINHS)
DIAG1 = SINHIN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
DIAGIN = 1./DIAG1
F(1) = DIAGIN*(DX1-SLPP1)
SPDIAG = SINHIN*(SINHS-DELS)
S(1) = DIAGIN*SPDIAG
IF (N.EQ.2) GO TO 3
DO 2 I = 2,N1
    DELX2 = ARCYA(I+1)-ARCYA(I)
    DX2= (Y2P(I+1)-Y2P(I))/DELX2
    DELS = SIGMAP*DELX2
    EXPS = EXP(DELS)
    SINHS = .5*(EXPS+1./EXPS)
    SINHIN = 1./((DELX2*SINHS)
    DIAG2 = SINHIN*(DELS*(.5*(EXPS+1./EXPS))-SINHS)
    DIAGIN = 1./((DIAG1+DIAG2-SPDIAG)* S(I-1))
    F(I) = DIAGIN*(DX2-DX1-SPDIAG* F(I-1))
    SPDIAG = SINHIN*(SINHS-DELS)
    S(I) = DIAGIN*SPDIAG
DX1 = DX2
2 DIAG1 = CIAG2
3 DIAGIN = 1./((CIAG1-SPCIAG* S(NM1))
F(N) = DIAGIN*(SLPPN-DX2-SPDIAG* F(NM1))
DO 4 I = 2,N
    IBAK = NPI-1

```

```

4  F(1BAK) = F(IEAK) - S(IEAK)* F(1BAK+1)
   RETURN
5  IF (N.EQ.2) GO TO 6
   DELX2 = ARCYA(3)-ARCYA(2)
   DELX12 = ARCYA(3)-ARCYA(1)
   C1 = -(DELX12+DELX1)/DELX12/DELX1
   C2 = DELX12/DELX1/DELX2
   C3 = -DELX1/DELX12/DELX2
   SLPP1 = C1*Y2P(1) + C2*Y2P(2) + C3*Y2P(3)
   DELN = ARCYA(N)-ARCYA(NM1)
   DELNM1 = ARCYA(NM1)-ARCYA(N-2)
   DELNN = ARCYA(N)-ARCYA(N-2)
   C1 = (DELNN+DELN)/DELNN/DELN
   C2 = -DELNN/DELN/DELMN1
   C3 = DELN/DELNN/DELMN1
   SLPPN = C3*Y2P(N-2) + C2*Y2P(NM1) + C1*Y2P(N)
   GO TO 1
6  F(1) = 0.
   F(2) = 0.
   RETURN

```

END

FUNCTION CURSYA(T , SIGMA , IT)

DIMENSION ARCYA(150)

DIMENSION X2P(150) , Y2P(150)

DIMENSION F(150)

COMMON/JCHNF/ F

COMMON/AYA/ ARCYA

COMMON/YA/ X2P , Y2P , MQP

C THIS FUNCTION INTERPOLATES THE SEAWARD BCY AT A GIVEN VALUE FOR
C THE ARCLNGTH. THE VALUE RETURNED IN CURSYA IS THE VALUE OF Y
C AT ITS PARTICULAR ARCLNGTH. SUBROUTINE CUR3YA MUST BE CALLED BEFORE.


```

N= MQP
S = ARCYA(N)-ARCYA(1)
SIGMAP = ABS(SIGMA)*(N-1)/S
IF (IT.EQ.1) I1 = 2
1 DO 2 I = I1,N
  IF( ARCYA(I)-T ) 2,2,3
2 CONTINUE
  I = N
3 IF( ARCYA(I-1) .LE. T .OR. T .LE. ARCYA(1) ) GO TO 4
  I1 = 2
  GO TO 1
4 DEL1 = T-ARCYA(I-1)
  DEL2 = ARCYA(I)-T
  DELS = ARCYA(I)-ARCYA(I-1)
  EXPS1 = EXP(SIGMAP*DEL1)
  SINHD1 = .5*(EXPS1-1./EXPS1)
  EXPS = EXP(SIGMAP*DEL2)
  SINHD2 = .5*(EXPS-1./EXPS)
  EXPS = EXPS1*EXPS
  SINHS = .5*(EXPS-1./EXPS)
  SINHS = .5*(EXPS-1./EXPS)
  CUR5YA= ( F(I)*SINHD1+ F(I-1)*SINHD2)/SINHS+( Y2P(I)-F(I))*DEL1 +
9(Y2P(I-1) -F(I-1))*DEL2 )/DELS
  I1 = I
  RETURN
END
FUNCTION SINH(X)
Y=X
S=EXP(X)-EXP(Y)
SINH= S/2.
RETURN

```

```
END  
FUNCTION COSH(X)  
Y=X  
S=EXP(X)+EXP(Y)  
COSH= S/2.  
RETURN  
END
```

APPENDIX B

FORTRAN Listing of Program GRID

PROGRAM GRID. DETERMINES THE COMPUTING GRID DATA FOR INPUT
TO PROGRAM SSURGE. IT IS ASSUMED THAT THE CONFORMAL MAPPING
OF THE REGION IS COMPLETE (PROGRAM CONFORM) WITH OUTPUT OF THE
COEFFS.

GRID FOR HURRICANE CARLA

```

DIMENSION COB(200) , COC(200)
DIMENSION X2(1000) , Y2(1000)
DIMENSION X2P(1000) , Y2P(1000)
DIMENSION ATXA(1000) , ATYA(1000) , ATXB(100) , ATYB(1000)
DIMENSION XI(47) , ETA(15) , X(47,15) , Y(47,15) , Z(47,15)
DIMENSION SX(100) , SY(100)
DIMENSION A(5),B(5),C(5),IIC(5)
COMMON /YE/ X2,Y2,MQ
COMMON /YA/ X2P,Y2P,MQP
COMMON/XIETXY/ XI,ETA,X,Y
COMMON/SXY/ SX,SY
COMMON/ED/ XKBETA,BZPBT,BZMBT
COMMON /FORIA/ COB,COB,COC,BZPC,XK,NMAX

```

READ NUMBER OF COEFFS. NUMBER OF XI LINES+2, NUMBER OF ETA LINES,
VALUE OF DELTA S STAR IN NM, FIRST VALUE OF S STAR IN NM, VALUE OF
DELTA T STAR IN MINUTES, NUMBER OF DEPTHS, NUMBER OF POINTS

```

READ(5,1)NMAX,NUMXI,NUMETA,DELSS,SSSTRT,DELT,ND,NS
1 FORMAT(3I4, 3F5.1, 2I4)

```

SLMAP=60./51.
XLAMDA= 360.


```

XIDUM= 360.0*26.0/33.0
PI = 3.141593
XK = PI/XLAMD
SIGMA = -1.
G= 32.2
NUMET1= NUMETA-1
NUMXI1= NUMXI-1
NUMXI2= NUMXI-2

C
READ (5,27) BETA,BZRO
DC 26 N=1,NMAX
READ (5,27) COE(N),COC(N)
26 CONTINUE
27 FORMAT (2E14.7)
BZPBT= BZRO + BETA
BZMBT= BZRO - BETA
XKBETA= XK*BETA

C
C*** DETERMINE SHORELINE COORDINATES (XI,ETA) IN TERMS OF A STRETCHED SHELF
C*** COORDINATE SYSTEM (S*,T*).
C*** S* AXIS IS PARALLEL TO XI AND IS REPRESENTATIVE OF COASTLINE
C*** ARCLENGTH.
C*** T* AXIS IS PARALLEL TO ETA AND IS REPRESENTATIVE OF LONG WAVE
C*** TRAVEL TIME.
C
C
C*** DETERMINE TRANSFORM GENERATED COASTLINE AND SEA BDY
C
N3=1
N4= 121
DELXI= XLAMD/(N4-1)

```

```

DO 85 I=N3,N4
  XID = (I-1)*DELXI
  CALL TRAN( XC,YC,XS,YS, XID )
  ATXB(I)= XC
  ATYB(I)= YC
  ATXA(I)= XS
  ATYA(I)= YS
  CONTINUE
  WRITE(6,29)
  WRITE(6,39)
  WRITE(6,79)
  CALL XUT( ATXB , ATYB , N3,N4 )
  WRITE(6,29)
  WRITE(6,49)
  WRITE(6,69)
  WRITE(6,79)
  CALL XUT( ATXA , ATYA , N3 , N4 )

C
C*** DETERMINE TRANSFORM GENERATED ARCLNGTH OF CCASTLINE AND SEA BDRY
C*** AS A FUNCTION OF (EVENLY SPACED) XI.
C
  Y2(1)= 0.
  X2(1)= 0.
  X2P(1)= C.
  DO 91 I=N3,N4
    Y2(I)= (I-1)*DELXI
    II= I+1
    IF( I .EQ. N4 ) GO TO 91
    DELX= ABS( ATXB(II)-ATXB(I) )
    DELY= ABS( ATYB(II)-ATYB(I) )
    X2(II)= SLMAP*SQRT( DELX*DELX + DELY*DELY )

```

```

X2(II)= X2(II) + X2(I)
DELX= ABS( ATXA(II)-ATXA(I) )
DELY= ABS( ATYA(II)-ATYA(I) )
X2P(II)= SLMAP*SORT( DELX*DELX + DELY*DELY )
X2P(II)= X2P(II) + X2P(I)
91  CONTINUE
    WRITE(6,29)
    WRITE(6,79)
    WRITE(6,89)
    CALL XUT( X2,Y2,N3,N4 )
    WRITE(6,29)
    WRITE(6,79)
    WRITE(6,99)
    CALL XUT( X2P,Y2,N3,N4 )
C 29  FORMAT( I1,/,/,46X,39HREGION---LAGUN #ADRE TC MARSH ISLAND )
39  FORMAT (/,/,55X,21HCOASTLINE COORDINATES,/)
40  FORMAT ( 62X,8HCRIGIAL,////)
49  FORMAT (/,/,51X,29HSEAWARD BOUNDARY COORDINATES)
50  FORMAT (53X,24H( 100 FM DEPTH CONTOUR ),/)
59  FORMAT (54X,23HINTERPCLATION BY SPLINE,////)
69  FORMAT( // )
79  FORMAT( 56X,19HTRANSFCRM GENERATED ,/// )
89  FORMAT( 50X,30HARCLENGTH,XI ALONG CCASTLINE,/// )
99  FORMAT( 47X,37HARCLENGTH,XI ALONG SEAWARD BOUNDARY,/// )
C
MQ= N4
CALL CURV1( SLP1,SLPN,SIGMA )
C
C  DETERMINE APPROPRIATE VALUES OF XI SUCH THAT DELTA S* IS CONSTANT.
    WRITE(6,29)

```

```

WRITE(6,113)
113 FORMAT(///.53X,33HSTRETCHED SHELF COORDINATE SYSTEM
          9/.39X,52HEVENLY SPACED IN S=STAR (DISTANCE PARALLEL TO COAST)
          9/.39X,57HAND EVENLY SPACED IN T=STAR (TRAVEL TIME NORMAL TO COAST)
          9,///)
C TOTAL OF IIC(IRG)=NUM OF INCREMENTS OF DEL S*. REMEMBER THERE ARE
C TWO EXTRA XI LINES= ONE AT EACH END OF THE GRID.
C USER SUPPLIES EXPANSION CCEFFS A,B,C FOR EACH REGION OF THE CURVE
C S=PAR= A+B*(S*)**C
C

```

```

IRG= 5
IIC(1)= 10
IIC(2)= 4
IIC(3)= 7
IIC(4)= 9
IIC(5)= 16
A(1)= 0.6058735E+03
B(1)= 0.5479735E+05
C(1)= 0.9044300E+00
A(2)= 0.1395315E+03
B(2)= 1.5
C(2)= 1.
A(3)= 0.4788464E+03
B(3)= 0.3028714E+07
C(3)= 0.1707694E+01
A(4)= 0.
B(4)= 1.
C(4)= 1.
A(5)= 0.2870103E+03
B(5)= 0.4707750E+11
C(5)= 0.5160192E+01

```



```

114 WRITE(6,114)
   FORMAT(20X,11HD S PL/D S* ,9X,6HS=STAR,7X,10HS=PARALLEL,11X,2HXI,
9//)
C
K2= 0
K1= 1
DO 120 I=1,IRG
  A1= A(I)
  B1= B(I)
  C1= C(I)
  WRITE(6,115) I,A1,B1,C1
115 FCRMAT(/,1X,7HREGION ,11,3X,6HA,B,C= ,3(2X,F14.7),//)
K2= K2+11C(I)
K3= K2+1
DO 119 J=K1,K3
  K=J
  XCUM= SSSTRT + (J-1)*DELS
  CALL CURVS( XCUM,SDUM,CDUM,A1,P1,C1 )
  XI(J)= CURV2( SDUM,SIGMA,K )
  WRITE(6,117) DDUM,XDUM,SDUM,XI(J),J
117 FORMAT( 30X,F8.4,10X,F6.1,9X,F6.1,9X,F6.1 , 4X,I2 )
119 CONTINUE
K1= K3
120 CONTINUE
C
C*** XI VALUES NOW KNOWN FOR EVENLY SPACED INCREMENTS OF S*.
C
C
C*** PROCEEDING TO FIND ETA VALUES FOR EVENLY SPACED INCREMENTS OF T*.
C
C*** DETERMINE ARCLENGTH ALONG A PARTICULAR ISCLINE OF XI ( XIDUM ).

```

```

C
DELETA= 2.0*BETA/(NS-1)
X2(1)= 0.
WRITE(6,29)
WRITE(6,79)
WRITE(6,999) XIDUM
FORMAT( 41X,33HARCLENGTH (N MI),ETA  ALCNG XI=  .F8.3,/// )
999 DO 94 J=1,NS
Y2(J) = -EETA + (J-1)*DELETA
CALL TRAN1( XDUM,YDUM, XIDUM,Y2(J) )
X2P(J)= XDUM
Y2P(J)= YDUM
IF( J .EQ. 1 ) GO TO 94
JJ= J-1
DELX= ABS( X2F(J)-X2P(JJ) )
DELY= ABS( Y2P(J)-Y2P(JJ) )
X2(J)= X2(JJ) + SLMAP*SQRT( DELX*DELX + DELY*DELY )
CONTINUE
94 DO 98 I=1,NS
WRITE(6,97) I,X2(I),Y2(I) ,X2P(I),Y2P(I)
FORMAT( 42X,I2,2X,F6.1,IH,,F7.3,10X,F6.1,1F,,F6.1 )
97 CONTINUE
98
C
MQ= NS
CALL CURV1( SLP1,SLPN,SIGMA )
C
C DETERMINE APPROPRIATE VALUES OF ETA SUCH THAT DELTA T* IS CONSTANT.
C
C READ WATER DEPTH (FM) AT ND PLACES EVENLY SPACED ALONG XI=XIDUM.
ND1= ND-1
DELS= X2(NS)/ND1

```

```

Y2P(I)= 0.
DO 123 I=1,ND
  READ(5,124) SY(I)
  J=I+1
  IF( I .EQ. ND ) GO TO 123
  Y2P(J)= Y2P(I) + DELS
123 CONTINUE
124 FORMAT( F8.2 )
C DETERMINE LONG WAVE TRAVEL TIME (MIN) ALONG XI=XIDUM.
  X2P(I)= 0.0
  DO 128 I=1,ND1
    J=I+1
    F1= 1.0/SQRT( G*SY(I)*6.0 )
    F2= 1.0/SQRT( G*SY(J)*6.0 )
    X2P(J)= X2P(I) + (F1+F2)*(Y2P(J)-Y2P(I))*50.0
128 CONTINUE
    TIME= X2P(ND)
  C
  C
  C
  WRITE(6,25)
  WRITE(6,131) XIDUM
131 FORMAT( 7CX,3HXI=F6.1,/,13X,8HD T/D T*,12X,6HT=STAR,6X,4HTIME,
    96X,8HS=NORMAL,8X,3HETA,10X,SHDEPTH, // )
  DO 133 I=1,ND
133 WRITE(6,134) X2P(I),Y2P(I),SY(I)
134 FORMAT( 42X,F6.1,6X,F6.1,21X,F6.1 )
  C
  C TOTAL OF IIC(IRG)=NUM CF INCRFMENTS OF DEL-T*.
  C EXPANSION CURVE= T= A+E*(T*)**C

```

C

```

IRG= 2
IIC(1)= 4
IIC(2)= 10
TIM1= IIC(1)*DELT
TIM2= IIC(2)*DELT
A(1)= 0.
C(1)= TIM1/(TIM-TIM2)
B(1)= (TIM-TIM2)*TIM1**(-C(1))
A(2)= TIM-TIM1-TIM2
B(2)=1.
C(2)=1.
IF( IIC(1)+1 .EQ. NUMETA ) DELT= TIM/(NUMETA-1)
IF( IIC(1)+1 .EQ. NUMETA ) B(1)=1.
IF( IIC(1)+1 .EQ. NUMETA ) C(1)=1.
WRITE(5,29)
WRITE(6,113)
WRITE(6,131) XDUM
K2= 0
K1= 1
DO 146 I=1,IRG
  A1= A(I)
  B1= B(I)
  C1= C(I)
  WRITE(6,115) I,A1,B1,C1
  K2= K2+IIC(I)
  K3= K2+1
DO 145 J=K1,K3
  K=J
  WDUM= (J-1)*DELT
  CALL CURV9( WDUM,XDUM,DDUM,A1,B1,C1 )

```

```

YDUM= CURV4( XDUM,SIGMA, K )
ZDUM= CURV2( YDUM,SIGMA,K )
ETA(J)= ZDUM
IF( J.EQ. 1 ) FTA(J)=BETA
IF( J.EQ. NUMETA ) ETA(J)= BETA
WRITE(6,143) DDUM,WDUM,XDUM,YDUM,ZDUM, J
143 FORMAT( 11X,F8.4,12X,F6.1,6X,F6.1,7X,F7.3,2X,I2 )
145 CONTINUE
KI= K3
146 CONTINUE
*****
C
C
C *** THE VALUES OF XI AND ETA ARE NOW DETERMINED PERMITTING OUTPUT/
C *** PUNCH OF ALL COMPUTING GRID DATA.
C
C X,Y GRID POINT LOCATIONS
C SCALE FACTOR MU (XI)
C SCALE FACTOR NU (ETA)
C SCALE FACTOR S (X,Y/XI,ETA)
C COS AND SIN THETA - ORIENTATION OF XI AXIS TO X AXIS
C
C
C *** COMPUTE X,Y COORDINATES OF GRID POINT LOCATIONS
C
C CALL SHRCOR( DFLSS,NUMXI, DELTT,NUMETA, SLMAP )
C
C PUNCH X,Y COORDINATES HERE AS READ IN PROGRAM SSURGE WITH NAME XX,YY.
C THESE COORDINATES ARE IN ARRAYS X,Y FOR I=2,3--NUMXI--1
C AND J=1,2--NUMETA
C
C

```



```

C*** COMPUTE SCALE FACTOR MU
C
      WRITE(6,200)
      FORMAT( 1H1, '//,50X,35H+HURRICANE CARLA COMPUTING GRID DATA      )
      WRITE(6,201)
      FCNMT( //,60X,15HSCALE FACTOR MU  ,// )
      DO 204 I=2,NUMXI1
      J=I-1
      SX(J)= ( XI(I+1)-XI(I-1) )/2./DELSS
      WRITE(6,202) J,SX(J)
      FORMAT( 60X,3HMU( .I2, 3H)= ,F14.7 )
      204 CONTINUE
C
C PUNCH MU HERE AS READ IN PROGRAM SSURGE WITH NAME DSDXI.
C MU IS IN ARRAY SX FOR I=1,2--NUMXI-2
C
C*** COMPUTE SCALE FACTOR NU
C
      WRITE(6,200)
      WRITE(6,210)
      FORMAT( //,60X,15HSCALE FACTOR NU  ,// )
      SY(1)= (ETA(2)-ETA(1))/DELT
      SY(NUMETA)= (ETA(NUMETA)-ETA(NUMET1))/DELT
      DO 214 J=1,NUMETA
      IF( J.EQ. 1 .OR. J.EQ. NUMETA ) GO TO 211
      SY(J)= (ETA(J+1)-ETA(J-1))/2./DELT
      WRITE(6,212) J , SY(J)
      FCNMT( 60X,3HNU( .I2, 3H)= ,F14.7 )
      214 CONTINUE
C

```

```

C PUNCH NU HERE AS READ IN PROGRAM SSURGE WITH NAME DTDET.
C NU IS IN ARRAY SY FOR J=1,2--NUMETA.
C
C
C *** COMPUTE SCALE FACTOR F AS READ IN PROGRAM SSURGE WITH NAME S.
C RECALL F IS SQRT CF AREA IN X,Y PLANE / MU*NU*DELS*DELT
C FIRST COMPUTE AREA OF EACH QUADRANGLE SUB-DIVIDED INTO
C IQUAD INTERVALS BETWEEN XI LINES AND JQUAD INTERVALS BETWEEN
C ETA LINES
C
C IQUAD= 4
C JQUAD= 2
C KCP= 1
C CALL TRAN2( KCP, 0., 0., 0., 0., 0., 0. )
C KOP= 2
C WRITE(6,200)
C WRITE(6,300)
C FORMAT(/,60X,14HSCALE FACTOR F ,// )
C DC 330 I=1,NUMXI
C DELXI= (XI(I+1)-XI(I))/IQUAD
C FRST= XI(I) +DELXI/2.
C DO 310 K=1,IQUAD
C X2(K)= FRST + (K-1)*DELXI
C DC 330 J=1,JQUAD
C DELETA= (ETA(J+1)-ETA(J))/JQUAD
C FRST= ETA(J) + DELETA/2.
C SUM= 0.
C DO 320 K=1,IQUAD
C DO 320 L=1,JQUAD
C DUMETA= FRST + (L-1)*DELETA
C CALL TRAN2( KOP,X2(K),DUMETA,0.,DF1,DF2 )

```

```

320     SUM = SUM + CF1*CF1 + CF2*CF2
      CONTINUE
330     X(I,J) = SUM*DELXI*DELETA
      CONTINUE
      FAC1 = 2.*DELSE*DELT
      FAC2 = 2.*FAC1
      N = NUMETA
      DO 370 I=1,NUMXI2
        Z(I,1) = SQR((X(I,1)+X(I+1,1))/FAC1/SX(I)/SY(1))
        Z(I,N) = SQR((X(I,N-1)+X(I+1,N-1))/FAC1/SX(I)/SY(N))
      DO 370 J=2,NUMET1
        Z(I,J) = SQR((X(I,J)+X(I+1,J)+X(I,J-1)+X(I+1,J-1))/FAC2/SX(I)/SY(J
          9))
370     CCNTINUE
      DO 390 J=1,NUMETA
        WRITE(6,381) J
381     FORMAT(//,10X,11HROW NUMBER ,I2,// )
        WRITE(6,382) ( I,2(I,J),I=1,NUMXI2 )
382     FORMAT( ,I4,2X,E14.7,4X))
390     CCNTINUE
C
C PUNCH F HERE AS READ IN PROGRAM SSURGE WITH NAME S. SCALE FACTOR F
C IS IN ARRAY Z FOR I=1,2--NUMXI-2 AND J=1,2--NUMETA
C
C
C*** COMPUTE COS AND SIN THETA - ORIENTATION OF XI AXIS TO X AXIS.
C RECALL, THETA IS A WEIGHTED AVERAGE.
C
      WRITE(6,200)
      WRITE(6,395)
395     FORMAT(//, 60X, 27HVALUES OF COS AND SIN THETA , // )

```

```

CC 400 I=1,NUMXI
XID= XI(I)
DO 400 J=1,NUMETA
ETAD= ETA(J)
CALL TRAN2( KCF,XID,ETAD, ANGLE,CF1,DF2 )
Z(I,J)= ATAN2( CF2,DF1 )
400 CONTINUE
N= NUMETA
DO 410 I=2,NUMXI1
K= I-1
X(K,1)= COS((Z(I-1,1)+2.*Z(I,2)+Z(I+1,1)+ 4.*Z(I,1))/8.)
Y(K,1)= SIN((Z(I-1,1)+2.*Z(I,2)+Z(I+1,1)+ 4.*Z(I,1))/8.)
X(K,N)= CCS((Z(I-1,N)+2.*Z(I,N-1)+Z(I+1,N)+4.*Z(I,N))/8.)
Y(K,N)= SIN((Z(I-1,N)+2.*Z(I,N-1)+Z(I+1,N)+4.*Z(I,N))/8.)
CO 410 J=2,NUMET1
X(K,J)= CCS((Z(I-1,J)+Z(I,J-1)+Z(I+1,J)+Z(I,J+1)+4.*Z(I,J))/8.)
Y(K,J)= SIN((Z(I-1,J)+Z(I,J-1)+Z(I+1,J)+Z(I,J+1)+4.*Z(I,J))/8.)
410 CONTINUE
DC 440 J=1,NUMETA
WRITE(6,381) J
WRITE(6,430) ( I,X(I,J),Y(I,J), I=1,NUMXI2)
430 FORMAT( 5(I3,2X,F8.5,1X,F8.5,4X))
440 CONTINUE
C
C PUNCH COS AND SIN THETA HERE AS READ IN PROGRAM SSURGE WITH
C NAMES COSG AND SING. THESE VALUES ARE IN ARRAYS X AND Y FOR
C I=1,2--NUMXI-2 AND J=1,2--NUMETA.
C
C STOP
C END
C SUBROUTINE XUT( X,Y,N1,N2 )

```

```

10 DIMENSION X(1000) , Y(1000)
11 M= N2-N1+1
    M14= M/4
    M4= M14*4
    IADD= M-M4
    DC 10 I=N1,M14
    J= I+M14
    K= J+M14
    L= K+M14
    WRITE(6,11) I,X(I),Y(I),J,X(J),K,X(K),L,X(L),Y(L)
    FORMAT( 4(6X,I4,2X,F6.1,1X,1H,,1X,F6.1,6X) )
    IF( IADD .EQ. 0 ) GC TO 25
    IF( IADD .EQ. 1 ) NUM1= N2
    IF( IADD .EQ. 2 ) NUM1= N2-1
    IF( IADD .EQ. 3 ) NUM1= N2-2
    DO 20 I=NUM1,N2
20 WRITE(6,21) I,X(I),Y(I)
21 FORMAT( 105X,I4,2X,F6.1,1X,1H,,1X,F6.1,6X )
25 CONTINUE
    RETURN
    END
    SUBROUTINE SHRCOR( DFLXI,NLUMXI, DELETA,NUMETA,SLMAP )
    DIMENSION XI(47) , ETA(15) , X(47,15) , Y(47,15)
    DIMENSION SX(100) , SY(100)
    COMMON/XIETAY/ XI,ETA,X,Y
    COMMON/SXY/ SX,SY
    NLMPG= NLUMXI/5
    IADD= NLUMXI-5*NLMPG
    NPAGE= 1
    DO 40 I=1,NLUMXI
    DO 40 J=1,NUMETA

```



```

CALL TRAN1( XDUM,YDUM,XI(I),ETA(J) )
X(I,J)= XCUM
Y(I,J)= YDUM
CONTINUE
CONTINUE

40
55
WRITE(6,900) DELXI , DELETA

N1= NPAGE*5 -4
N2= NPAGE*5
IF( N2 .GT. NUMXI ) GO TO 80
IF( NUNPG .EQ. 0 ) GO TO 80
I1= N1
I2= N1+1
I3= N1+2
I4= N1+3
I5= N1+4
WRITE(6,903) XI(I1),XI(I2),XI(I3),XI(I4),XI(I5),I1,I2,I3,I4,I5
DO 70 K=1,NUMETA
J= NUMETA-K+1
JJ= J-1
DC 60 I=N1,N2
IF( I .EQ. NUMXI ) GO TO 62
I1= I+1
DELX= ABS( X(I1,J)-X(I,J) )
DELY= ABS( Y(I1,J)-Y(I,J) )
SX(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
CONTINUE
CONTINUE
60
62
IF( IACC .EQ. 0 .AND. N2 .EQ. NUMXI ) GO TO 64
WRITE(6,904) ETA(J),X(I1,J),Y(I1,J),SX(I1,J),X(I2,J),Y(I2,J),SX(I2,J),
9X(I3,J),Y(I3,J),SX(I3,J),X(I4,J),Y(I4,J),SX(I4,J),X(I5,J),Y(I5,J)
9SX(I5), J

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```

64      GC TO 66
        CONTINUE
        WRITE(6,905) ETA(J),X(I1,J),Y(I1,J),SX(I1),X(I2,J),Y(I2,J),SX(I2),
9X(I3,J),Y(I3,J),SX(I3),X(I4,J),Y(I4,J),SX(I4),X(I5,J),Y(I5,J), J
66      CONTINUE
        IF( K .EQ. NUMETA ) GO TO 70
        DO 68 I=N1,N2
        DELX= ABS( X(I,JJ)-X(I,J) )
        DELY= ABS( Y(I,JJ)-Y(I,J) )
        SY(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
68      CONTINUE
        WRITE(6,906) SY(I1),SY(I2),SY(I3),SY(I4),SY(I5)
70      CONTINUE
        IF( IADD .EQ. 0 .AND. N2 .EQ. NUMXI ) GO TO 150
        NPAGE= NPAGE + 1
        GC TO 55
80      CONTINUE
        IF( IADD .EQ. 1 ) GO TO 100
        IF( IADD .EQ. 2 ) GO TO 110
        IF( IADD .EQ. 3 ) GO TO 120
        IF( IADD .EQ. 4 ) GO TO 130
100      CCNTINUE
        I1= N1
        I= I1
        WRITE(6,910) X(I1),I1
        DO 102 K=1,NUMETA
        J= NUMETA-K+1
        JJ= J-1
        WRITE(6,911) X(I1,J),Y(I1,J)
        IF( K .EQ. NUMETA ) GO TO 102
        DELX= ABS( X(I,JJ)-X(I,J) )

```

```

      DELY= ABS( Y(I,JJ)-Y(I,J) )
      SY(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
      WRITE(6,912) SY(I1)
      CCNTINUE
      GO TO 150
110  CONTINUE
      I1= N1
      I2= N1+1
      WRITE(6,914) XI(I1),XI(I2),I1,I2
      DC 114 K=1,NUMETA
      J= NUMETA-K+1
      JJ= J-1
      DELX= ABS( X(I2,J)-X(I1,J) )
      DELY= ABS( Y(I2,J)-Y(I1,J) )
      SX(I1)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
      WRITE(6,915) X(I1,J),Y(I1,J),SX(I1),X(I2,J),Y(I2,J)
      IF( K .EQ. NUMETA ) GO TO 114
      DC 112 I=I1,I2
      DELX= ABS( X(I,JJ)-X(I,J) )
      DELY= ABS( Y(I,JJ)-Y(I,J) )
      SY(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
      CONTINUE
      WRITE(6,916) SY(I1),SY(I2)
      CCNTINUE
      GO TO 150
120  CONTINUE
      I1= N1
      I2= N1+1
      I3= N1+2
      WRITE(6,917)XI(I1),XI(I2),XI(I3),I1,I2,I3
      CC 128 K=1,NUMETA

```

```

J= NUMETA-K+1
JJ= J-1
DO 122 I=11,13
IF( I .EQ. NUMXI ) GO TO 124
II= I+1
DELX= ABS( X(II,J)-X(I,J) )
DELY= ABS( Y(II,J)-Y(I,J) )
SX(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
122 CONTINUE
124 CONTINUE
WRITE(6,918) ETA(J),X(11,J),Y(11,J),SX(11,J),X(12,J),Y(12,J),SX(12,J),
9X(13,J),Y(13,J), J
IF( K .EQ. NUMETA ) GO TO 128
DO 126 I=11,13
DELX= ABS( X(I,JJ)-X(I,J) )
DELY= ABS( Y(I,JJ)-Y(I,J) )
SY(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
126 CONTINUE
WRITE(6,919) SY(11),SY(12),SY(13)
128 CONTINUE
GO TO 150
130 CONTINUE
I1= N1
I2= N1+1
I3= N1+2
I4= N1+3
WRITE(6,921) XI(11),XI(12),XI(13),XI(14),I1,I2,I3,I4
DO 138 K=1,NUMETA
J= NUMETA-K+1
JJ= J-1
DO 132 I=11,14

```

```

132 IF( I .EQ. NUMXI ) GO TO 134
133 I= I+1
      DELX= ABS( X(II,J)-X(I,J) )
      DELY= ABS( Y(II,J)-Y(I,J) )
      SX(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
132 CONTINUE
134 CONTINUE
      WRITE(6,922) ETA(J),X(II,J),Y(II,J),SX(II,J),Y(12,J),SX(12,J),
9X(13,J),Y(13,J),SX(13,J),X(14,J),Y(14,J),J
      IF( K .EQ. NUMETA ) GO TO 138
      CC 136 I=11,I4
      DELX= ABS( X(I,JJ)-X(I,J) )
      DELY= ABS( Y(I,JJ)-Y(I,J) )
      SY(I)= SLMAP*SQRT( DELX*DELX + DELY*DELY )
136 CONTINUE
      WRITE(6,923) SY(11),SY(12),SY(13),SY(14)
138 CONTINUE
150 CONTINUE
900 FORMAT( 1F1.4X,3SPRECISION==LAGUNA MADRE TO MARSH ISLAND
9// ,55X,21HSHORELINE COORDINATES
9//,58X,16HURRICANE CARLA
9// ,46X,10HDELTA-S= ,F6.3,6X,10HDELTA-T= ,F6.3, ///
903 FORMAT( 2X,5(14X,3HXI=,F7.2),/ ,5(19X,1P(,12,1H),1X),//
904 FORMAT( 1X,4HETA=,F7.3,2X,F6.1,1H,,F6.1
, 94(3X,F4.1,4X,F6.1,1H,,F6.1), 2X,F4.1,/ ,5X,1P(,12,1H)
905 FORMAT( 1X,4HETA=,F7.3,2X,F6.1,1H,,F6.1
94(3X,F4.1,4X,F6.1,1P,,F6.1), / ,5X,1H(,12,1H)
906 FORMAT( 5(18X,F4.1,2X),/
910 FORMAT( 16X,3HXI=,F7.2,/ ,19X,1H(,12,1H),//
911 FORMAT( 14X,F6.1,1P,,F6.1,/
912 FORMAT( 18X,F4.1,/

```



```

914 FCRMAT( 2X,2(14X,3HXI=F7.2),/ 2(19X,1F(,I2,1H),1X),//
915 FORMAT( 14X,F6.1,1H,,F6.1,3X,F4.1,4X,F6.1,1H,,F6.1, /
916 FCRMAT( 2(18X,F4.1,2X),/
917 FORMAT( 2X,3(14X,3HXI=F7.2),/ 3(19X,1F(,I2,1H),1X),//
918 FORMAT( 1X,4PETA=F7.3,2X,F6.1,1H,,F6.1
92(3X,F4.1,4X,F6.1,1F,,F6.1), / 5X,1F(,I2,1H)
919 FORMAT( 3(18X,F4.1,2X),/
921 FCRMAT( 2X,4(14X,3HXI=F7.2),/ 4(19X,1H(,I2,1H),1X),//
922 FORMAT( 1X,4PETA=F7.3,2X,F6.1,1H,,F6.1
93(3X,F4.1,4X,F6.1,1H,,F6.1), / 5X,1H(,I2,1H)
923 FCRMAT( 4(18X,F4.1,2X),/
RETURN
END
SUBROUTINE TRAN( XCST,YCST,XSEA,YSEA,XI )
DIMENSION COB(200), CCC(200)
COMMON/ED/ XKBETA,BZPBT,BZMHT
COMMON/FCRIA/ (CB,CCC,EZRC,XK,NMAX
XCST= 0.
YCST= 0.
XSEA= 0.
YSEA= 0.
XKXI= XKXI
DO 10 N=1,NMAX
XN=N
XNKBT= XN*XKEETA
XNKXI= XN*XKXI
CSH= COSH( XNKBT )
SNH= SINH( XNKBT )
A= COC(N)*CSH
B= COB(N)*SNH
C= CCC(N)*SNH

```

```

D= CCE(N)*CSH
E= SIN( XNKXI )
F= COS( XNKXI )
XCST= XCST + (A+E)*E
XSEA= XSEA + (A-B)*E
YCST= YCST + ( D+C)*F
YSEA= YSEA + ( D-C)*F
CONTINUE
XCST= XCST + XI
XSEA= XSEA + XI
YCST= YCST + BZPBT
YSEA= YSEA + EZMBT
RETURN
END
SUBROUTINE TRAN1( XDUM , YDUM , XI , ETA )
DIMENSION CCB(200), CCC(200)
COMMON/FORIA/ CCB,CCC,BZRC,XK,NMAX
XDUM= 0.
YDUM= 0.
XKXI= XK*XI
XKETA= XK*ETA
DO 10 N=1,NMAX
XN=N
XNKBT= XN*XKETA
XNKXI= XN*XKXI
CSH= CCSI( XNKET )
SNH= SINH( XNKBT )
A= CCB(N)*CSH
B= CCB(N)*SNH
C= CCB(N)*SNH
D= CCE(N)*CSH

```

10

```

E= SIN( XNKXI )
F= COS( XNKXI )
XDUM= XDUM + (A+B)*E
YDUM= YDUM + ( C+C)*F
CONTINUE
10 XDUM= XDUM + XI
YDUM= YDUM + EZRO + ETA
RETURN
END
SUBROUTINE TRAN2( KOP,XI,ETA,ANGLE,DXDXI,DYDYI )
DIMENSION COB(200) , CCC(200) , XNK(200)
COMMON/FORIA/CCB,COB,BZRC,XK,NMAX
IF(KOP.EQ.1)GC TO 100
GC TO 200
100 DO 105 N=1,NMAX
XN= N
XNK(N)= XN*XK
GO TO 999
200 DXDXI= 1.
DYDYI= 0.
CO 205 N=1,NMAX
XNKETA= XNK(N)*ETA
XNKXI= XNK(N)*XI
SNH= SIN( XNKETA )
CSH= COS( XNKETA )
DXDXI= DXDXI+XNK(N)*((CCB(N)*SNH+CCC(N)*CSH)*CCS(XNKXI))
DYDYI= DYDYI-XNK(N)*((COB(N)*CSH+CCC(N)*SNH)*SIN(XNKXI))
205 CONTINUE
IF( KOP.EQ.2) GC TO 999
ANGLE= ATAN2(DYDYI,DXDXI)
999 RETURN

```

```

END
SUBROUTINE CURVS( XDUM,Y,Y1,A,B,C )
Z= ABS( XDUM )
W= ABS( C-1. )
Y1= B
Y= A+B*(XDUM)**C
IF( Z .LT. 0.0001 .OR. W .LT. 0.001 ) GO TO 10
Y1= B*C*(XDUM)**(C-1.)
CONTINUE
RETURN
END
10
SUBROUTINE CURV1( SLP1 , SLPN , SIGMA )
C
DIMENSION X2(1000) , Y2(1000)
DIMENSION R(800) , S(800)
COMMON/YF/ X2, Y2 , WC
COMMON/JOHN1/ R
COMMON/JOHN2/ S
C*****
C THIS SUBROUTINE DETERMINES THE PARAMETERS NECESSARY TO
C COMPUTE AN INTERPOLATORY SPLINE UNDER TENSION THROUGH
C A SEQUENCE OF FUNCTIONAL VALUES. THE SLOPES AT THE TWO
C ENDS OF THE CURVE MAY BE SPECIFIED OR OMITTED. FOR ACTUAL
C COMPUTATION OF POINTS ON THE CURVE IT IS NECESSARY TO CALL
C THE FUNCTION CURV2.
C*****
C ON INPUT--

```

```

C
C N= MC IS THE NUMBER OF VALUES TO BE INTERPOLATED ( .GE. 2)
C X2 IS AN ARRAY OF N INCREASING ABSCISSAE OF THE FUNCTIONAL VALUES
C Y2 IS AN ARRAY OF N ORDINATES OF THE VALUES
C I.E. Y2(K) IS THE FUNCTIONAL VALUES CORRESPONDING TO X2(K).
C R IS AN ARRAY OF LENGTH AT LEAST N ( PERMANENT STORAGE )
C S IS AN ARRAY OF LENGTH AT LEAST N ( SCRATCH STORAGE ).
C
C SLP1 AND SLPN CONTAIN THE DESIRED VALUES FOR THE FIRST
C DERIVATIVE OF THE CURVE AT X2(1) AND X2(N), RESPECTIVELY.
C IF THE QUANTITY SIGMA IS NEGATIVE THESE VALUES WILL BE
C DETERMINED INTERNALLY AND THE USER NEED ONLY FURNISH
C PLACE-HOLDING PARAMETERS FOR SLP1 AND SLPN. SUCH PLACE-
C HOLDING PARAMETERS WILL BE IGNORED BUT NOT DESTROYED.
C
C SIGMA CONTAINS THE TENSION FACTOR. THIS IS NON-ZERO AND
C INDICATES THE CURVINESS DESIRED. IF ABS(SIGMA) IS NEARLY
C ZERO (E.G. .001) THE RESULTING CURVE IS APPROXIMATELY A
C CUBIC SPLINE. IF ABS(SIGMA) IS LARGE (E.G. 50.) THE
C RESULTING CURVE IS NEARLY A POLYGONAL LINE. THE SIGN
C OF SIGMA INDICATES WHETHER THE DERIVATIVE INFORMATION
C HAS BEEN INPUT OR NOT. IF SIGMA IS NEGATIVE THE ENDPOINT
C DERIVATIVES WILL BE DETERMINED INTERNALLY. A STANDARD
C VALUE FOR SIGMA IS APPROXIMATELY 1. IN ABSOLUTE VALUE.
C
C
C CN OUTPUT --
C
C R CONTAINS VALUES PROPORTIONAL TO THE SECOND DERIVATIVE
C OF THE CURVE AT THE GIVEN NODES ( X2,Y2 ) .
C

```



```

C      N (MG), X2, Y2, SLF1, SLFN, SIGMA ARE UNALTERED.
C
C
C
C
C      N = MG
C      NM1 = N-1
C      NP1 = N+1
C      DELX1 = X2(2)-X2(1)
C      DX1 = (Y2(2)-Y2(1))/DELX1
C
C      DETERMINE SLOPES IF NECESSARY
C
C      IF (SIGMA.LT.0.) GO TO 5
C      SLPP1 = SLF1
C      SLPPN = SLFN
C
C      DENORMALIZE TENSION FACTOR
C
C      1 SIGMAP = AES(SIGMA)*(N-1)/(X2(N)-X2(1))
C
C      SET UP RIGHT HAND SIDE AND TRIDIAGONAL SYSTEM FOR R AND
C      PERFORM FORWARD ELIMINATION
C
C      DELS = SIGMAP*DELX1
C      EXPS = EXP(DELS)
C      SINHS = .5*(EXPS+1./EXPS)
C      SINHN = 1./((DELX1*SINHS)
C      DIAG1 = SINHN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
C      DIAGN = 1./DIAG1
C      R(1) = DIAGN*(DX1-SLPP1)

```

```

C      SPDIAG = SINHIN*(SINHS=DELS)
C      S(1) = CIACIN*SPCIAG
C      IF (N.EQ.2) GO TO 3
C
C      DC 2 I = 2,NM1
C      DELX2 = X2(I+1)-X2(I)
C      DX2 = (Y2(I+1)-Y2(I))/DELX2
C      DELS = SIGMAP*DELX2
C      EXPS = EXF(DELS)
C      SINHS = .5*(EXPS-1./EXPS)
C      SINHIN = 1./((DELX2*SINHS)
C      DIAG2 = SINHIN*(DELS*(.5*(EXPS+1./EXPS))-SINHS)
C      DIAGIN = 1./((DIAG1+DIAG2-SPDIAG* S(I-1))
C      R(1) = CIACIN*(CX2-CX1-SPCIAG* R(I-1))
C      SPDIAG = SINHIN*(SINHS=DELS)
C      S(I) = CIACIN*SPCIAG
C      DX1 = DX2
C      DIAG1 = DIAG2
C
C      2 DIAGIN = 1./((DIAG1-SPCIAG* S(NM1))
C      R(N) = DIAGIN*(SLPPN-DX2-SPDIAG* R(NM1))
C
C      PERFORM BACK SUBSTITUTION
C
C      DC 4 I = 2,N
C      IBAK = NF1-I
C      4 R(IBAK) = R(IRAK)- S(IRAK)* R(IBAK+1)
C
C      RETURN
C

```

```

C
5 IF (N.EQ.2) GO TO 6
C
C IF NO DERIVATIVES ARE GIVEN USE SECCND ORDER POLYNOMIAL
C INTERPOLATION ON INPLT DATA FOR VALUES AT ENDPONITS.
C
DELX2 = X2(3)-X2(2)
DELX12 = X2(3)-X2(1)
C1 = -(DELX12+DELX1)/DELX12/DELX1
C2 = DELX12/DELX1/DELX2
C3 = -DELX1/DELX12/DELX2
SLPP1 = C1*Y2(1) + C2*Y2(2) + C3*Y2(3)
DELN = X2(N)-X2(NM1)
DELNM1 = X2(NM1)-X2(N-2)
DELNN = X2(N)-X2(N-2)
C1 = (DELNN+DELN)/DELNN/DELN
C2 = -DELNN/DELN/DELNM1
C3 = DELN/DELNN/DELNM1
SLPPN = C3*Y2(N-2) + C2*Y2(NM1) + C1*Y2(N)
GC TO 1
C
C IF ONLY TWO POINTS AND NO DERIVATIVES ARE GIVEN, USE
C STRAIGHT LINE FOR CURVE
C
6 R(1) = 0.
R(2) = 0.
C
RETURN
END
FUNCTION CURV2( T , SIGMA , IT )
C

```

```

      DIMENSION X2(1000) , Y2(1000)
      DIMENSION R(800)
      COMMON/YB/ X2, Y2 , MC
      COMMON/JOHN1/ R

```

```

C *****
C
C THIS FUNCTION INTERPOLATES A CURVE AT A GIVEN POINT
C USING A SPLINE UNDER TENSION. THE SUBROUTINE CURV1 SHOULD
C BE CALLED EARLIER TO DETERMINE CERTAIN NECESSARY
C PARAMETERS.
C
C *****
C ON INPUT--
C
C T (X-COORD) CONTAINS A REAL VALUE TO BE MAPPED ONTO THE CURVE
C N= (MQ) IS THE NUMBER OF POINTS WHICH WERE INTERPOLATED TO
C DETERMINE THE CURVE.
C X2,Y2 ARE ARRAYS CONTAINING THE ABSCISSAS AND ORDINATES OF THE
C ORIGINAL INTERPOLATED POINTS.
C R IS AN ARRAY WITH VALUES PROPORTIONAL TO THE SECOND
C DERIVATIVE OF THE CURVE AT THE NODES (X2,Y2) .
C SIGMA CONTAINS THE TENSION FACTOR (ITS SIGN IS IGNORED)
C
C IT IS AN INTEGER SWITCH. IF IT IS NOT 1 THIS INDICATES
C THAT THE FUNCTION HAS BEEN CALLED PREVIOUSLY (WITH N,X2,
C Y2,R, AND SIGMA UNALTERED) AND THAT THIS VALUE OF T
C EXCEEDS THE PREVIOUS VALUE. WITH SUCH INFORMATION THE
C FUNCTION IS ABLE TO PERFORM THE INTERPOLATION MUCH MORE
C RAPIDLY. IF A USER SEEKS TO INTERPOLATE AT A SEQUENCE

```

```

C OF POINTS, EFFICIENCY IS GAINED BY ORDERING THE VALUES
C INCREASING AND SETTING IT TO THE INDEX OF THE CALL.
C IF IT IS 1 THE SEARCH FOR THE INTERVAL (X2(K),X2(K+1))
C CONTAINING T STARTS WITH K=1.
C
C THE PARAMETERS N (MQ), X2, Y2, R, AND SIGMA SHOULD BE INPUTTED
C UNALTERED FROM THE OUTPUT OF CURV1 AND THESE ARE UNALTERED IN CURV2 .
C
C CN OUTPUT--
C
C CURV2 (=Y=COORD) CONTAINS THE INTERPOLATED VALUE.
C FOR T .LT. X2(1), CURV2= Y2(1). FOR T .GT. X2(N),CURV2= Y2(N).
C
C
C N= MQ
C
C DENORMALIZE SIGMA
C S = X2(N)-X2(1)
C SIGMAP = AES(SIGMA)*(N-1)/S
C
C IF IT.NF.1 START SEARCH WHERE PREVIOUSLY TERMINATED,
C OTHERWISE START FROM BEGINNING
C
C IF (IT.EQ.1) I1 = 2
C
C SEARCH FOR INTERVAL
C
C 1 DO 2 I = I1,N
C   IF( X2(I)-T ) 2,2,3
C 2 CONTINUE

```



```

C
      I = N
C CHECK TO INSURE CORRECT INTERVAL
C
      3 IF( X2(I-1) .LE. T .OR. T .LE. X2(1) ) GO TO 4
C
C RESTART SEARCH AND RESET I1
C ( INPUT ..IT.. WAS INCORRECT )
C
      I1 = 2
      GO TO 1
C
C SET UP AND PERFORM INTERPOLATION
C
      4 DEL1 = T-X2(I-1)
      DEL2 = X2(I)-T
      DELS = X2(I)-X2(I-1)
      EXPS1 = EXP(SIGMAP*DEL1)
      SINHD1 = .5*(EXPS1-1./EXPS1)
      EXPS = EXP(SIGMAP*DEL2)
      SINHD2 = .5*(EXPS-1./EXPS)
      EXPS = EXPS1*EXPS
      SINHS = .5*(EXPS-1./EXPS)
      CURV2 = ( R(I)*SINHD1+ R(I-1)*SINHD2)/SINHS+((Y2(I)-R(I))*DEL1
      9(Y2(I-1) - R(I-1))*DEL2 )/DELS
C
      I1 = I
      RETURN
      END
SUBROUTINE CURVE( SLP1 , SLPN , SIGMA )
DIMENSION X2F(1000) , Y2P(1000)

```

```

      DIMENSION V(800) , S(800)
      COMMON/JCHN2/ S
      COMMON/JOHN4/ V
      COMMON /YA/ X2P,Y2P,MQP

```

```

C *****
C THIS SUBROUTINE DETERMINES THE PARAMETERS NECESSARY TO
C COMPUTE AN INTERPOLATORY SPLINE UNDER TENSION T816UGH
C A SEQUENCE OF FUNCTIONAL VALUES. THE SLOPES AT THE TWO
C ENDS OF THE CURVE MAY BE SPECIFIED OR OMITTED. FOR ACTUAL
C COMPUTATION OF POINTS ON THE CURVE IT IS NECESSARY TO CALL
C THE FUNCTION CURV4.
C *****
C ON INPUT==
C
C N= MQP IS THE NUMBER OF VALUES TO BE INTERPOLATED ( .GE. 2)
C X2P IS AN ARRAY OF N INCREASING ABSCISSAE OF THE FUNCTIONAL VALUES
C Y2P IS AN ARRAY OF N ORDINATES OF THE VALUES
C V IS AN ARRAY OF LENGTH AT LEAST N (PERMANENT STORAGE )
C S IS AN ARRAY OF LENGTH AT LEAST N ( SCRATCH STORAGE ).
C ON OUTPUT==
C
C V CONTAINS VALUES PROPORTIONAL TO THE SECOND DERIVATIVE
C OF THE CURVE AT THE GIVEN NODES ( X2P,Y2P )
C
C N(MQP), X2P,Y2P,SLP1, SLPN, SIGMA ARE UNALTERED.
C

```

```

N= MQP
NM1 = N-1
NP1 = N+1
DELX1 = X2P(2)-X2P(1)
CX1 = (Y2F(2)-Y2P(1))/DELX1
IF (SIGMA.LT.0.) GO TC 5
SLPP1 = SLPI
SLPFN = SLFN
1 SIGMAP = APS(SIGMA)*(N-1)/(X2P(N)-X2P(1))
DELS = SIGMAP*DELX1
EXPS = EXP(DELS)
SINHS = .5*(EXPS+1./EXPS)
SINHIN = 1./(DELX1*SINHS)
DIAG1 = SINHIN*(DELS*.5*(EXPS+1./EXPS)-SINHS)
DIAGIN = 1./DIAG1
V(1) = DIAGIN*(DX1-SLPP1)
SPDIAG = SINHIN*(SINHS-DELS)
S(1) = DIAGIN*SPDIAG
IF (N.EG.2) GO TC 3
DO 2 I = 2,NM1
  DELX2 = X2P(I+1)-X2P(I)
  DX2 = (Y2F(I+1)-Y2P(I))/DELX2
  DELS = SIGMAP*DELX2
  EXPS = EXP(DELS)
  SINHS = .5*(EXPS+1./EXPS)
  SINHIN = 1./(DELX2*SINHS)
  DIAG2 = SINHIN*(DELS*(.5*(EXPS+1./EXPS))-SINHS)
  DIAGIN = 1./(DIAG1+DIAG2-SPDIAG* S(I-1))
  V(I) = DIAGIN*(DX2-DX1-SPDIAG* V(I-1))
  SPDIAG = SINHIN*(SINHS-DELS)
  S(I) = DIAGIN*SPDIAG

```

```

DX1 = DX2
2  DIAG1 = CIAG2
3  DIAGIN = 1./(CIAG1-SPCIAG* S(NM1))
V(N) = DIAGIN*(SLPPN-DX2-SPDIAG* V(NM1))
DC 4 I = 2,N
      IBAK = NP1-1
4  V(IBAK) = V(IBAK)- S(IBAK)* V(IBAK+1)
      RETURN
5  IF (N.EQ.2) GO TO 6
DELX2 = X2P(3)-X2P(2)
DELX12 = X2P(3)-X2P(1)
C1 = -(DELX12+DELX1)/DELX12/DELX1
C2 = DELX12/DELX1/DELX2
C3 = -DELX1/DELX12/DELX2
SLPP1 = C1*Y2P(1) + C2*Y2P(2) + C3*Y2P(3)
DELN = X2F(N)-X2P(NM1)
DELN1 = X2F(NM1)-X2P(N-2)
DELN = X2P(N)-X2P(N-2)
C1 = (DELN+DELN)/DELN/DELN1
C2 = -DELN/DELN/DELN1
C3 = DELN/DELN/DELN1
SLPPN = C3*Y2F(N-2) + C2*Y2P(NM1) + C1*Y2P(N)
GO TO 1
6  V(1) = 0.
V(2) = C.
      RETURN
END
FUNCTION CURV4( T , SIGMA , IT )
DIMENSION X2P(1000) , Y2P(1000)
DIMENSION V(800)

```

C

```

COMMON/JCHN4/ V
COMMON /YA/ X2P,Y2P,MGP
C *****
C THIS FUNCTION INTERPOLATES A CURVE AT A GIVEN POINT
C USING A SPLINE UNDER TENSION. THE SUBROUTINE CURV3 SHOULD
C BE CALLED EARLIER TO DETERMINE CERTAIN NECESSARY PARAMETERS.
C *****
C *****
C ON INPUT==
C T (X=COORD) CONTAINS A REAL VALUE TO BE MAPPED ONTO THE CURVE
C N= MGP IS THE NUMBER OF POINTS WHICH WERE INTERPOLATED TO
C DETERMINE THE CURVE.
C X2P,Y2P ARE ARRAYS CONTAINING THE ABSCISSAS AND ORDINATES OF THE
C ORIGINAL INTERPOLATED POINTS.
C V IS AN ARRAY WITH VALUES PROPORTIONAL TO THE SECOND
C DERIVATIVE OF THE CURVE AT THE NODES ( X2P,Y2P ).
C THE PARAMETERS N(MGP),X2P,Y2P, V AND SIGMA SHOULD BE INPUTTED
C UNALTERED FROM THE OUTPUT OF CURV3 AND THESE ARE UNALTERED IN CURV4 .
C ON OUTPUT==
C CURV4 (Y=COORD) CONTAINS THE INTERPOLATED VALUE.
C
C N= MGP
C S = X2P(N)-X2P(1)
C SIGNAP = AES(SIGMA)*(N-1)/S

```



```

IF (IT.EQ.1) I1 = 2
1 DC 2 I = I1,N
IF( X2P(I)-T ) 2,2,3
2 CONTINUE
I = N
3 IF( X2P(I-1) .LE. T .CR. T .LE. X2P(1) ) GC TC 4
I1 = 2
GC TO 1
4 CEL1 = T-X2P(I-1)
CEL2 = X2P(I) - T
DELS = X2P(I)-X2P(I-1)
EXPS1 = EXP(SIGMAP*DEL1)
SINH1 = .5*(EXFS1-1./EXPS1)
EXPS = EXP(SIGMAP*DEL2)
SINH2 = .5*(EXPS-1./EXPS)
EXPS = EXFS1*EXPS
SINHS = .5*(EXPS-1./EXPS)
CURV4 = ( V(I)*SINH1+ V(I-1)*SINH2)/SINH5+((Y2P(I)-V(I))*DEL1 +
9(Y2P(I-1) -V(I-1))*CEL2 )/DELS
I1 = I
RETURN
END
FUNCTION COSH(XDAM)
YDAM = XDAM
COSH= EXP(XDAM) + EXP(YDAM)
COSH= COSH/2.0
RETURN
END
FUNCTION SINH(XDAM)
YDAM = XDAM
SINH= EXP(XDAM) - EXP(YDAM)
SINH= SINH/2.0
RETURN
END

```

APPENDIX C

FORTRAN Listing of Program SSURGE

C

SSURGE

COMMON/BLK2/C2,CC,C1X1,C1ETA,DX1,DETA,DELT,F,IM,JM, IMM,JMM, N

COMMON /BLK20/ CCRI0,CS,C3,C4,ROT,IMM2,IMM3,JMM2

COMMON/BLK3/ GRAV, NMAX,IH1,JH1,IT1,IT1,IH2,

1 JH2,IT2,JT2,IH3,JH3,IT3,JT3,IH4,JH4,IT4,JT4,INC

COMMON/BLK6/IH5,JH5,IT5,JT5,IH6,JH6,IT6,JT6

COMMON /HURRI/ YRANCE ,THIT ,XHIT ,YHIT ,

3 C10 ,C11 ,PHI ,

4 NT1 ,NT2 , PINF ,IX ,IY

5 DATA IM,JM, NMAX,INC/

1 45,15, 1321, 10/

DATA DX1, DETA, DELT, GRAV, F/

1 13081.3,17441.7, 180.0, 9.8,.0025/

DATA IH1,JH1,IT1,JT1,IH2,JH2,IT2,JT2/

1 18, 15, 18, 14, 10, 15, 10, 14/

DATA IH3,JH3,IT3,JT3,IH4,JH4,IT4,JT4/

1 16, 15, 16, 14, 32, 15, 32, 14/

DATA IH5, JH5, IT5, JT5, IH6, JH6, IT6, JT6/

1 36, 15, 36, 14, 38, 15, 38, 14/

C

IMM=IM=1

IMM2 = IM=2

IMM3 = IM=3

JMM=JM=1

JMM2=JM=2

CORIO= 6.70875E-05

CC=SQRT(GRAV*DELT)

CS = SQRT (GRAV*3048.)

C2=2.0*DELT

C3 = CORIO*DELT

```

C4 = C3*C3
ROT = C3
CIXI=GRAV*DELT/DXI
CIETA=GRAV*DELT/DETA

```

C

```

IX=IM
IY=JM
XMIT=160.
YMIT=168.
THIT=49.35
YRANGE=17.
PHI=20.
PINF=1016.
DEGRAD=3.141593/180.
C10=COS(PHI*DEGRAD)
C11=SIN(PHI*DEGRAD)

```

C

```

CALL ZERO
CALL FIELD
DO 100 N=1,NMAX
IF((N/2)*2.EQ.N)GC TO 30
CALL WINDF
CALL ELEV
CALL DRAW1
GO TO 100
30 CONTINUE
CALL FLUX
100 CONTINUE
CALL HUV
STOP
END

```



```

100 CONTINUE
   NDEX= NMAX/INC+1
   DO 200 K=1,NDEX
     HYD1(K)=0.0
     HYD2(K)=0.0
     HYD3(K)=0.0
     HYD4(K)=0.0
     HYD5(K)=0.0
     FYD6(K)=0.0
     UCM1(K)=0.
     UCM2(K)=0.
     UCM3(K)=0.
     UCM4(K)=0.
     UCM5(K)=0.
     UCM6(K)=0.
     VCM1(K)=0.
     VCM2(K)=0.
     VCM3(K)=0.
     VCM4(K)=0.
     VCM5(K)=0.
     VCM6(K)=0.
200 CONTINUE
   IMAX = IM+1
   DO 300 I=1,IMAX
     DO 300 J=1,JM
       WIND(I,J) = 0.0
300 CONTINUE
     DO 400 J=1,JM
       DTDET(J)= 0.
400 CONTINUE
     DO 500 K=1,67

```

```

HOB51(K)= 0.
HOB52(K)= 0.
HOB53(K)= 0.
HOB54(K)= 0.
HOB55(K)= 0.
HOB56(K)= 0.
500 CONTINUE
DO 600 K=1,50.
TIM(K)= 0.
RCT(K)= 0.
RAD(K)= 0.
VRMAX(K)= 0.
PZRO(K)= 0.
600 CONTINUE
DO 700 K=1,150
TIMPOS(K)= 0.
XPOS(K)= 0.
YPOS(K)= 0.
700 CONTINUE
RETURN
END
SUBROUTINE FIELD
COMMON/BLK1/GRID1(45,15),GRID2(45,15),
COMMON/BLK2/HYD3(300),HYD4(300),UCM1(300),UCM2(300),UCM3(300),UCM
10),HYD2(300),HYD3(300),HYD4(300),UCM1(300),UCM2(300),UCM3(300),UCM
24(300),VCM1(300),VCM2(300),VCM3(300),VCM4(300)
COMMON/BLK2/C2,CC,C1XI,C1ETA,DXI,DETA,DELT,F,IN,JM, IMM,JMM, N
COMMON/BLK5/DSCX1(45),DTDET(15),HYD5(300),HYD6(300),UCM5(300),UCM6
1(300),VCM5(300),VCM6(300)
COMMON/PLK7/HOB51(67),HOB52(67),HOB53(67),HOB54(67),HOB55(67),HOB5
16(67)
COMMON /TRANS/ XX(45,15) ,YY(45,15) ,CCSG(45,15),SING(45,15)

```

```

COMMON /HURR/ TIM(50) ,ROT(50) ,RAD(50) ,VRMAX(50)
1 PZRO(50) ,TIMPOS(150),XPOS(150),YPOS(150)
COMMON /HURR1/ YRANGE ,THIT ,XHIT ,YHIT ,
3 C10 ,C11 ,PHI ,
4 NT1 ,NT2 , PINF ,IX ,IY
5

C READ(5,11) NT1
FORMAT(15)
11 READ(5,12)(TIM(I),RCT(I),RAD(I),VRMAX(I),PZRO(I),I=1,NT1)
FORMAT(5F10.1)
12 READ(5,11) NT2
READ(5,13)(TIMPOS(I),XPOS(I),YPCS(I),I=1,NT2)
13 FORMAT(3F10.1)
WRITE(6,15)
15 FORMAT(1H1,15X,24HTHE STORM PARAMETERS ARE ,//,1X,
151H TIME ROTATION RADIUS MAX WINDS CEN PRESS ,//,1X,
250H (HRS) (DEG) (NM) (KNOTS) (MB) ,/)
WRITE(6,16)(TIM(I),ROT(I),RAD(I),VRMAX(I),PZRO(I),I=1,NT1)
16 FORMAT(1X,F8.0,F10.0,2F10.1,F10.0)
WRITE(6,17)
17 FORMAT(1H1,15X,37HTHE POSITIONS FOR THE STORM TRACK ARE ,//,1X,
129H TIME X COORD Y COORD ,//,1X,
210H (HRS) ,/)
WRITE(6,18)(TIMPOS(I),XPOS(I),YPOS(I),I=1,NT2)
18 FORMAT(1X,F8.0,2F10.1)
NU1 = 5
DO 400 I=1,IM
READ(NU1,5) (GRID2(I,J),J=1,JM)
5 FORMAT(11F7.2)
400 CONTINUE

```

```

DC 500 I=1,IM
READ(NU1,6) (S(I,J),J=1,JM)
6 FORMAT(5E14.7)
500 CONTINUE
DO 600 I=1,IM
READ(NU1,7) CSDXI(I)
7 FORMAT(E14.7)
600 CONTINUE
DC 700 J=1,JM
READ(NU1,8) DTDF(J)
8 FORMAT(2X,E14.7)
700 CONTINUE
READ(NU1,9)(HCRS1(I),I=1,67)
READ(NU1,9)(HCRS2(I),I=1,67)
READ(NU1,9)(HCRS3(I),I=1,67)
READ(NU1,9)(HCRS4(I),I=1,67)
READ(NU1,9)(HCRS5(I),I=1,67)
READ(NU1,9)(HCRS6(I),I=1,67)
9 FORMAT(19F4.1)
DC 300 II=1,67
HCRS1(II)= 99999.
HCRS1(II)=HCRS1(II)*0.3048
HCRS2(II)=HCRS2(II)*0.3048
HCRS3(II)=HCRS3(II)*0.3048
HCRS4(II)=HCRS4(II)*0.3048
HCRS5(II)=HCRS5(II)*0.3048
HCRS6(II)=HCRS6(II)*0.3048
300 CONTINUE
DC 101 I=1,IM
READ (5,10) (XX(I,J),YY(I,J),J=1,JM)
10 FORMAT (10F7.2)

```

C

```

101 CONTINUE
DC 102 I=1,IM
  READ(5,19) (COSG(I,J),SING(I,J),J=1,JM)
19  FORMAT (10F8.5)
102 CONTINUE
DO 200 J=1,JM
DC 100 I=1,IM
  IJ=I+J
  IF((IJ/2)*2.EQ.IJ)GO TO 110
  GRID2(I,J)=GRID2(I,J)*0.3048*6.0
  GO TO 100
110 CONTINUE
  GRID1(I,J)=0.
  GRID2(I,J)=C.C
100 CONTINUE
200 CONTINUE
CCC****
  WRITE(6,210)
210 FORMAT(1H1,////,20X,16HD F P T H S (M) ,///,7X,5HS E A ,58X,9HC 0
      9 A S T ,//)
  WRITE(6,211)(J,J=2,JMM,2)
211 FORMAT(8X,7(6X,2HJ=,I2),/)
  WRITE(6,212)(J,J=1,JM,2)
212 FORMAT(4X,8(6X,2HJ=,I2),/)
  DO 215 I=1,IM,2
  K= I+1
  WRITE(6,213)I,(GRID2(I,J),J=2,JMM,2)
213 FORMAT(1X,2HI=,I2,3X,7(4X,F6.1),/ )
  IF( I .EQ. IM ) GO TO 215
  WRITE(6,214)K,(GRID2(K,J),J=1,JM,2)
214 FORMAT(1X,2HI=,I2,8(4X,F6.1),/ )

```



```

215 CONTINUE
RETURN
END
SUBROUTINE ELEV
COMMON/BLK1/GRID1(45,15),GRID2(45,15),
10),HYD2(300),HYD3(300),HYD4(300),UCM1(300),UCM2(300),UCM3(300),UCM
24(300),VCM1(300),VCM2(300),VCM3(300),VCM4(300)
COMMON/FLK2/C2,CC,CIXI,Cieta,dXI,DETA,DELTA,F,IM,JM,
COMMON /BLK20/ CERIC,CS,C3,C4,RCI,INW2,IMW3,JMM2
COMMON/BLK5/DSDXI(45),DTDET(15),HYD5(300),HYD6(300),UCM5(300),UCM6
1(300),VCM5(300),VCM6(300)
COMMON/STCRW/AC,XEYE,YEYF,P(45,15),WIND(46,15)

DO 180 J=3,JMM
DTET=DTDET(J)*DETA
IS= 4
IMS= IMM3
IF((J/2)*2.EQ.J) IS = 3
IF(IS.EQ.3) IMS = IMM2
JP1 = J+1
JM1 = J-1
DO 130 I=IS,IMS,2
IP1 = I+1
IM1 = I-1
C9= DELT/S(I,J)/S(I,J)
DSXI=DSDXI(I)*DXI
URIT = GRID1(IP1,J)*S(IP1,J)
ULEF = GRID1(IM1,J)*S(IM1,J)
VTOP = GRID2(I,JP1)*S(I,JP1)
VBOT = GRID2(I,JM1)*S(I,JM1)
GRID1(I,J) = GRID1(I,J)- C9*( (URIT-ULEF)/DSXI+(VTOP-VBOT)/DTET )

```

C

```

130 CCNT INUE
180 CONTINUE
CC***
CTET= CTDET(JM)*DETA
DO 170 II=2,IMM,2
  IP1=II+1
  IM1=II-1
  C9= DELT/S(II,JM)/S(II,JM)
  DSXI= DSXI(II)*DXI
  URIT= GRID1(IP1,JM)*S(IP1,JM)
  ULEF= GRID1(IM1,JM)*S(IM1,JM)
  IF( II .EQ. 2 .OR. II .EQ. IMM ) ULEF=URIT
  VBOT= GRID2(II,JM)*S(II,JM)
  VTOP= -VBOT
  GRID1(II,JM)=GRID1(II,JM)-C9*((URIT-ULEF)/DSXI+(VTOP-VBOT)/DIET)
170 CONTINUE
C
DC 30 J=3,JMM2,2
II= 2
GRID1(II,J)=GRID1(II,J)-(DELT/S(II,J)/S(II,J))*(S(II,J+1)*GRID2(II
1,J+1)-S(II,J-1)*GRID2(II,J-1))/(DETA*CTDET(J))
II= IMM
GRID1(II,J)=GRID1(II,J)-(DELT/S(II,J)/S(II,J))*(S(II,J+1)*GRID2(II
1,J+1)-S(II,J-1)*GRID2(II,J-1))/(DETA*CTDET(J))
30 CONTINUE
CC***
DC 150 II=2,IMM
IF((II/2)*2.EQ.II) GO TO 140
GRID1(II,2)= P(II,2)- GRID2(II,3)/CS
GRID1(II,2)=0.25*(P(II-1,1)+GRID1(II-1,3)+P(II+1,1)+GRID1(II+1,3))
GO TO 150
CCC

```

```

140 BARO=P(11,1)
CCC  GRID1(11,1)= BARO=GRID2(11,2)/CS
    GRID1(11,1)= BARC
150 CONTINUE
    RETURN
    END
    SUBROUTINE FLUX
    COMMON/ELK1/GRID1(45,15),GRID2(45,15),
10),HYD2(300),HYD3(300),HYD4(300),UCM1(300),UCM2(300),UCM3(300),UCM
24(300),VCM1(300),VCM2(300),VCM3(300),VCM4(300)
    COMMON/ELK2/C2,CC,CIX1,C1ETA,DX1,DETA,DELT,F,IM,JM, IMM,JMM, N
    COMMON /BLK20/ CCRIO,CS,C3,C4,RCI,IMM2,IMM3,JMM2
    COMMON/BLK5/DSDX1(45),DTDET(15),HYDS(300),HYD6(300),UCM5(300),UCM6
1(300),VCM5(300),VCM6(300)
    COMMON/STCRN/NO,XEYE,YEYE,P(45,15),WIND(46,15)

C
DO 8999 J=1,JM
DO 8999 I=1,IM,2
    IP1=I+1
    WABS=SQRT(WIND(I,J)**2+WIND(IP1,J)**2)
    IF(WABS.LE.7.0)GO TO 9998
    WCOF=1.100E-06+((1.-7./WABS)**2)*2.50E-06
    GO TO 9997
9998 WCOF=1.100E-06
9997 DUWX=WIND(I,J)
    DUWY=WIND(IP1,J)
    WIND(I,J)=WCOF*WABS*DUWX
    WIND(IP1,J)=WCOF*WABS*DUWY
8999 CONTINUE
C
DO 130 J=2,JMM

```

```

IS = 3
IMS = IMM2
IF((J/2)*2.EQ.J) IS=4
IF(IS.EQ.4) IMS=IMN3
JP1 = J+1
JM1 = J-1
CC 80 I=IS,IMS,2
IP1 = I+1
IM1 = I-1
IX=I
IY=IP1
IF(IS=4) 270, 280, 270
280 IX=IM1
IY=I
270 CCNTINUE
CXI= CXI/S(I,J)/DSDXI(I)
CETA= CETA/S(I,J)/DIDET(J)
C1 = GRID1(IM1,J)-GRID2(IM1,J)
D2 = GRID1(IP1,J)-GRID2(IP1,J)
C3 = GRID1(I,JM1)-GRID2(I,JM1)
C4 = GRID1(I,JP1)-GRID2(I,JP1)
DELHX = GRID1(IP1,J)-GRID1(IM1,J)-(P(IP1,J)-P(IM1,J))
DELHY = GRID1(I,JP1)-GRID1(I,JM1)-(P(I,JP1)-P(I,JM1))
G = SQRT(GRID1(I,J)*GRID1(I,J)+GRID2(I,J)*GRID2(I,J))
AVHX = C.5*(D1+D2)
AVHY = C.5*(D3+D4)
DBAR = C.5*(AVHY+AVFX)
G = (1.C+C2*F*Q)/(DBAR*DBAR)).
G2 = G*G
A = GRID1(I,J)+RCT*GRID2(I,J)-CXI*AVHX*DELFX+C2*WIND(IWX,J)
B = GRID2(I,J)-ROT*GRID1(I,J)-CETA*AVHY*DELFY+C2*WIND(IWY,J)

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```

GRID1(I,J) = (G*A+C3*B)/(G2+C4)
GRID2(I,J) = (G*B-C3*A)/(G2+C4)
      80 CONTINUE
      130 CONTINUE
CC*****
DC 140 I=3,IMW2,2
CXI=C1X1/(S(I,JM)*DSDXI(I))
DELHX = GRID1(I+1,JM)-GRID1(I-1,JM)=(P(I+1,JM)-P(I-1,JM))
Q = ABS(GRID1(I,JM))
DBAR = 0.5*(GRID1(I-1,JM)-GRID2(I-1,JM)+GRID1(I+1,JM)-
+GRID2(I+1,JM))
G = (1.0+C2*F*Q)/(DBAR*DBAR)
GRID1(I,JM) = (GRID1(I,JM)-CXI*DBAR*DELHX+C2*WIND(I,JM))/G
      140 CONTINUE
      GRID1(1,JM)= GRID1(3,JM)
      GRID1(IM,JM)= GRID1(IMM2,JM)
CC*****
DO 9000 II=2,IMM,IMM3
DC 9000 J=3,JMM
IF( (J/2)*2 .EQ. J ) GO TO 8100
GO TO 8500
      8100 CCNTINUE
CETA= C1ETA/S(II,J)/DTDET(J)
DELHY=GRID1(II,J+1)-GRID1(II,J-1)=(P(II,J+1)-P(II,J-1))
AVHY=0.5*(GRID1(II,J+1)-GRID2(II,J-1)+GRID1(II,J-1)-GRID2(II,J-1))
Q= SQRT( GRID1(II,J)*GRID1(II,J)+GRID2(II,J)*GRID2(II,J) )
G= (1.0+C2*F*Q)/(AVHY*AVHY)
      III=3
      IF( II .EQ. IMM ) III= IMM2
      UBAR= 0.5*( GRID1(II,J+1)+GRID1(III,J-1) )
      UFLUX= UBAR + GRID1(II,J)

```



```

E= GRID2(II,J)-RCT*UFLUX-CETA*AVHY*DELHY+C2*WIND(II,J)
GRID2(II,J)=B/G
GRID1(II,J)= UHAR
GC TO 9000
8900 CONTINUE
III= 1
IIII= 3
IF( II .EQ. IMM ) III= IM
IF( II .EQ. IMM ) IIII= IMM2
GRID1(III,J)= GRID1(IIII,J)
9000 CONTINUE
CC*****
CC SPECIAL CALCULATIONS FOR SEAWARD CORNERS
DO 9050 I=2,IMM,IMM3
II= 3
IF( I .EQ. IMM ) II= IMM2
IS= II-1
Q1= SORT(GRID1(II,1)**2+GRID2(II,1)**2)
Q2= SORT(GRID1(I,2)**2+GRID2(I,2)**2)
D1=(GRID1(II-1,1)-GRID2(II-1,1)+GRID1(II+1,1)-GRID2(II+1,1))/2.
D2=(GRID1(I,1)-GRID2(I,1)+GRID1(I,3)-GRID2(I,3))/2.
G1=(1.+C2*F*Q1/(D1**2))
G2=(1.+C2*F*Q2/(D2**2))
DELHX= GRID1(II+1,1)-GRID1(II-1,1)-(P(II+1,1)-P(II-1,1))
DELHY= GRID1(I,3)-GRID1(I,1)-(F(I,3)-F(I,1))
CXI = CXI/S(II,1)/DSCXI(II)
CETA = CETA/S(I,2)/DTDET(2)
AB = GRID1(II,1)+C3*GRID2(II,1)-CXI*D1*DELHX+C2*WIND(II,1)
AP = AP+.5*C3*GRID2(II+IS,2)
BB = GRID2(I,2)-C3*GRID1(I,2)-CETA*D2*DELHY+C2*WIND(I,2)
BP = BP+.5*C3*GRID1(II,3)

```

```

DENOM = G1*G2+.25*C4
GRID1(I1,1) = (AP*G2+BP*.5*C3)/DENOM
C_02(I,2) = (BP*G1-AP*.5*C3)/DENOM
GR_1(I,2) = .5*(GRID1(I1,3)+GRID1(I1,1))
GRID2(I1,1) = .5*(GRID2(I,2)+GRID2(I1+IS,2))
9050 CONTINUE
GRID1(I,1) = GRID1(I,1)
GRID1(IM,1) = GRID1(IMM2,1)
RETURN
END
SUBROUTINE CRAW1
COMMON/BLK1/GRID1(45,15),GRID2(45,15),
10),HYD2(300),HYD3(300),HYD4(300),UCM1(300),UCM2(300),UCM3(300),UCM
24(300),VCM1(300),VCM2(300),VCM3(300),VCM4(300)
COMMON/BLK2/C2,CC,C1XI,C1ETA,DXI,DETA,DELT,F,IM,JM, IMM,JMM, N
COMMON /BLK20/ CORIO,CS,C3,C4,ROT,IMM2,IMM3,JMM2
COMMON/BLK3/ GRAV, NMAX,IH1,JH1,IT1,JT1,IH2,
1JH2,IT2,JT2,IH3,JH3,IT3,JT3,IH4,JH4,IT4,JT4,INC
COMMON/BLK5/DSCXI(45),DTDET(15),HYD5(300),HYD6(300),UCM5(300),UCM6
1(300),VCM5(300),VCM6(300)
COMMON/BLK6/IF5,JH5,IT5,JT5,IH6,JH6,IT6,JT6

C
DIMENSION UVEL(45,15),VVEL(45,15)
EQUIVALENCE (UVEL(2),VVEL)

C
MIN = ((N-1)*DELT)/60. + 1.E-5
IF(MOD(MIN,30).NE.0)RETURN
NP = N/INC + 1
HYD1(NH) = GRID1(IH1,JH1)
HYD2(NH) = GRID1(IH2,JH2)
HYD3(NH) = GRID1(IH3,JH3)

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```

C
HYD4(NH) = GRID1(IH4,JH4)
HYD5(NH) = GRID1(IH5,JH5)
HYD6(NH) = GRID1(IH6,JH6)
CALL METER

C
IF (MOD(MIN,60) .NE. 0) RETURN
C
CALCULATE THE X AND Y VELOCITIES
C
AT THE INTERIOR POINTS
DO 100 J=2,JNM
IS = 3
IMS = IMM2
IF ((J/2)*2 .EQ. J) IS = 4
IF (IS .EQ. 4) IMS = IMM3
CCC FOR RAD. LBC IS=2 AND IMS=IMM
CCC REM CHANGE IN DO 310
JPI = J+1
JMI = J-1
DO 100 I=IS,IMS,2
IP1 = I+1
IM1 = I-1
D1 = GRID1(IM1,J)-GRID2(IM1,J)
D2 = GRID1(IP1,J)-GRID2(IP1,J)
D3 = GRID1(I,JMI)-GRID2(I,JMI)
D4 = GRID1(I,JPI)-GRID2(I,JPI)
DEAR = .25*(D1+D2+D3+D4)
UVEL(I,J) = GRID1(I,J)/DEAR
VVEL(I,J) = GRID2(I,J)/DEAR
100 CONTINUE
C
BOUNDARY POINTS
DO 201 J=1,JM,JNM
DO 200 I=3,IMM2,2

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```

IP1 = I+1
IM1 = I-1
D1 = GRID1(IM1,J)=GRID2(IM1,J)
D2 = GRID1(IP1,J)=GRID2(IP1,J)
DBAR = .5*(D1+D2)
UVEL(I,J) = GRID1(I,J)/DBAR
VVEL(I,J) = GRID2(I,J)/DBAR
200 CONTINUE
UVEL(IM,J) = GRID1(IM,J)/DBAR
VVEL(IM,J) = GRID2(IM,J)/DBAR
201 CONTINUE
I = 1
DO 202 J=1,JM,JMM
D1 = GRID1(2,J)=GRID2(2,J)
D2 = GRID1(4,J)=GRID2(4,J)
DBAR = .5*(D1+D2)
UVEL(I,J) = GRID1(I,J)/DBAR
VVEL(I,J) = GRID2(I,J)/DBAR
202 CONTINUE
DO 310 I=2,IMM,IMM3
DO 310 J=2,JMM
IF ((J/2)*2.EQ. J) GC TC 305
II = 1
IIII = 4
IF (I.EQ. IMM) II = IM
IF( I.EQ. IMM ) IIII= IMM3
D1 = GRID1(I,J)=GRID2(I,J)
D2 = GRID1(IIII,J)=GRID2(IIII,J)
DBAR = 0.5*(D1+D2)
UVEL(II,J) = GRID1(II,J)/DBAR
VVEL(II,J) = GRID2(II,J)/DBAR

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```

305 GO TO 310
CONTINUE
JP1 = J+1
JM1 = J-1
D3 = GRID1(I,JP1)-GRID2(I,JP1)
D4 = GRID1(I,JM1)-GRID2(I,JM1)
DBAR = 0.5*(D3+D4)
UVEL(I,J) = GRID1(I,J)/DBAR
VVEL(I,J) = GRID2(I,J)/DBAR
310 CONTINUE
DO 311 I=1,IM
DO 311 J=1,JM
IF( MOD(I+J,2) .EQ. 1 ) GO TO 311
UVEL(I,J) = UVEL(I,J)*100.
VVEL(I,J) = VVEL(I,J)*100.
311 CCNT INUF
C
T = MIN/60.
WRITE (6,400) T
400 FCRMAT (1H1,6X,13HTIME (F5) = ,F5.2,///,20X,12HE L E V (M),
1///,7X,5HS E A,5RX,5HC O A S T,/)
WRITE (6,405) (J,J=2,JMM,2)
405 FCRMAT (8X,7(6X,2HJ=,I2),/)
WRITE (6,406) (J,J=1,JM,2)
406 FCRMAT (4X,9(6X,2HJ=,I2),/)
DO 415 I=1,IM,2
K = I+1
WRITE (6,410) I,(GRID1(I,J),J=2,JMM,2)
410 FCRMAT (1X,2HI=,I2,3X,7(4X,F6.2),/)
IF (I .EQ. IM) GO TO 415
WRITE (6,411) K,(GRID1(K,J),J=1,JM,2)

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```

411 FORMAT (1X,2H1=,I2,8(4X,F6.2),/ )
415 CONTINUE
      WRITE (6,419) T
419 FORMAT (1H1,6X,13HTIME (PRS) = ,F6.2,///,20X,35HX AND Y V E L O C
1 I T I F S (CM/S),//,7X,5HS E A,58X,9HC C A S T,/)
      WRITE (6,425) (J,J=2,JMM,2)
      WRITE (6,426) (J,J=1,JM,2)
420 425 I=1,IM,2
      K = I+1
      WRITE (6,421) I,(LVEL(I,J),J=1,JM,2)
      WRITE (6,422) (VVEL(I,J),J=1,JM,2)
421 FORMAT (1X,2H1=,I2,8(4X,F6.1))
422 FORMAT (5X,8(4X,F6.1),/ )
      IF (I.EG. IM) GO TO 425
      WRITE (6,423) K,(LVEL(K,J),J=2,JMM,2)
      WRITE (6,424) (VVEL(K,J),J=2,JMM,2)
423 FORMAT (1X,2H1=,I2,3X,7(4X,F6.1))
424 FORMAT (8X,7(4X,F6.1), /)
425 CONTINUE
      RETURN
      END
      SUBROUTINE METER
      COMMON/BLK1/GFID1(45,15),GRID2(45,15),
10),HYD2(300),HYD3(300),HYD4(300),LCM1(300),UCM2(300),UCM3(300),UCM
24(300),VCM1(300),VCM2(300),VCM3(300),VCM4(300)
      COMMON/BLK2/C2,CC,C1X1,C1ETA,DX1,DETA,DELTA,F,IM,JM,
      COMMON/BLK3/ GRAV,
1 JF2,IT2,IT2,IF3,JF3,IT3,JT3,IF4,JH4,IT4,JT4,INC
      COMMON/BLK5/DSDXI(45),DIDET(15),HYDS(300),HYD6(300),UCM5(300),UCM6
1(300),VCM5(300),VCM6(300)
      COMMON/BLK6/IF5,JF5,IT5,JT5,IF6,JF6,IT6,JT6

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C

```

NUV= N/INC+1
DO 10 KK=1,6
  GC TO (20,30,40,50,60,70),KK
20  II = IT1
   JJ = JT1
   GC TO 80
30  II = IT2
   JJ = JT2
   GC TO 80
40  II = IT3
   JJ = JT3
   GC TO 80
50  II = IT4
   JJ = JT4
   GC TO 80
60  II=IT5
   JJ=JT5
   GC TO 80
70  II=IT6
   JJ=JT6
80  II = II-1
   I2 = II+1
   J1 = JJ-1
   J2 = JJ+1
   AVEDX = (GRID1(II,JJ)-GRID2(II,JJ)+GRID1(I2,JJ)-GRID2(I2,JJ))*0.5
   AVEDY = (GRID1(II,J1)-GRID2(II,J1)+GRID1(I1,J2)-GRID2(I1,J2))*0.5
   GC TO (110,120,130,140,150,160),KK
110 UCM1(NUV) = GRID1(I11,JT1)/AVEDX
   VCM1(NUV) = GRID2(I11,JT1)/AVEDY
   GC TO 10

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120 UCM2(NUV) = GRIC1(IT2,JT2)/AVEDX
    VCM2(NUV) = GRID2(IT2,JT2)/AVEDY
    GO TO 10
130 UCM3(NUV) = GRIC1(IT3,JT3)/AVEDX
    VCM3(NUV) = GRID2(IT3,JT3)/AVEDY
    GO TO 10
140 UCM4(NUV) = GRIC1(IT4,JT4)/AVEDX
    VCM4(NUV) = GRID2(IT4,JT4)/AVEDY
    GO TO 10
150 UCM5(NUV)=GRIC1(IT5,JT5)/AVEDX
    VCM5(NUV)=GRID2(IT5,JT5)/AVEDY
    GO TO 10
160 UCM6(NUV)=GRIC1(IT6,JT6)/AVEDX
    VCM6(NUV)=GRID2(IT6,JT6)/AVEDY
10 CCNT INUE
    RETURN
    END
    SUBROUTINE HUV
    COMMON/BLK1/GRID1(45,15),GRID2(45,15),
    10),HYD2(300),HYD3(300),HYD4(300),LCM1(300),UCM2(300),UCM3(300),UCM
    24(300),VCM1(300),VCM2(300),VCM3(300),VCM4(300)
    COMMON/BLK2/C2,CC,C1XI,C1ETA,DXI,DETA,DELT,F,IM,JM,
    10),IMM,JMM,N
    COMMON/ELK3/
    10),NMAX,IH1,JH1,IT1,JT1,IH2,
    10),JH2,IT2,JT2,IH3,JH3,IT3,JT3,IH4,JH4,IT4,JT4,INC
    COMMON/BLK5/DSDXI(45),DIDET(15),HYD5(300),HYD6(300),UCM5(300),UCM6
    1(300),VCM5(300),VCM6(300)
    COMMON/BLK6/IH5,JH5,IT5,JT5,IH6,JH6,IT6,JT6
    COMMON/BLK7/HOBS1(67),HOBS2(67),HOBS3(67),HOBS4(67),HCBSS5(67),HOBS
    16(67)
    WRITE (6,505) IH1,JH1,IH2,JH2,IH3,JH3,IH4,JH4,IH5,JH5,IH6,JH6

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C

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WRITE (6,506) IT1,JT1,IT2,JT2,IT3,JT3,IT4,JT4,IT5,JT5,IT6,JT6
505 FCRMAT(1H1,41F ADJUSTED-COMPUTED HYDROGRAPH (M) AT ,6(12,1H,,
6 12,7X),/,30H AND THE OBSERVED WATER LEVEL ,// )
506 FCRMAT(11X,34F-SIMULATED CURRENT (M/S) AT ,6(12,1H,,12,7X),/
1//)
J=1
K = 1
NDEX= NMAX/INC+1
DO 500 I=1,NDEX
T = (K-1)*DELTA/3600.
MINE = (K-1)*DELTA/60. +1.0F=05
C CORRECT COMPUTED H FOR INITIAL OBSERVED WATER LEVEL CONDITIONS
C
HYD1(I) = HYD1(I)+HORS1(I)
HYD2(I) = HYD2(I)+HORS2(I)
HYD3(I) = HYD3(I)+HORS3(I)
HYD4(I) = HYD4(I)+HORS4(I)
HYD5(I) = HYD5(I)+HORS5(I)
HYD6(I) = HYD6(I)+HORS6(I)
WRITE (6,510) K,T,HYD1(I),HYD2(I),HYD3(I),HYD4(I),HYD5(I),HYD6(I)
IF( MOD(MINE,50).EQ.0)WRITE(6,513)HORS1(J),HORS2(J),HORS3(J),HORS4(
9J),HORS5(J),HORS6(J)
WRITE (6,511) UCM1(I),UCM2(I),UCM3(I),UCM4(I),UCM5(I),UCM6(I)
WRITE (6,512) VCM1(I),VCM2(I),VCM3(I),VCM4(I),VCM5(I),VCM6(I)
K = K+INC
IF(MOD(MINE,60).EQ.0) J=J+1
500 CONTINUE
510 FORMAT (/,13X,2HN=,15,10H T (HRS)=,F6.2,5H + ,6(F6.2,6X))
511 FCRMAT (39X,4FV ,6(F7.2,5X))
512 FCRMAT (39X,4FV ,6(F7.2,5X))
513 FCRMAT( 34X,7HORS H ,6(F6.2,6X))

```

```

RETURN
END
SUBROUTINE WINDF
COMMON/BLK2/C2,CC,C1X1,C1ETA,DX1,DETA,DELT,F,IN,JM, IMM,JMM, N
COMMON/ TRANS/XX(45,15),YY(45,15),COSG(45,15),SING(45,15)
COMMON /HURR/ TIM(50) ,ROT(50) ,RAC(50) ,VRMAX(50) ,
1 PZRO(50) ,TIMPCS(150),XPOS(150),YPOS(150)
COMMON /HURR1/ YRANCE ,THIT ,X+IT ,YHIT ,
3 C10 ,C11 ,PHI ,
4 NT1 ,NT2 , PINF ,IX ,IY
5 COMMON /EXTRA/ X(45,15) ,Y(45,15)
COMMON/ STCRM /NO,XEYE,YEYE,P(45,15),WIND(46,15)

DATA IT1P1,IT2P1/2,2/

NC=N
TIME=FLCAT(N-1)*DELT/3600.
DO 101 I=IT1P1,NT1
IF(TIM(I).GE.TIME) GO TO 102
101 CONTINUE
I=NT1
102 IT1=I-1
DO 103 I=IT2P1,NT2
IF(TIMPCS(I).GE.TIME)GO TO 104
103 CONTINUE
I=NT2
104 IT2= I-1
IT1P1=IT1+1
IT2P1=IT2+1
TFAC1=(TIME-TIM(IT1))/(TIM(IT1P1)-TIM(IT1))

```



```
TFAC2=(TIME-TIMPCS(IT2))/(TIMPOS(IT2P1)-TIMPOS(IT2))
DELT2=(TIMPCS(IT2F1)-TIMPCS(IT2))*3600.
```

C

```
R=RAD(IT1)+TFAC1*(RAD(IT1P1)-RAD(IT1))
VR=VRMAX(IT1)+TFAC1*(VRMAX(IT1P1)-VRMAX(IT1))
THETA=ROT(IT1)+TFAC1*(ROT(IT1P1)-ROT(IT1))
P=PZRC(IT1)+TFAC1*(PZRO(IT1P1)-PZRO(IT1))
XEYE=XPOS(IT2)+TFAC2*(XPCS(IT2P1)-XPOS(IT2))
YEYE=YPOS(IT2)+TFAC2*(YPOS(IT2P1)-YPOS(IT2))
US=(XPOS(IT2F1)-XPOS(IT2))/DELT2
VS=(YPOS(IT2F1)-YPOS(IT2))/DELT2
R=R*.84167
VR=VR*.515
US=US*2201.6
VS=VS*2201.6
THETA=(90.-THETA+PHI)*.0174533
CO=COS(-THETA)
C1=SIN(-THETA)
```

C

```
USR=US*CO + VS*C1
VSP=VS*CO - US*C1
```

C

```
CO 108 I=1,IX
CC 107 J=1,IY
XP=XX(I,J)
YP=YY(I,J)
XF1=XP-XEYE
YP1=YP-YEYE
RSM=SCRT(XP1**2 + YP1**2)
IF(MOD(I+J),2).EQ.1)GO TO 109
A=-YP1*C10 -XP1*C11
```

```

C
C
C
R= XPI*CI0 -YPI*CI1
IF(RSML.LT.1.0E-10) RSML= 1.0E-10
IF(RSML.LE. 9)GC TO 105

C
C
C
POINT IS OUTSIDE RADIUS TO MAX WINDS

S1=R/(R+RSML)
S2=(VR/RSML)*(R/RSML)**.45
GC TO 106

C
C
C
POINT IS INSIDE RADIUS TO MAX WINDS

105 S1=RSML/(R+RSML)
S2=(VR/RSML)*((RSML/R)**1.5)
106 X1=(USR*S1)+(A*S2)
Y1=(VSR*S1)+(B*S2)

C
C
C
ROTATE VELOCITY FOR CURV GRID

C=COSG(I,J)
S=SING(I,J)
XR=X1*C+Y1*S
YR=Y1*C-X1*S
X(I,J)=XR
Y(I,J)=YR
GC TO 107

109 RDIST=22.*.84167
PP=P0+(FINF-P0)*EXP(-RDI ST/RSML)
P(I,J)=(FINF-PP)*.01
107 CONTINUE
108 CCNTINUE

```

```

DO 110 J=1, IV
DC 110 I=1, IX, 2
IF((J/2)*2.EQ.J)GO TO 112
WIND(I, J)=X(I, J)
WIND(I+1, J)=Y(I, J)
GO TO 110
112 IF(I.EQ.IX)GO TO 110
WIND(I, J)=X(I+1, J)
WIND(I+1, J)=Y(I+1, J)
110 CCNTINUE
RETURN
END
FUNCTION YLAND(XD)
DATA YRANGE /17./
YLAND=ABS(XD-YRANGE)/7.
RETURN
END

```

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